

## Supplemental Material to

# Physical transport of magmatic sulfides promotes copper enrichment in hydrothermal ore fluids

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## Stokes calculations

T-X dependent viscosities of silicate magmas were calculated with the excel calculator available at <https://www.eoas.ubc.ca/~krussell/VISCOSITY/grdViscosity.html> Giordano et al. (2008; with thanks to Daniele Giordano, pers. comm, 2021).

P-T-X dependent melt densities were calculated with the calculator supplement to Iacovino and Till (2018; Supplementary File 1 at

<https://www.jvolcanica.org/ojs/index.php/volcanica/article/view/12>). A fixed sulfide density of 4600 kg m<sup>-3</sup> was used, ignoring compositional variations, the small P-T dependence of sulfide density (Nishida et al., 2011) and the composition-dependent melting of the FeS-rich phase (e.g., Kress et al., 2008). As sulfides observed in lower-crustal cumulates are interpreted to have been mostly solid (Chen et al., 2020; Du and Audétat, 2020), we use the Stokes formula for solids; liquid droplets might sink up to 1.5 times faster (cf. De Bremond d'Ars et al., 2001; Yao et al., 2019), an effect that is insignificant in light of parameter uncertainties. For the silicate melt, three compositions were considered, with additional 3 or 10% H<sub>2</sub>O, normalised to 100 wt%:

Table S1: Average continental arc basalt composition from Rezeau and Jagoutz (2020) (left, used for thermodynamic and Stokes calculations) and the reference diorite (dacite) reported by Cox et al. (2020) (for Stokes calculations). For the thermodynamic modeling shown in Figures 2 and 3, minor MnO and P<sub>2</sub>O<sub>5</sub> was neglected, the H<sub>2</sub>O content was varied between 3 and 6% and Fe<sup>III</sup>/Fe<sup>tot</sup> was varied between 0.18 and 0.48.

	Continental arc basalt	BH-1 diorite / dacite
SiO <sub>2</sub>	50.43	62.9
TiO <sub>2</sub>	0.99	0.35
Al <sub>2</sub> O <sub>3</sub>	15.64	12.99
FeO <sup>tot</sup>	8.56	4.76
MnO	0.14	0.13
MgO	10.24	2.25
CaO	9.86	2.76
Na <sub>2</sub> O	2.79	3.04
K <sub>2</sub> O	1.04	0.68
P <sub>2</sub> O <sub>5</sub>	0.26	0.07
H <sub>2</sub> O	10 / 3 or 6	10.00
Fe <sup>III</sup> /Fe <sup>tot</sup>	0.18 - 0.48	

Magma ascent rates vary over many orders of magnitude depending on data source (U-Th-series disequilibrium data or speedometers based on component diffusion profiles between phenocryst, glass matrix or inclusions) and geological process or tectonic setting – see reviews by Turner and Costa (2007) and Neave and MacLennan (2020; many estimates extend to even higher flow rates than shown in Figure 1, especially in the upper crust).

