

**SUPPLEMENTARY MATERIALS FOR:**

**Direct evidence for fluid overpressure during hydrocarbon  
generation and expulsion from organic-rich shales**

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**ADDITIONAL DETAILS ON METHODS**

**Micro-spectrofluorimetry analysis**

Fluid inclusion petrographic analysis carried out by using a Leica DM-2700P  
microscope with transmitted light (TL) and ultra-violet (UV) illumination (365 nm peak of  
Hg). The wavelength of excitation filter used for the fluorescence is from 340 – 380 nm, and  
of suppression filter is 425 nm. Micro-spectrofluorimetry was used to study the liquid  
hydrocarbon phase of individual inclusions under ultra-violet illumination, using a TIDAS  
MSP 400 miniature fibre optic spectrometer. Parameters  $\lambda_{\text{max}}$  (wavelength of maximum  
intensity),  $Q_{(650/500)}$  (the ratio of the intensity at 650 nm to the intensity at 500 nm) and  $Q_{\text{F-535}}$

22 (the ratio of the 535 – 750 nm flux to the 430 – 535 nm flux) were used to determine the  
23 gross compositions of liquid hydrocarbons of entrapped oil and their maturity.

#### 24 **Laser Raman spectroscopic analysis**

25 Raman spectroscopy of organic matter can be used as an indicator of the thermal  
26 maturity. Laser Raman analyses of the median plane and primary bitumen inclusions in  
27 BDPVs were performed on a Bruker SENTERRA spectrometer and a 532 nm Ar-ion laser  
28 focused to a 1  $\mu\text{m}$  spot through a 100x objective mounted on a petrographic microscope at  
29 MacEwan University (Edmonton, AB). All spectra were acquired using a laser power of 20  
30 mW and two to three, 5-10s exposures summed to the final reported spectra. A silicon wafer  
31 was used for wavenumber calibration. The Raman spectra were acquired and processed by  
32 using the LabSpec 5 software by HORIBA. Linear baseline subtraction was performed on a  
33 spectra truncated between 1100 and 1800  $\text{cm}^{-1}$  (Fig. DR1A). Following this processing, D1-,  
34 D2-, D3-, D4- and G-bands (Fig. DR1B) were fitted by a decomposition using  
35 Gaussian-Lorentzian peak shapes, following the procedure described by Sforza et al. (2014).  
36 Peak positions, intensities, areas and widths of each band was recorded. Raman spectra have  
37 been widely used as proxies to estimate the peak temperatures and thermal maturities  
38 experienced by organic matter (Liu et al., 2013; Wilkins et al., 2014; Kouketsu et al., 2014;  
39 Schito et al., 2017). In light of the known geological context of our study area, we applied the  
40 thermometer established by Kouketsu et al. (2014) based on full width at half maximum of  
41 D1-band (FWHM-D1, Eq. 1). Previous testing by Baludikay et al. (2018) has shown that this  
42 empirical model provides the best performance for the conditions of diagenesis (i.e., < 200  
43  $^{\circ}\text{C}$ ).

44 
$$T (^{\circ}\text{C}) = -2.15 * \text{FWHM-D1} + 478. \quad (1)$$

45 **Microthermometry of fluid inclusions**

46 Microthermometric studies of fluid inclusions were carried out by using a Linkam  
47 THMSG600 heating-cooling stage with temperature calibrated according to the triple point of  
48 H<sub>2</sub>O (0.0 °C) and the critical point of H<sub>2</sub>O (374.1 °C) using synthetic pure H<sub>2</sub>O fluid  
49 inclusion, and the triple point of CO<sub>2</sub> (-56.6 °C) using synthetic CO<sub>2</sub> fluid inclusions. For the  
50 inclusions measured here, we always conducted the heating measurements (analysis of  
51 homogenization temperature,  $T_h$ ) prior to cooling the samples, because the volume fraction of  
52 vapor in the aqueous inclusions was small and freezing could have induced stretching, which  
53 would affect the measured  $T_h$ . Thus, by heating prior to cooling, we were able to confidently  
54 measure unmodified  $T_h$ , and determine salinity thereafter by subsequent freezing. During  
55 heating from room temperature, both the two-phase hydrocarbon and aqueous inclusions  
56 homogenized to liquid. The homogenization temperatures of fluid inclusions in each FIA  
57 were obtained by thermal cycling using temperature steps of 1°C as described by Goldstein  
58 and Reynolds (1994). For the monophasic hydrocarbon inclusions, all inclusions nucleated a  
59 gas bubble when temperature reached approximately -60 °C during cooling. After nucleation,  
60 the inclusions were re-heated to measure the homogenization temperature. Final ice melting  
61 temperatures of aqueous inclusions were obtained after freezing using temperature steps of  
62 1°C. The precision of the microthermometry is estimated to be  $\pm 0.1^{\circ}\text{C}$  over the entire  
63 temperature range.

