

1 Supplementary data

2 MATERIALS AND METHODS

3 **Starting Materials**

4 Starting materials were prepared from analytical MgO, SiO<sub>2</sub>, MgF<sub>2</sub> and Mg(OH)<sub>2</sub>. To release absorbed  
5 water and unwanted hydroxide components, the MgO starting material was fired in a Pt-crucible at  
6 1000°C for at least 2 h. The starting materials were ground in an agate mortar under acetone (>1 h)  
7 to obtain homogenous fine grained mixtures. All starting materials including the fired MgO were  
8 stored in a drying furnace at >110°C to prevent the mixtures from absorbing moisture.

9 **Experimental techniques**

10 All experiments were performed in sealed 2 mm O.D. Pt-capsules to prevent volatile loss. In our low  
11 pressure experiments, F partially volatilizes and forms a gas phase which reduces the F activity in the  
12 melt and causes excess MgO in the melts (Hinz & Knuth, 1960). Two experiments were conducted at  
13 atmospheric pressure (1 atm) in a vertical gas-mixing furnace (Gero GmbH, Germany) at  
14 temperatures between 1350-1500°C (Table DR1). Experiments at pressures between 0.5 -2 GPa and  
15 at 1350°C<T<1600°C were conducted in Boyd & England type piston cylinder apparatus at Münster  
16 University. The ½ inch piston cylinder assemblies consisted of concentric cylinders of talc, Duran®  
17 glass, a thin graphite heater (Ringsdorff®), and a 4 mm diameter inner cylinder made from crushable  
18 alumina. The temperatures were monitored with a W<sub>97</sub>Re<sub>3</sub>-W<sub>75</sub>Re<sub>25</sub> thermocouple and controlled by  
19 a Eurotherm™-controller. The temperatures were accurate within 10°C. The pressure assemblies  
20 were calibrated using the quartz–coesite transition (Bose & Ganguly, 1995) and the MgCr<sub>2</sub>O<sub>4</sub>+SiO<sub>2</sub> =

21  $\text{MgSiO}_3 + \text{Cr}_2\text{O}_3$  reaction (Klemme & O'Neill, 1997). Based on our pressure calibration, the quoted  
22 pressures are estimated to be accurate within 0.1 GPa.

23 Experiments at pressures between 5 GPa and 19 GPa were run in a 1000 t Walker-type (Walker *et al.*,  
24 1990) multi-anvil apparatus at Münster University. Experiments from 5 to 8 GPa were performed  
25 with 14/8 assemblies, experiments at 17 and 19 GPa with 10/4 assemblies. The 14/8 and 10/4  
26 notation refers to octahedra size and truncated edge lengths in mm. All multi-anvil assemblies  
27 consist of Cr-bearing MgO octahedra, stepped  $\text{LaCrO}_3$  heaters and pyrophyllite gaskets  
28 (Wonderstone Ltd). The starting materials were sealed in Pt capsules, encapsulated into crushable  
29  $\text{Al}_2\text{O}_3$  containers and finally placed in the center of the furnace. We used one 1.6 mm O.D. Pt-capsule  
30 with a length of about 2.7 mm in the 14/8 assemblies and two 1.2 mm O.D. Pt-capsules with a length  
31 of 1.2 mm for the 10/4 assemblies. Temperatures were measured with  $\text{W}_{97}\text{Re}_3$ - $\text{W}_{75}\text{Re}_{25}$   
32 thermocouples and were inserted on top of the capsules (for the 14/8 assemblies) or centered  
33 between the two capsules (for 10/4 assemblies). First, the pressure was applied using a computer-  
34 controlled system and subsequently experiments were heated up fast with about 300°C/min and  
35 then kept constant for 1-5 h (Table DR1). Temperatures were controlled by a Eurotherm™ 2404 -  
36 controller. The temperatures measured at the thermocouples were accurate within 10°C. All  
37 experiments were quenched rapidly by turning off the power supply. Temperature fell from the run  
38 temperature to below 500°C in less than 1 s.

39 Run M-92 at 17 GPa and 1900°C seems to violate Gibb's phase rule. This is caused by a large  
40 temperature gradient of about 100 °C in this particular experiment and is a common challenge in the  
41 most very high temperature multi anvil experiments (Stewart *et al.*, 2007; Leinenweber *et al.*, 2012).  
42 As the thermocouple is located in the center of the 10/4 assembly between two capsules, the  
43 measured temperature defines the upper limit of the T gradient. The characterization of the run with  
44 SEM imaging analyses confirms that the humite group minerals are concentrated at the cold end of  
45 the capsule, whereas forsterite, enstatite and melt are concentrated at the hot end of the capsule.  
46 Temperature gradients might also explain the small number of clinohumites found in run M-117,

47 which are only located at the cold end of the capsule and are, therefore, not be stable at the nominal  
48 run temperature of 1700°C.