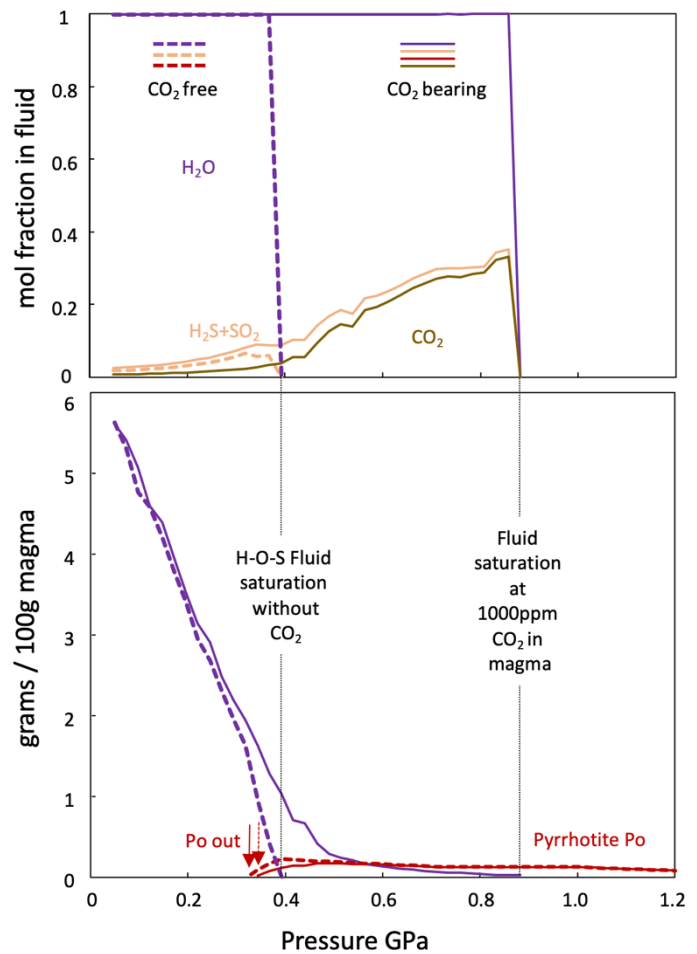
### **Thermodynamic modeling**

The Perple\_X free energy minimization package (Connolly, 2005, v. 6.9.1 of July 2021, <https://www.perplex.ethz.ch>) was used to compute phase relations in multicomponent model systems of fixed bulk composition, representing hydrous arc basalt with excess FeS. Mark Caddick (Virginia Tech) is thanked for its compilation for MacOS.

For the silicate melt we chose the multicomponent model of Holland et al. (2018). This model does not include S dissolved in the silicate melt, which has been modelled in many detailed experimental (e.g., Mavrogenes and O'Neill, 1999; Liu et al., 2007; Jugo, 2009; Fortin et al., 2015; Matjuschkin et al., 2016) and computational studies (e.g., Rottier et al., 2019; Chen et al., 2020; Yao and Mungall, 2020). In reality, CaSO<sub>4</sub> dissolved in silicate melt will replace some of the predicted anhydrite field in oxidized magmas. The solubility of FeS is more limited and solid FeS is stabilised to higher T and fO<sub>2</sub> with increasing total pressure (Matjuschkin et al., 2016).

Our results focus on the competition among solid sulfide, sulfate, and S dissolved in a magmatic molecular H-O-S fluid. We avoid sequential computing of the thermodynamics of FeO as a major schematic component, e.g., from initial calculations using MELTS (Ghiorso and Sack, 1995) followed by computation of fluid species via fO<sub>2</sub> or fS<sub>2</sub> (Mungall et al., 2015; Yao and Mungall, 2020). Although thermodynamically equivalent, calculation of overall multicomponent equilibrium by Gibbs energy minimization has the advantage of yielding quantities and compositions of all mineral, melt and fluid phases simultaneously. This approach emphasises the arguably most fundamental behavior of porphyry-mineralising arc magmas: the positive feedback between crystallization and massive production of H<sub>2</sub>O-dominant fluid over a narrow P-T interval ('second boiling'; Burnham and Ohmoto, 1980). The high concentration of H<sub>2</sub>O in arc magmas justifies ignoring minor CO<sub>2</sub> which is generally insufficient to drive sulfide decomposition at mid- to lower-crustal pressures (Fig. S1). Our computational approach can be readily extended to future models which should incorporate the distribution and speciation of S as well as chalcophile trace-elements between coexisting S-bearing silicate melt, solid and liquid sulfide, other minerals, and hydrothermal fluids including Cl as the next-most influential fluid component (Dolejs and Zajacz, 2018).