64 **PVT modeling**

65           The compositions of the petroleum inclusions were acquired on populations of  
66   inclusions by crushing the samples, and analyzing the resulting leachates by chromatography  
67   and mass spectrometry (Table DR1). The volume fraction of vapor of the two-phase  
68   hydrocarbon inclusions at room temperature were estimated by optical microscopy as  
69   described by Roedder (1984), and by digital image analysis. Only the inclusions with regular  
70   and equilateral shapes were selected for estimation of the volume fraction of vapor.

71           The thermodynamic calculations of fluid phase equilibria and isochore for  
72   hydrocarbon inclusions was done using the Peng-Robinson equation of state as implemented  
73   in the computer program *PVTsim*. The input parameters in these calculations were 1) the  
74   hydrocarbon compositions acquired on populations by crush/leach analysis, and 2) the  
75   homogenization temperatures of the 5 samples. In these calculations, we followed the method  
76   of Aplin et al. (1999). Specifically, we used the *PVTsim* software to calculate the saturation  
77   pressure at the homogenization temperature of the inclusion, and then calculated the total  
78   molar volume at the pressure-temperature point of homogenization. The calculated  
79   (theoretical) volume fraction of vapor at room temperature was obtained by calculating the  
80   conditions at which the molar volume of the mixture at room temperature matched the molar  
81   volume calculated at the homogenization temperature. Thus, the representativeness  
82   (accuracy) of the measured petroleum composition (measured based on populations, and now  
83   compared to the petroleum composition within each individual inclusion) was verified by  
84   comparison of the calculated volume fraction of vapor and the measured values obtained by  
85   optical microscopy and image analysis.

86 Methane is the most soluble hydrocarbon component in the aqueous phase coexisting  
87 with oil phase, and even minor concentrations of CH<sub>4</sub> in the aqueous inclusions can greatly  
88 influence PVT interpretation (Dubessy et al., 2001; Caumon et al., 2014). However, as  
89 described below, no CH<sub>4</sub> was detected in the aqueous inclusions by Raman analysis (Fig.  
90 DR4). Hence the PVT properties of the aqueous inclusions were modeled based on the  
91 H<sub>2</sub>O-NaCl system. The thermodynamic calculations of phase equilibria and isochore of the  
92 aqueous inclusions were based on the model of Steele-MacInnis et al. (2012), with input  
93 parameters of ice melting temperatures and the homogenization temperatures. To determine  
94 the trapping pressure, we used the approach of intersecting isochores of coexisting petroleum  
95 and aqueous inclusions (Goldstein, 2001).

## 96 **Basin modeling**

97 Basin modeling of Well NY-1 was conducted using the *Basinmod 1D* software. Input  
98 parameters in this modeling were: the strata top depth; stratigraphic present thickness;  
99 absolute ages; lithology; missing erosional thickness; surface temperature; measured borehole  
100 temperatures (BHT); and heat flux during each stage. Modeling based on these parameters  
101 was done to generate the standard burial history of the well. A summary of the information  
102 upon which this parameterization was based is as follows.

