**Supplemental Data Table S2.** Orientations of Principal Axes of the Best-fit Strain Ellipsoid (with statistics) and ellipticity ratios and orientations on the bedding plane.

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| **Sample** | **Province** | **Interval** | **Fm** | **Bedding** | **“X-Axis”** | | | | **“Y-Axis”** | | | | **“Z-Axis”** | | | | **Bedding Plane** | |
| **Dip Dir, Dip** | **Trend** | **Plunge** | **95% Error Angle** | **Axis Length** | **Trend** | **Plunge** | **95% Error Angle** | **Axis Length** | **Trend** | **Plunge** | **95% Error**  **Angle** | **Axis Length** | **Rs** | **** |
| 15-19 | GV | 16 | Om | 325, 85 | 249 | 38 | 57 | 0.879 | 111 | 44 | 59 | 0.797 | 358 | 22 | 23 | 0.736 | 1.14 | -42.16 |
| 15-15 | V&R | 16 | Db | 144, 80 | 067 | 15 | 14 | 0.890 | 303 | 64 | 15 | 0.862 | 163 | 20 | 05 | 0.767 | 1.07 | -25.60 |
| 15-13 | V&R | 16 | Dmt | 144, 15 | 039 | 36 | 83 | 0.740 | 199 | 52 | 82 | 0.724 | 302 | 10 | 11 | 0.686 | 1.06 | 19.74 |
| 15-12 | V&R | 16 | Ojo | 136, 54 | 073 | 03 | 16 | 0.782 | 166 | 45 | 05 | 0.745 | 340 | 45 | 17 | 0.708 | 1.04 | -16.66 |
| 15-11 | V&R | 16 | Ojo | 135, 60 | 121 | 41 | 12 | 0.762 | 317 | 48 | 12 | 0.738 | 218 | 08 | 04 | 0.697 | 1.09 | -79.37 |
| 15-20 | V&R | 16 | Dmt | 153, 34 | 022 | 08 | 72 | 0.809 | 267 | 72 | 48 | 0.728 | 114 | 16 | 51 | 0.692 | 1.13 | -34.08 |
| 15-25 | V&R | 15 | DSkt | 140, 35 | 085 | 13 | 40 | 0.810 | 201 | 62 | 40 | 0.793 | 349 | 24 | 07 | 0.732 | 1.05 | -42.64 |
| 15-26 | V&R | 15 | St | 128, 14 | 220 | 00 | 34 | 0.843 | 310 | 86 | 35 | 0.772 | 130 | 04 | 11 | 0.738 | 1.14 | -1.97 |
| 15-27 | V&R | 15 | St | 321, 18 | 270 | 26 | 88 | 0.746 | 144 | 50 | 86 | 0.720 | 015 | 28 | 19 | 0.680 | 1.09 | -46.60 |
| 15-29 | V&R | 14 | Dch | 302, 78 | 199 | 14 | 35 | 0.751 | 306 | 50 | 35 | 0.730 | 098 | 37 | 08 | 0.695 | 1.04 | -20.55 |
| 15-30 | V&R | 14 | Dhs | 295, 55 | 044 | 05 | 37 | 0.748 | 290 | 78 | 37 | 0.732 | 135 | 11 | 08 | 0.696 | 1.03 | -28.16 |
| 15-32 | V&R | 14 | Dch | 125, 70 | 055 | 20 | 21 | 0.790 | 294 | 55 | 24 | 0.781 | 156 | 28 | 15 | 0.741 | 1.05 | -6.64 |
| 15-33 | V&R | 14 | Dch | 307, 27 | 071 | 14 | 44 | 0.833 | 176 | 46 | 29 | 0.742 | 329 | 40 | 52 | 0.717 | 1.13 | -22.60 |
| 15-34 | V&R | 14 | Dch | 306, 52 | 274 | 20 | 25 | 0.822 | 062 | 67 | 34 | 0.817 | 180 | 11 | 40 | 0.763 | 1.05 | -74.04 |
| 15-10 | V&R | 14 | Dhs | 102, 24 | 034 | 15 | 27 | 0.775 | 285 | 51 | 27 | 0.757 | 135 | 35 | 02 | 0.718 | 1.08 | -26.88 |
| 15-9 | V&R | 14 | Dhs | 145, 20 | 265 | 14 | 52 | 0.804 | 061 | 75 | 52 | 0.754 | 174 | 06 | 08 | 0.675 | 1.17 | -27.48 |
| 15-8 | V&R | 14 | Dhs | 155, 20 | 077 | 17 | 52 | 0.775 | 184 | 44 | 53 | 0.745 | 331 | 41 | 12 | 0.700 | 1.05 | -10.53 |