Figure S1: The calculated effect of CO<sub>2</sub> for the near-adiabatic *P-T* transect shown in Figures 2B and D of the main paper, including the addition of 1000ppm CO<sub>2</sub>. CO<sub>2</sub> solubility in the melt was modelled by assuming Henryian behavior and matching the solubilities reported by Morizet et al. (2010), which extends older experimental data that are commonly used in fluid - melt modelling studies (e.g., Mungall et al., 2015; Yao and Mungall, 2020). Fluid composition (top) and phase quantities (bottom) for the CO<sub>2</sub> bearing system are shown by solid lines, compared with those of the simplified H-O-S system shown with dashed lines. CO<sub>2</sub> addition causes fluid saturation at higher pressure, but the fluid quantity is too small to significantly affect the abundance of magmatic sulfides, which become destabilized by massive H<sub>2</sub>O exsolution closer to the solidus. Most importantly, the pressure at which de-sulfidation of entrained sulfide is completed is practically unchanged (small arrows indicating “Po out”). Thus magmatic CO<sub>2</sub> has a minor, albeit moderating, influence on the sulfide stability predicted for the CO<sub>2</sub>-free system. We ignored this second-order complexity and consider only the H-O-S limiting model because, unlike iron sulfide, the C-content of the melt adds an arbitrary degree of freedom that is not directly constrained by the presence of an additional phase.



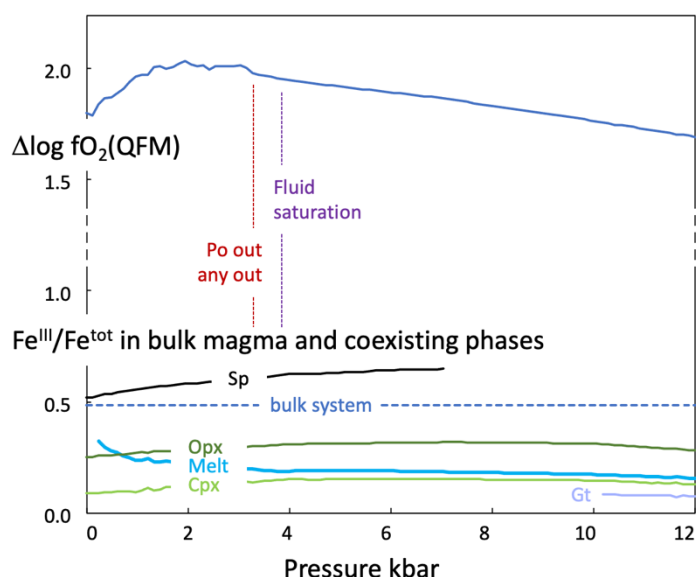
For the supercritical H-O-S or C-H-O-S fluid, the Hybrid Molecular Fluid model following Connolly (1995) was used: [https://perplex.ethz.ch/Perple\\_X\\_generic\\_hybrid\\_fluid\\_EoS.html](https://perplex.ethz.ch/Perple_X_generic_hybrid_fluid_EoS.html)

Crystalline solid-solution models are from (or as recommended by) Holland et al. (2018) based on endmember thermodynamic data for minerals from the ds6.33 revision of Holland and Powell (2011). MSS or pyrrhotite (Po(HP)) is modelled as solid solution with the endmembers  $\text{tro} = \text{FeS}$  and  $\text{trov} = \text{Fe}_{0.88}\text{S}$ . In the binary Fe-S system solid MSS is stable to  $\sim 1200^\circ\text{C}$  (e.g., Kitakaze et al., 2016) and a Cu-Ni-bearing sulfide melt is stabilised to lower temperatures, but these minor components contribute less than 10% to natural (possibly composite liquid + solid) magmatic sulfide particles (e.g., Rottier et al., 2020). We suppressed amphibole (cAmph(G)) and ilmenite solution (Ilm(WPH)) because these models have unrealistically high stable ferric iron-contents and destabilize magnetite even at the most oxidising conditions, counter to geological observation. The 'Mafics' (= pyroxenes  $\pm$  olivine  $\pm$  biotite shown in Figure 2) will in reality be dominated by amphibole in water-rich oxidised arc magmas considered here (Nandedkar et al., 2014; Loucks, 2021).

For the magma composition we chose the average continental arc basalt of Rezeau and Jagoutz (2020) and Schmidt and Jagoutz (2017). Their anhydrous model composition (Table S1) was varied by adding a fixed quantity of FeS (0.5 wt%) and variable concentrations of H<sub>2</sub>O between 3 and 6 wt% (a range considered to be ideal for subsequent hydrothermal ore formation; Chiaradia, 2020), and by varying the bulk Fe<sup>III</sup>/Fe<sup>tot</sup> ratio between 0.18 and 0.48 at given FeO<sup>tot</sup>. This variation covers the range of Fe<sup>III</sup>/Fe<sup>tot</sup> reported from modelling-independent Fe-XANES measurements on silicate melt inclusions (~ 0.15 – 0.4; (Kelley and Cottrell, 2009; Brounce et al., 2022)).