103 The Bohai Bay Basin is located in East China (Fig. 1A), and represents a  
104 faulted-depressed basin developed in the Paleozoic cratonic basement, filled by  
105 Mesozoic-Cenozoic strata. The Cenozoic strata of the Dongying Depression comprise the  
106 Eocene Kongdian Formation (Ek), Eocene Shahejie Formation (Es), Eocene Dongying  
107 Formation (Ed), Neogene Guantao Formation (Ng), Neogene Minghuazhen Formation (Nm)

and the Quaternary Pingyuan Formation (Qp), respectively from bottom to top (Fig. 1B). The tectonic evolution of the basin consists of the syn-rifting stage (65.0-24.6 Ma, during the deposition stage of the Kongdian, Shahejie and Dongying Formations) and post-rifting stage (24.6 Ma to the present, during the deposition stage of Guantao, Minghuazhen and Pingyuan Formations). The syn-rifting stage occurred from the Palaeocene to the Oligocene and can be subdivided into 4 episodes including an initial episode (I), an expansion episode (II), an expansion and rapid subsiding episode (III), and a contraction episode (IV) (Chang, 1991; Xie et al., 2001). A subsequent period of uplift and erosion followed the deposition of the Dongying Formation from 24.6 to 14 Ma, and the contact with the overlying Guantao Formation is a regional unconformity in the study area (Guo et al., 2014).

The data we used for the basin modelling are presented in the Table DR4. The input information about the strata top depth, the present thickness, the lithology and the missing erosional thickness of the Well NY-1 was acquired from the well log profile from Shengli Oil Company, SINOPEC. The current heat flux was calculated based on the measured BHT, with the result of  $67.3 \text{ mW/m}^2$ , using the transient heat flux model in the software. The values of the paleo heat flux during the deposition of each formation were from Guo et al. (2012) and Qiu et al. (2014) in the Bohai Bay Basin, from which a good agreement between the measured and calculated Ro and temperature has been verified. An average surface temperature was set at  $15^\circ\text{C}$  for the entire geological time in the modelling (Guo et al., 2012; Qiu et al., 2014). The initial porosity, matrix density, matrix thermal conductivity and matrix heat capacity were adopted from the default values in the *Basinmod 1D* software.

After completion of the basin model, the time dependent litho- and hydro-static regimes of the five samples were then deduced from the basin model following the procedures outlined by Bourdet et al. (2010) and Renard et al. (2019). The modelling provides a reconstruction of the pressure-temperature-time trajectory under both hydrostatic and lithostatic regimes throughout the basin evolution. The resulting trajectory in PT space is related to the evolving heat flow, sedimentation and compaction rates through time. Combined with the fluid inclusion data plotted in the same graph, this provides an assessment of the relationship between fluid pressure versus hydrostatic and lithostatic pressures at the time when the fluid inclusions were trapped (Fig. 4 and DR5).

## **ADDITIONAL DETAILS ON RESULTS**

The two-phase hydrocarbon inclusions consist of both a hydrocarbon liquid phase with various UV-fluorescence colors (yellow, yellow-green, green) and a non-luminescent hydrocarbon gas phase (Figs. DR2). The inclusions in any individual FIA show consistent fluorescence colors. In most cases fluorescence of petroleum is used to give a fingerprint of the composition of hydrocarbons and different fluorescence colors indicate variable compositions and maturities of the oil inclusions. Thus, the parameters deduced from the micro-spectrofluorimetry are very sensitive to the chemical compositions and API (American Petroleum Institute) gravity of hydrocarbon in inclusions (Stasiuk and Snowdon, 1997; Bourdet et al., 2014; Nandakumar and Jayanthi, 2016). As for the micro-spectrofluorimetry results, the yellow fluorescence color have relatively high value of  $\lambda_{\max}$  (avg. = 568 nm),  $Q_{(650/500)}$  (avg. = 0.71) and  $Q_{F-535}$  (avg. = 1.99), the yellow-green fluorescence colors exhibit

lower  $\lambda_{\max}$  (avg. = 536 nm),  $Q_{(650/500)}$  (avg. = 0.51) and  $Q_{F-535}$  (avg. = 1.38), while the green fluorescence colors show the lowest  $\lambda_{\max}$  (avg. = 511 nm),  $Q_{(650/500)}$  (avg. = 0.39) and  $Q_{F-535}$  (avg. = 1.09) (Fig. DR2; Table DR2). From yellow to green fluorescence, the heavy components (heterocompounds and aromatic hydrocarbons fraction) decrease, whereas the light components (saturated hydrocarbons fraction) increase with the green fluorescent color indicative of relatively high maturity (Hagemann and Hollerbach, 1986; Munz, 2000). In addition, the spectral shape (Fig. DR2) and the fluorescence parameters (Table DR2) of the individual petroleum inclusions that make up a given FIA are very consistent along the direction of the fiber growth. Thus, the gross degree of maturity of the hydrocarbon fluids in these veins is relatively low, and the liquid hydrocarbon composition remained consistent during the BPFVs growth.