| 15-7 | V&R | 14 | Dch | 204, 07 | 219 | 25 | 14 | 0.794 | 033 | 65 | 09 | 0.780 | 128 | 02 | 14 | 0.675 | 1.17 | 75.88 |
| 15-4 | V&R | 14 | Dhs | 195, 10 | 236 | 04 | 60 | 0.819 | 020 | 85 | 13 | 0.753 | 146 | 03 | 59 | 0.704 | 1.16 | 49.13 |
| 15-5 | V&R | 14 | Dhs | 308, 52 | 226 | 38 | 17 | 0.779 | 056 | 52 | 29 | 0.722 | 320 | 05 | 31 | 0.704 | 1.08 | -32.43 |
| 15-2 | V&R | 14 | Dch | 045, 15 | 290 | 03 | 25 | 0.809 | 040 | 81 | 39 | 0.774 | 200 | 08 | 36 | 0.754 | 1.07 | 24.86 |
| 13-24 | V&R | 14 | Dhs | 130, 45 | 060 | 10 | 66 | 0.800 | 164 | 54 | 66 | 0.786 | 323 | 34 | 06 | 0.721 | 1.02 | -27.83 |
| 13-20 | V&R | 14 | Dm | 305, 50 | 230 | 27 | 21 | 0.826 | 089 | 57 | 19 | 0.758 | 329 | 18 | 15 | 0.711 | 1.14 | -28.53 |
| 13-9 | AP | 13 | St | 130, 20 | 212 | 17 | 34 | 0.746 | 078 | 66 | 08 | 0.713 | 307 | 16 | 34 | 0.667 | 1.09 | 8.11 |
| 13-11 | AP | 13 | St | 113, 72 | 067 | 42 | 38 | 0.740 | 262 | 48 | 68 | 0.721 | 164 | 08 | 75 | 0.690 | 1.06 | -62.70 |
| 13-19 | AP | 13 | Mp | 340, 10 | 035 | 12 | 86 | 0.789 | 154 | 66 | 54 | 0.741 | 300 | 20 | 74 | 0.732 | 1.08 | 36.52 |
| 13-5 | AP | 12 | Dhs | 295, 20 | 238 | 02 | 16 | 0.860 | 331 | 56 | 12 | 0.798 | 147 | 34 | 16 | 0.754 | 1.10 | -34.81 |
| 13-4 | AP | 11 | Mg | 290, 15 | 063 | 08 | 10 | 0.801 | 198 | 79 | 02 | 0.750 | 332 | 08 | 10 | 0.700 | 1.14 | -41.02 |
| 13-3 | AP | 11 | Dhs | 305, 09 | 292 | 08 | 30 | 0.791 | 039 | 64 | 09 | 0.741 | 198 | 24 | 29 | 0.710 | 1.10 | -77.27 |
| 13-2 | AP | 10 | Dch | 115,15 | 082 | 07 | 74 | 0.769 | 310 | 80 | 03 | 0.738 | 173 | 08 | 74 | 0.657 | 1.17 | -57.13 |
| 13-8 | AP | 10 | Dch | 290, 40 | 248 | 03 | 07 | 0.830 | 139 | 81 | 01 | 0.772 | 338 | 08 | 07 | 0.672 | 1.20 | -48.57 |
| 15-42 | AP | 9 | \*pv | 078, 14 | 116 | 04 | 22 | 0.758 | 021 | 51 | 21 | 0.741 | 209 | 38 | 04 | 0.692 | 1.06 | 56.38 |
| 15-43 | AP | 8 | \*c | 131, 16 | 247 | 19 | 21 | 0.758 | 017 | 62 | 08 | 0.725 | 150 | 20 | 21 | 0.678 | 1.11 | -18.44 |
| 15-47 | AP | 7 | \*m | 359, 10 | 216 | 17 | 85 | 0.796 | 081 | 67 | 81 | 0.742 | 311 | 16 | 23 | 0.713 | 1.10 | 48.87 |
| 15-46 | AP | 6 | \*m | 051, 06 | 037 | 27 | 11 | 0.772 | 157 | 45 | 22 | 0.714 | 287 | 33 | 20 | 0.695 | 1.09 | -73.03 |
| 15-48 | AP | 5 | \*c | 235, 05 | 083 | 17 | 22 | 0.858 | 185 | 34 | 22 | 0.778 | 331 | 51 | 04 | 0.684 | 1.13 | 73.42 |
| 15-51 | AP | 4 | \*c | 268, 05 | 206 | 48 | 09 | 0.772 | 031 | 42 | 03 | 0.755 | 299 | 03 | 09 | 0.700 | 1.09 | -30.96 |
| 15-52 | AP | 3 | \*m | 058, 03 | 082 | 02 | 25 | 0.791 | 312 | 88 | 01 | 0.683 | 172 | 02 | 25 | 0.645 | 1.23 | 66.08 |
| 15-53 | AP | 2 | \*m | 355, 04 | 079 | 02 | 83 | 0.736 | 175 | 72 | 23 | 0.700 | 348 | 18 | 81 | 0.646 | 1.13 | 6.38 |
| 15-55 | AP | 1 | Pd | 240, 10 | 039 | 19 | 45 | 0.781 | 174 | 64 | 10 | 0.746 | 303 | 17 | 46 | 0.680 | 1.13 | 29.22 |