Fe<sup>III</sup>/Fe<sup>tot</sup> in the bulk system dominates the redox potential of the magma, which can be measured by oxygen fugacity relative to the quartz – fayalite – magnetite equilibrium ( $\Delta\log fO_2(QFM)$ ; (Mavrogenes and O'Neill, 1999). Gibbs energy minimization emphasizes that the trace volatile components (O<sub>2</sub>, H<sub>2</sub>) are dominated by equilibria between major ferrous and ferric components of oxides, silicates and the melt and modified by reactions among minor sulfur species: SO<sub>2</sub> and H<sub>2</sub>S in the fluid and magmatic FeS and sulfate (here modelled by anhydrite, in reality partly dissolved in melt). We deliberately avoid fixing  $\Delta\log fO_2(QFM)$  (as commonly done using the MELTS model following Ghiorso and Sack, 1995; e.g., Rezeau and Jagoutz, 2020), to illustrate the natural competition among the main redox-sensitive phases. The model of Holland et al. (2018) for Fe components in the silicate melt satisfies experimental relations between  $fO_2$  and Fe<sup>III</sup>/Fe<sup>tot</sup> (Kress and Carmichael, 1991; O'Neill et al., 2006) and resulting  $\Delta\log fO_2(QFM)$  between +1.0 and +2.2 for the chosen range of bulk compositions are consistent with oxybarometer results of natural porphyry-copper mineralizing magmas as reviewed by Richards (2015) and Loucks et al. (2020). Figure S2 shows Fe<sup>III</sup>/Fe<sup>tot</sup> variations along the P-T transect of Figure 2D of the paper and the resulting  $\Delta\log fO_2(QFM)$ .

Figure S2: Variation of  $\Delta\log fO_2(QFM)$  (upper part of diagram) and the Fe<sup>III</sup>/Fe<sup>tot</sup> ratio in silicate and oxide phases at given bulk ratio for the system (lower part), for the same model magma and P-T transect as shown in Figure 2 of the paper. The ratio in the silicate melt is lower than in the bulk system, not only because of the stabilization of Fe<sup>III</sup>-rich spinel at pressures below ~7 kbar but also because of the competition of O between the major phases and minor pyrrhotite and anhydrite at all pressures above 'Po out' and 'any out'.



The thermodynamic database files (hp633ver.dat), solid solution properties (solution\_model.dat) and computational options such as grid resolution (perplex\_options.dat) are stored in a folder Perple\_X\_6\_Cu at <https://polybox.ethz.ch/index.php/s/qwnROpGuNQBWgjf>, which also contains all job definition files (e.g., RJox3=2x2\_6H2O\_Po.dat — see box below for the job example used to calculate Figures 2, S1, S2) as well as the resulting output and plot files. Parts of this repository will be published at <https://www.research-collection.ethz.ch>.

The two gray P-T transects in Figure 2B along which phase proportions depicted in 2A and 2C are based on Annen et al. (2006) who coined the now widely used term ‘hot zone’ as a region of lower-crustal magma storage and differentiation.