Two types of bitumen-bearing inclusions are present in veins. The first is characterized by bitumen which coats the wall of the inclusions with the weak fluorescence intensity (Fig. 3A). The second type coexists with petroleum inclusions within the same FIAs and is difficult to differentiate from monophasic aqueous inclusions, based solely on petrography. However, Raman spectra of this second type of inclusions show a strong feature at around  $1600\text{ cm}^{-1}$  and a weaker feature at around  $1360\text{ cm}^{-1}$  (Fig. 3B), which indicates that these are bitumen inclusions. The formation temperatures of these primary monophasic bitumen inclusions based on Raman geothermometers range from 133.2 to 157.2 °C (avg. = 145.7 °C), which generally overlap with, but extend to slight higher values than the median planes (130.6 to 141.0 °C; avg. = 133.6 °C; Table DR3). This generally suggests that, from the median plane to the vein wall (i.e., along the direction of antitaxial growth) in BPFVs, the



temperatures were rising due to the increasing burial depth during the hydrocarbon generation and expulsion from organic-rich shales.

Verification of the representativeness of the (bulk) composition data used for the thermodynamic calculations of the two-phase hydrocarbon inclusions was as follows. The estimated volume fractions of vapor of the selected hydrocarbon inclusions in five samples, based on optical microscopy and image analysis, were from 5 to 10%. The values obtained from the thermodynamic calculations of the five samples, from shallow to deep, were 7.7-10.2%, 6.8-9.4%, 7.4-9.1%, 6.9-11.8% and 7.4-9.4%, respectively. Thus, the calculated volume fractions of vapor at room temperature matched the estimated values, suggesting the petroleum composition data acquired on populations of inclusions in the five samples are accurate representations of the petroleum within the individual inclusions in each sample. In addition, as we mentioned above, the HIs within any individual FIA show consistent fluorescence colors and nearly uniform micro-spectrofluorimetry parameters, which also indicate that the chemical compositions of the HIs are uniform within each FIA during the fiber growth.

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**DATA REPOSITORY FIGURES**

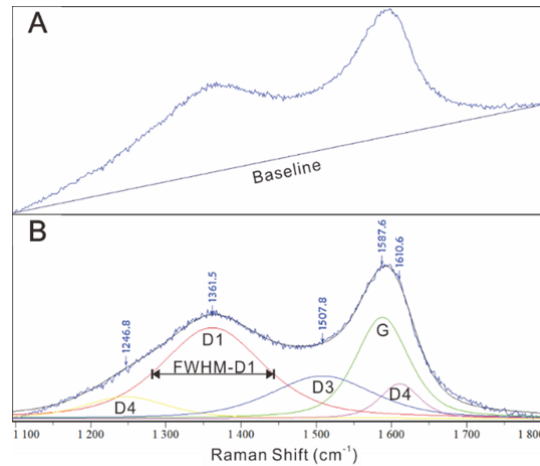


Figure DR1. A: Baseline subtraction of the Raman spectra of bitumen using a third order polynomial curve fit. B: Decomposition of the Raman spectra of bitumen. FWHM-D1 = full widths at half mean for a D1-band.