## 49 **Analytical Methods**

50 The experimental run products were characterized first by optical microscopy, followed by scanning  
51 electron microscopy, using JEOL 6610LV scanning electron microscope which is equipped with an EDX  
52 detector (Fig. DR1). To quantify major element concentrations of the experimental products, a JEOL  
53 JXA 8900 electron microprobe (EPMA) was used (Table DR2). Measurement conditions were typically  
54 15 kV acceleration voltage, 5 nA beam current and 10  $\mu\text{m}$  beam diameter. Fluorine concentrations of  
55 all phases were analyzed with a synthetic multi-layered diffraction crystal (LDE). Counting times were  
56 20 s on the peak and 10 s on the background for all elements.

57 In sample M-114, M-116 and M117 oxygen concentrations were measured using a LDE crystal at the  
58 aforementioned conditions. Water in all runs was then calculated using excess oxygen.

59 Raman spectroscopy measurements were performed at the Institute for Physical Chemistry in  
60 Münster, using a Jobin-Yvon LabRam HR800 spectrometer with a 532 nm wavelength laser, a focal  
61 length of 200mm and a diffraction grating of 1800 gr/mm (Fig. DR2). After using a Si standard for  
62 calibration, the spectra were obtained by averaging two spectra with an acquisition time of 30-40s  
63 for shift ranges of 150 to 1800  $\text{cm}^{-1}$ .

64

## 65 **The influence of Ti and Fe on clinohumite stability in subduction zones**

66 Our data show F-clinohumite is much more stable than its OH-bearing endmembers. This implies that  
67 F-clinohumite should also be stable at high temperatures in a more complex, i.e. in compositions  
68 close to natural systems. The most important additional chemical components in natural  
69 clinohumites are Fe and Ti (e.g. Aoki & Akaogi, 1976; Gaspar, 1992; Weiss, 1997; Koga et al., 2014).  
70 However, it is well known that the addition of Fe to the system will lower the temperature stability of  
71 clinohumite only very slightly (Iwamori, 2004). On the other hand, natural clinohumite contains

often high concentrations of Ti (e.g. Evans & Trommsdorff, 1983; López Sánchez-Vizcaíno et al., 2005) and it has been shown that Ti, very much like F, stabilizes clinohumite to higher temperatures (e.g. Weiss, 1997; Stalder & Ulmer, 2001; Koga et al., 2014). However, it is also known that Ti and F tend to exclude each other (Evans & Trommsdorff, 1983; Ribbe et al., 1968). Consequently, Evans & Trommsdorff (1983) describe natural clinohumites with varying amounts of Ti ( $X_{\text{Ti}} = 0-0.4$ ) and F ( $X_{\text{F}} = 0.1-0.45$ ), where both elements correlate inversely. A pioneering study from Ribbe et al. (1968) suggests that Ti has a destabilizing effect on the clinohumite structure, which limits the natural content to about 0.5 cations per formula unit ( $X_{\text{Ti}} = 0.5$ ). Weiss (1997) and Ulmer & Trommsdorff (1999) show that Ti-saturated OH-clinohumite with  $X_{\text{Ti}} = 0.46$  is stable at T well above the choke point (Figure 1 – line [A]), but these Ti-rich clinohumites are less stable than Ti-free OH-clinohumite with small amounts of fluorine of  $X_{\text{Ti}} < 0.1$  (Figure 1 – line [B]). We can therefore safely assume that the F in clinohumite plays the dominant role on the stability of clinohumite in subduction zones.