#### Job file example RJox3=2x2\_6H2O\_Po.dat

```
hp633ver.dat  thermodynamic data file.  | THIS INCLUDES THE MELT SPECIES OF  HOLLAND ET AL JPET 2018
print          | no_print suppresses print output
plot           | obsolete 6.8.4+
solution_model.dat  | solution model file, blank = none
RezeauJagoutz'2020_Calcalkaline_Basalt_Fe(III)=2xFe(II) 6%H2O  Po(HP)=trov-trot-ss
perplex_option.dat  | Perple_X option file
  5 calculation type: 0- composition, 1- Schreinemakers, 3- Mixed, 4- swash, 5- gridded min, 7- 1d fract, 8- gwash, 9- 2d fract,
10- 7 w/file input, 11- 9 w/file input, 12- 0d infiltration
  0 unused place holder, post 06
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  0 unused place holder, post 06
  0 number component transformations
  20 number of components in the data base
  0 component amounts, 0 - mole, 1 mass
  0 unused place holder, post 06
  0 unused place holder, post 06
  0 unused place holder, post 05
  0 ifug EoS for saturated phase
  2 gridded minimization dimension (1 or 2)
  0 special dependencies: 0 - P and T independent, 1 - P(T), 2 - T(P)
0.00000  0.00000  0.00000  0.00000  0.00000  Geothermal gradient polynomial coeffs.

begin thermodynamic component list
SiO2  1  .7880  0.00000  0.00000  molar amount
TiO2  1  .0116  0.00000  0.00000  molar amount
Al2O3 1  .1440  0.00000  0.00000  molar amount
O2    1  .0108  0.00000  0.00000  molar amount
FeO   1  .1172  0.00000  0.00000  molar amount
MgO   1  .2385  0.00000  0.00000  molar amount
CaO   1  .1651  0.00000  0.00000  molar amount
Na2O  1  .0423  0.00000  0.00000  molar amount
K2O   1  .0104  0.00000  0.00000  molar amount
H2O   1  .3127  0.00000  0.00000  molar amount
S2    1  .0027  0.00000  0.00000  molar amount
end thermodynamic component list

begin saturated component list
end saturated component list

begin saturated phase component list
end saturated phase component list

begin independent potential/fugacity/activity list
end independent potential list
```

[continued]

begin solution phase list

Chl(W)

melt(HGP)

HOS-Fluid

| cAmph(G) Suppressing this amphibole containing overly stable riebeckite component

Cpx(HGP)

Opx(HGP)

Sp(HGP)

| Ilm(WPH) Suppressing this ilmenite containing overly stable hematite component

Bi(HGP)

feldspar

Gt(HGP)

Mica(W)

Crd(HGP)

O(HGP)

Ep(HP11)

Po(HP) |solid solution of trot=FeS and trov=Fe0.88S endmembers

end solution phase list

12000.0	1473.00	0.00000	0.00000	0.00000	max p, t, xco2, mu_1, mu_2
1.00	973.000	0.00000	0.00000	0.00000	min p, t, xco2, mu_1, mu_2
0.00000	0.00000	0.00000	0.00000	0.00000	unused place holder post 06

2 1 4 5 3 indices of 1st & 2nd independent & sectioning variables

## H-S-metal diffusion in silicate melt and selective metal precipitation

We cite Zhang and Ni (2010) for the fast diffusion of H compared to most metal components. This recent review also discusses the difficulty of quantifying the diffusion of H<sub>2</sub>O and H<sub>2</sub> as molecular entities controlling magma devolatilization and redox equilibria. Comparison with S diffusion is further explored by Lierenfeld et al. (2018) who show that H<sub>2</sub>S diffusion is comparably fast whereas SO<sub>2</sub> and SO<sub>4</sub> diffuse much more slowly than H<sub>2</sub>O in silicate melt. Also Cu<sup>+</sup> diffuses comparably fast, similar to H species (Ni et al., 2017), so for Cu alone the mechanism of direct transfer from sulfide phase to fluid (Fig. 4) may not be decisive, but it is probably essential for wholesale transfer of Cu together with larger ions including Au, Pd and Pt. This process was proposed to explain the similarity of Au/Cu ratios between sulfides, fluids and bulk ore in some porphyry systems (Halter et al., 2002; Halter et al., 2005). Other deposits where metals ratios differ between magmatic sulfides and final ore show that subsequent selective metal precipitation is equally important (e.g., porphyry Au deposits; Murakami et al., 2010; Rottier et al., 2019). Because of the importance of selective precipitation, the low concentration of Au in some, and of Pt and Pd in most porphyry deposits (Cocker et al., 2015; Park et al., 2021) is not a conclusive argument against their transfer from magmatic sulfides to hydrothermal fluid, given their high solubility in magmatic-hydrothermal fluids (Simon and Pettke, 2009; Sullivan et al., 2022).