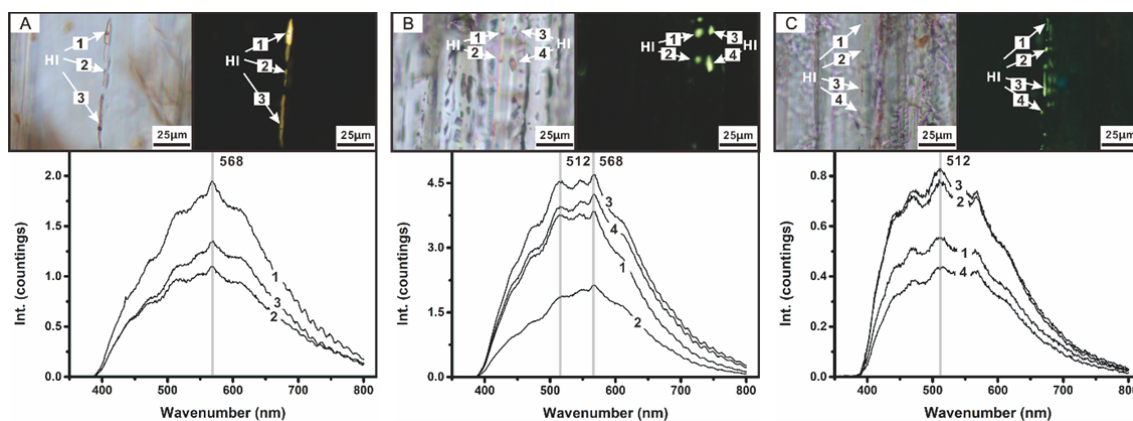


Figure DR2. Fluid inclusions hosted in BPFVs of Well NY-1 and micro-spectrofluorimetry.

HI = Hydrocarbon inclusion. A: From 3296.0 m, hydrocarbon inclusions in one FIA showing yellow fluorescence color and their micro-spectrofluorimetry features. B: From 3432.0 m, hydrocarbon inclusions in one FIA showing yellow-green fluorescence color and their micro-spectrofluorimetry features. C: From 3426.0 m, hydrocarbon inclusions in one FIA showing green fluorescence color and their micro-spectrofluorimetry features.

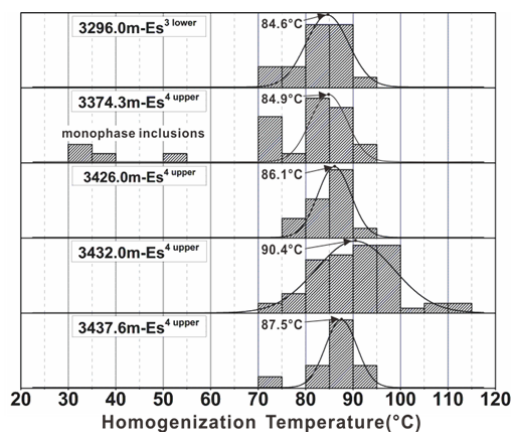
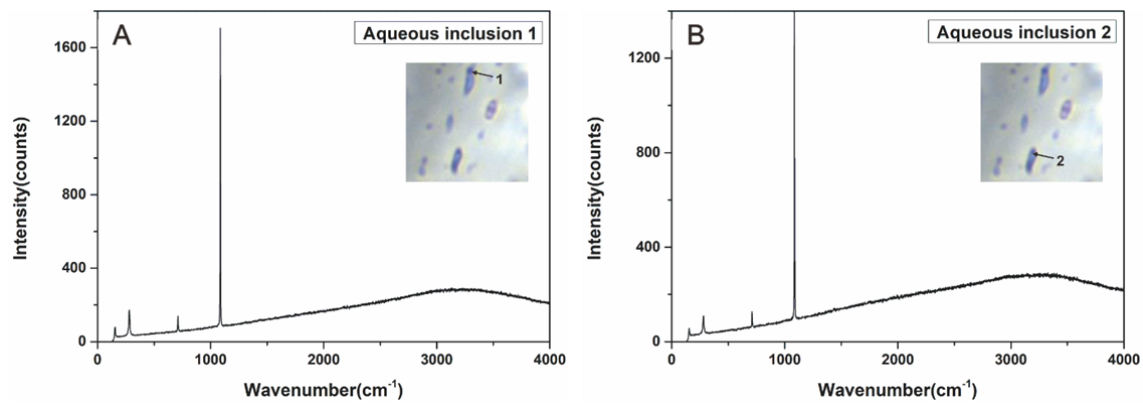


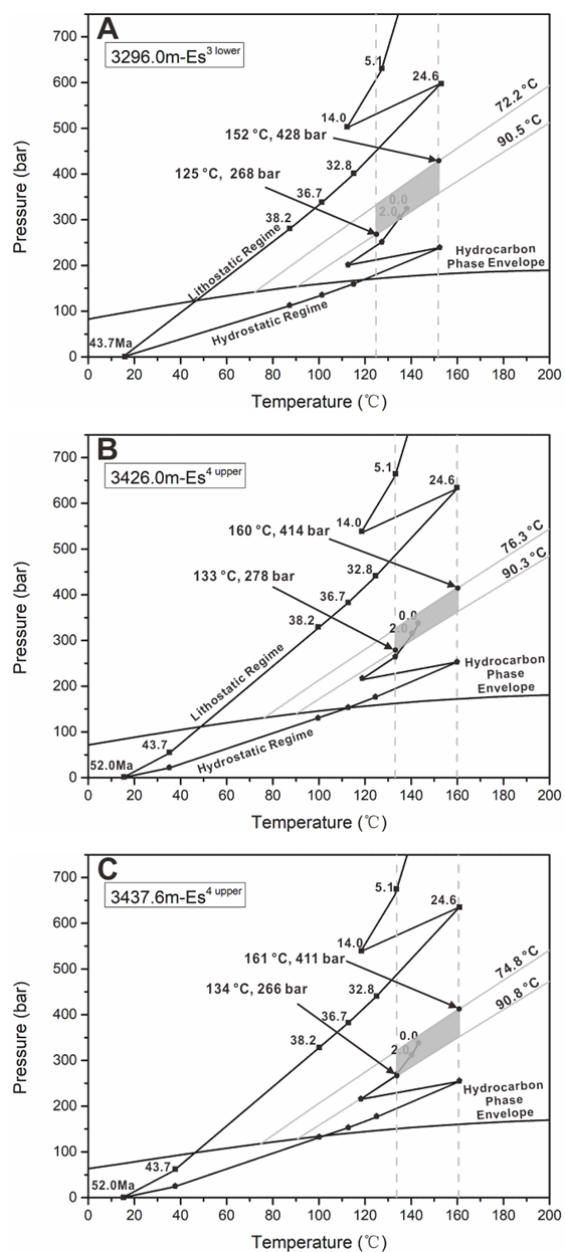
Figure DR3. Distribution histogram and Gaussian fit of hydrocarbon inclusions homogenization temperatures in BPFVs of 5 different burial-depths.



257

258 Figure DR4. Raman spectra of vapor phase within two-phase aqueous inclusions in the

259 sample of 3432.0 m.



260

261 Figure DR5. P-T diagram showing intersecting isochore of two-phase hydrocarbon inclusions

262 with the inferred trapping temperatures based on the burial history. The shaded area

263 illustrates the proposed entrapment conditions of the fluid inclusions during the BPFV

264 formation. A: From 3296.0 m. B: From 3426.0 m. C: From 3437.6 m.

265

266 **DATA REPOSITORY TABLES**

267 Table DR1. Hydrocarbon compositions of the five samples of Well NY-1

<b>Compositions (mol. %)</b>	<b>3296.0 (m)</b>	<b>3374.3 (m)</b>	<b>3426.0 (m)</b>	<b>3432.0 (m)</b>	<b>3437.6 (m)</b>
C <sub>1</sub>	45.1	38.6	40.8	35.3	36.2
C <sub>2</sub>	11.4	16.1	17.3	21.4	18.5
C <sub>3</sub>	7.3	8.2	6.8	8.6	10.2
C <sub>4</sub>	4.0	3.9	3.1	3.4	4.0
C <sub>5</sub>	1.6	1.8	1.3	1.0	1.0
C <sub>6</sub>	0.4	0.9	0.6	0.3	0.2
C <sub>7+</sub>	30.1	30.4	30.2	30.1	30.0

268 Table DR2. Homogenization temperature values and micro-spectrofluorimetry parameters of  
269 the inclusions in BPFVs of Well NY-1