## Cu,Ag mass-balance estimation

Published fractionation models have calculated the mass balance of S and chalcophile trace elements such as Cu and Ag between evolving silicate melt, iron sulfide (MSS), sulfide melt and fluid (e.g., Rottier et al., 2019; Yao and Mungall, 2020). Here we explore physical co-transportation of sulfide with the silicate melt, so we estimate the fraction of Cu and Ag

residing in sulfide for a fixed total amount of the trace element (e.g., Cu(total)) and a fixed ratio of sulfide: silicate melt (R-factor) corresponding to 0.2 to 0.5 wt% FeS. Then  $\text{Cu(sulfide)} = \text{Cu(total)} * D * (R+1) / (R+D)$ , where D is the distribution coefficient, e.g.,  $\text{Cu(sulfide)} / \text{Cu(silicate melt)}$  (Campbell and Naldrett, 1979; Richards, 2015). We assume  $D = 400$  for Cu and 60 for Ag, assuming the sulfide is MSS, but values would be higher if some of the sulfide was present as sulfide melt (Li and Audétat, 2012) which would make the process of sulfide entrainment even more effective for chalcophile metal transport. This is a simplified first-order estimation compared to earlier mass-balance modelling that explicitly consider sulfide phase state, sulfide phase composition, and the partitioning of Cu compared to the more chalcophile precious metals (Cocker et al., 2015; Mungall et al., 2015; Yao and Mungall, 2020). However, our estimate presents a limiting case showing that sulfide entrainment can avoid depletion of ore forming components from evolving arc magmas.

### **Comments on Cu in magmatic fluids and possible dispersal to the hydrosphere**

A review of Cu concentrations in natural magmatic fluids exceeds the size limitation of this paper, so a few supplementary references are cited here in support of the speculation that magmatic fluids may contribute significantly to dispersion of Cu from continental magmatic arcs to the hydrosphere. The solubility of Cu, but also of the even more strongly chalcophile trace-elements Au, Pt and Pd is so high at magmatic temperatures (Simon and Pettke, 2009; Sullivan et al., 2022) that all are likely to be highly undersaturated in primary magmatic fluids, which favors their wholesale transfer from decomposing sulfide to fluid (Halter et al., 2005). In natural fluid inclusions, high Cu concentrations are widespread in intermediate-density ('supercritical') fluids of ore-forming as well as barren upper-crustal plutons (Audétat, 2019) including subvolcanic ejecta in arc volcanoes (e.g., Fiedrich et al., 2020). Cu contents approaching percent levels are observed in vapor inclusions of volcanic phenocrysts (Lowenstern et al., 1991; Zajacz and Halter, 2009). Hot volcanic fumaroles are commonly metal-rich and were previously proposed to make a significant contribution to global S and Cu flux to atmosphere and hydrosphere (Nadeau et al., 2010; Wallace and Edmonds, 2011; Edmonds et al., 2018). Submarine volcanics and oceanic arcs under significant seawater pressure have a better chance to preserve magmatic sulfide particles even in the glassy matrix of quenched volcanics, compared to subaerial volcanics (Jenner et al., 2010). For example, Li et al. (2019) reported relict magmatic sulfides in dredged dacites and more primitive enclaves and cumulates of the Okinawa back-arc trough and linked their partial composition to the formation of hydrothermal sulfides in black smoker deposits.

Our thermodynamic calculations imply that the expulsion of S and chalcophile metals by hydrous sulfide-saturated magmas is most efficient from intrusions crystallizing at some depth in the upper crust (~ 3 - 10 km), in regions of thick continental crust that are most likely to promote earlier fractionation to high water content (Loucks, 2021). It should be noted that only a small fraction of their hydrothermal Cu is focussed into rare porphyry copper deposits, which themselves are geologically short-lived copper accumulations that are typically recycled by weathering and erosion within ~ 100 Ma (Wilkinson and Kesler, 2009). By far the greatest part of hydrothermal metals will never be concentrated but dispersed into deep groundwater and basement brines, allowing the possibility that a

significant fraction of chalcophile trace metals might become recycled via hydrosphere and oceanic sediments that are eventually subducted.

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