<b>Depth (m)</b>	<b>FIA</b>	<b>Type</b>	<b>Fluorescence Colour</b>	<b>T<sub>h</sub>/T<sub>m</sub> (°C)</b>	<b>λ<sub>max</sub></b>	<b>Q<sub>(650/500)</sub></b>	<b>Q<sub>F-535</sub></b>
3296	1	FI	Yell.	82.8	568	0.85	1.99
	2	FI	Yell.	77.2			
		FI	Yell.	83.5			
		FI	Yell.	72.2			
		FI	Yell.	79.1	568	0.83	2.06
	3	FI	Yell.	81.3	567	0.82	1.98
		FI	Yell.	85.6	569	0.81	2.08
		FI	Yell.	74.9			
		FI	Yell.-Gre.	86	566	0.49	1.42
	4	FI	Yell.-Gre.	86.5			
		FI	Yell.-Gre.	86.5			
		FI	Yell.-Gre.	87.5			
		FI	Yell.-Gre.	83.9			
		FI	Yell.-Gre.	84.4			
		FI	Yell.-Gre.	89			
		FI	Yell.-Gre.	90.5			
		FI	Yell.-Gre.	84.3			
3374.3	1	FI	Yell.	88.1			
		FI	Yell.	90.3	568	0.80	1.82
		FI	Yell.	86.1			
		FI	Yell.	90.6			
		FI	Yell.	86.1			
		FI	Yell.	89.8			
	2	FI	Yell.	74.9			
		FI	Gre.	74.9			
	3	FI	Yell.	80.9			



		FI	Yell.	84.5	568	0.88	2.17
		FI	Yell.	84.5			
		FI	Yell.	86.2			
		FI	Yell.	82.8	570	0.91	2.15
	4	FI	Yell.	85.8			
		FI	Yell.	84.4			
		FI	Yell.	83.9			
		FI	Yell.-Gre.	36.7			
	5	FI	Yell.-Gre.	32.3			
		FI	Yell.-Gre.	34.6	568	0.59	1.60
		FI	Yell.-Gre.	53.8			
	6	FI	Yell.	73.4	566	0.71	1.83
		FI	Yell.	70.2			
		FI	Yell.	80.1	568	0.84	2.04
	7	FI	Yell.	74.3			
		FI	Yell.	78.3			
3426	1	FI	Yell.	76.3			
		FI	Yell.	79.1	567	0.82	1.92
		FI	Yell.	88.1			
		FI	Yell.	87.8			
		FI	Yell.	84.4			
	2	FI	Yell.	84.4			
		FI	Yell.	85.3			
		FI	Yell.	85.4			
		FI	Yell.	82.4			
	3	FI	Yell.-Gre.	80.9	511	0.42	1.20
		FI	Gre.	89.5	512	0.40	1.13
		FI	Gre.	89.1	509	0.43	1.13
	4	FI	Gre.	90.3	510	0.43	1.15
		FI	Gre.	88.3	512	0.47	1.18
3432		FI	Yell.-Gre.	88.3			
		FI	Yell.-Gre.	76.8			
		FI	Yell.-Gre.	75.5			
	1	FI	Yell.-Gre.	75.5			
		FI	Yell.-Gre.	83.6			
		FI	Yell.-Gre.	71.7			
		FI	Yell.-Gre.	71.7			
		FI	Gre.	91.7			
		FI	Gre.	84.6			
	2	FI	Gre.	88.8			
		FI	Gre.	85.8			
		FI	Gre.	84.6			
		FI	Gre.	84.6			
		FI	Gre.	84.6			

3	FI	Gre.	83.3	509	0.43	1.13
	FI	Gre.	93.4			
	FI	Gre.	83.2			
	FI	Gre.	86.9			
4	FI	Yell.-Gre.	84.6	514	0.54	1.37
	FI	Yell.-Gre.	95.8			
	FI	Yell.-Gre.	86.4			
	FI	Yell.-Gre.	80.6			
	FI	Yell.-Gre.	80.6			
	FI	Yell.-Gre.	88			
	FI	Yell.-Gre.	93.8			
	FI	Yell.-Gre.	95.9			
	FI	Yell.-Gre.	92			
	FI	Yell.-Gre.	97.3			
5	FI	Yell.-Gre.	96.9	514	0.49	1.31
	FI	Yell.-Gre.	94.5			
	FI	Yell.-Gre.	95.3			
	FI	Yell.-Gre.	99.9			
	FI	Yell.-Gre.	95.3			
	FI	Yell.-Gre.	97.4			
	FI	Yell.-Gre.	96.2			
	FI	Yell.-Gre.	97.4			
	FI	Yell.-Gre.	97.4			
	FI	Yell.-Gre.	93.8			
	FI	Gre.	80.3			
	FI	Gre.	80.3			
	FI	Yell.-Gre.	89.1			
	FI	Yell.-Gre.	91.5			
7	FI	Yell.-Gre.	90.8	568	0.63	1.66
	FI	Yell.-Gre.	94.5			
	FI	Yell.-Gre.	91.1			
8	AI		142.4/-22.7	567	0.58	1.54
	AI		142.4/-23.5			
	AI		134.1/-23.3			
	AI		140.2/-23.8			
	AI		125.2/-22.7			
	AI		125.2/-21.9			
	AI		139.5/-22.1			
	FI	Yell.-Gre.	111.3			
	FI	Yell.-Gre.	111.3			
	FI	Yell.-Gre.	85.2			
	FI	Yell.-Gre.	89.6			
	FI	Yell.-Gre.	107.3			

		FI	Yell.-Gre.	96.8			
		FI	Yell.-Gre.	97.2			
	9	FI	Yell.-Gre.	106.5			
		FI	Yell.-Gre.	95.3			
		FI	Yell.-Gre.	100.3			
		FI	Yell.-Gre.	88.6			
		FI	Yell.-Gre.	86.9			
		FI	Yell.-Gre.	93.4			
	10	FI	Yell.-Gre.	93.4			
		FI	Yell.-Gre.	91.8			
		FI	Yell.-Gre.	78.9			
		FI	Yell.-Gre.	89.1			
		FI	Yell.-Gre.	91.8			
	1	FI	Yell.-Gre.	74.8			
		FI	Gre.	81.3	509	0.35	1.03
		FI	Gre.	86.8			
	2	FI	Gre.	86.8			
		FI	Gre.	86.4			
3734.6		FI	Gre.	83.9			
		FI	Yell.-Gre.	87.6			
		FI	Yell.-Gre.	90.8			
	3	FI	Yell.-Gre.	90.4	510	0.45	1.13
		FI	Yell.-Gre.	87.3			
		FI	Yell.-Gre.	89.3			

270 Table DR3. Raman geothermometers of bitumen in the BPFVs from 3432.0 m

Sample	Position-D1 (cm <sup>-1</sup> )	FWHM-D1 (cm <sup>-1</sup> )	T (FWHM-D1) (°C)
	1361.5	160.9	132.0
Median Plane	1366.1	156.7	141.0
	1358.8	161.6	130.6
	1364.1	161.5	130.8
	1353.1	158.7	136.7
	1349.2	160.4	133.2
	1351.1	156.9	140.6
	1345.9	157.5	139.4
Primary bitumen inclusions	1356.4	158.5	137.2
	1360.3	149.4	156.8
	1357.7	152.1	151.0
	1353.8	153.1	148.8
	1358.4	149.2	157.2
	1360.1	149.5	156.7

271 Table DR4. The strata top depth, stratigraphic present thickness, begin ages, the missing

272 erosion thickness and the heat flux of each formation of Well NY-1

<b>Formation</b>	<b>Begin age (Ma)</b>	<b>Top depth (m)</b>	<b>Present thickness (m)</b>	<b>Missing thickness (m)</b>	<b>Heat flux (mW/m<sup>2</sup>)</b>
Q	2	0	300		69
Nm	5.1	300	751		71
Ng	14	1051	471		72.5
Erosion	24.6			-400	84.5
Ed	32.8	1522	564		85.5
Es <sup>1</sup>	36.7	2086	212		86.5
Es <sup>2</sup>	38.2	2298	196.5		87
Es <sup>3</sup> upper	38.6	2494.5	290.5		88
Es <sup>3</sup> middle	42	2785	403		87.5
Es <sup>3</sup> lower	43.7	3188	127.98		86.5
Es <sup>4</sup> upper	45	3315.98	222.02		85
Es <sup>4</sup> below	52	3538	200		84

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