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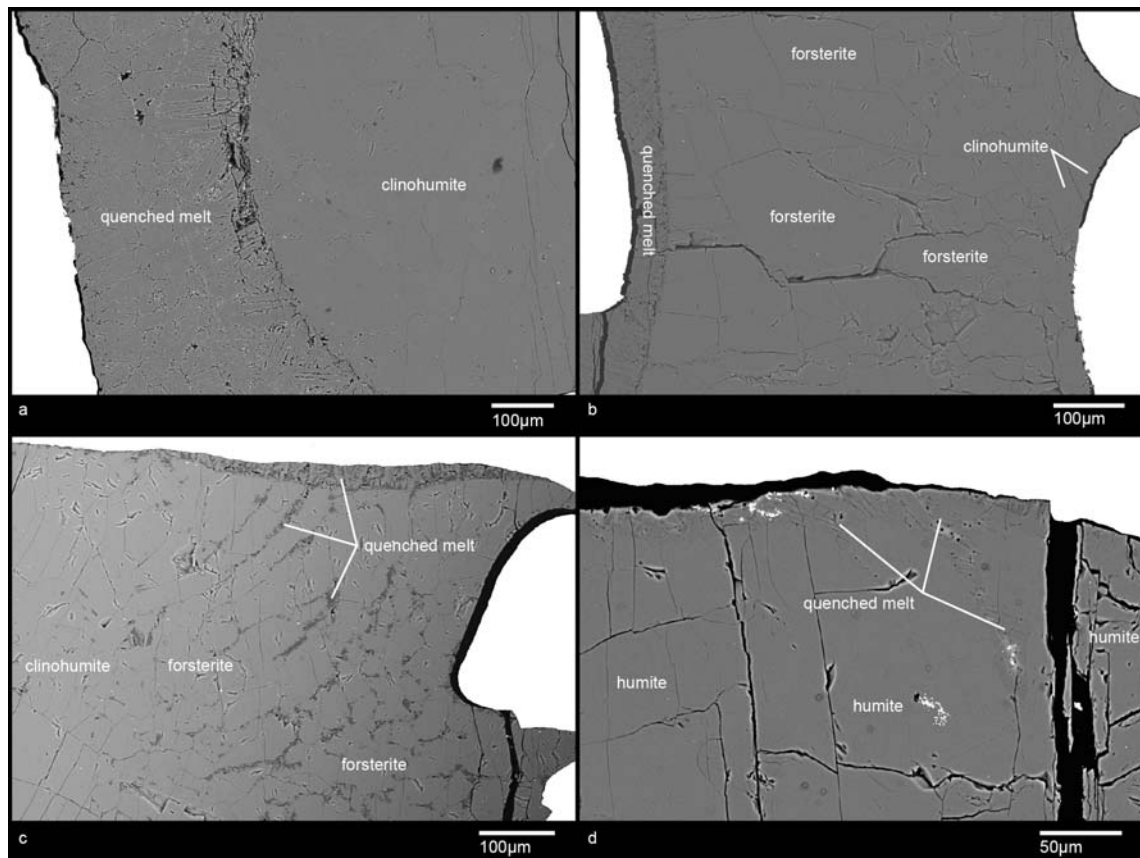


Figure DR1 Representative backscattered electron images of experimental run products. a) M-65, b) M-117, c) M-116, d) M-121. Phases were determined using Raman Spectroscopy and EPMA.

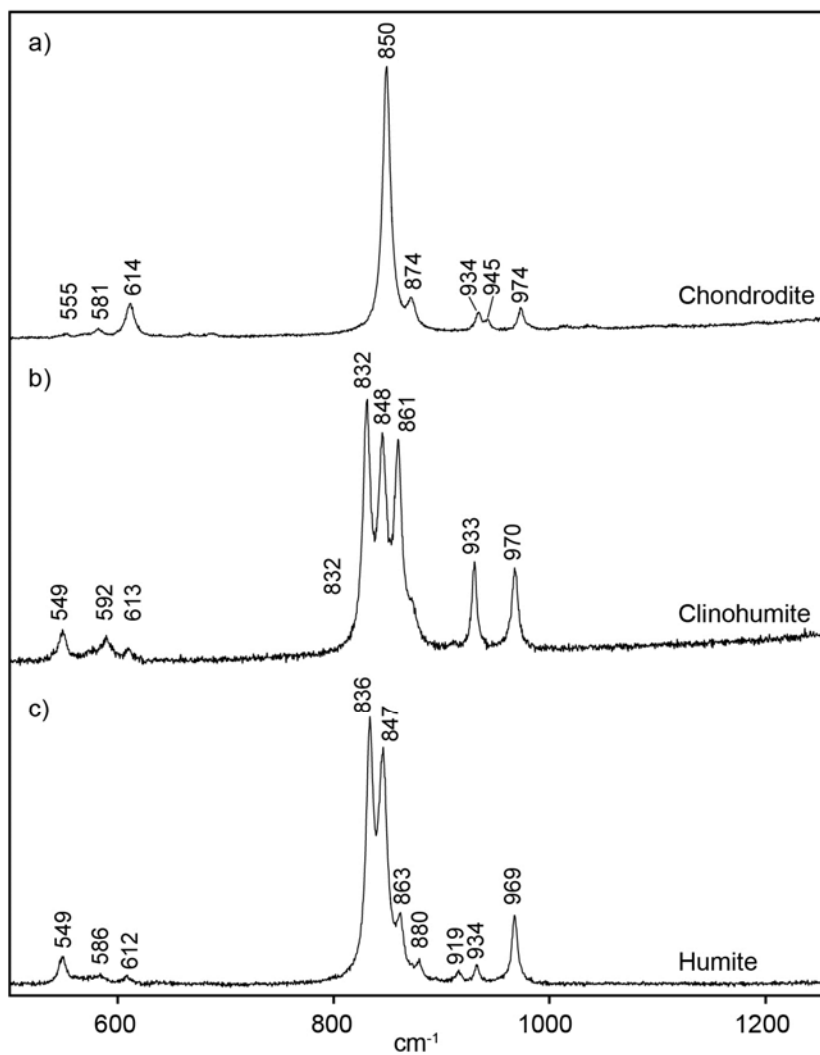


Figure DR2 Raman spectra of a) F-chondrodite (M-122), b) F-clinohumite (M-65) and c) F-Humite (M-122).



157 Table DR1 Experimental runs, 1 atm=atmospheric pressure, chn = chondrodite,  
 158 chu=clinohumite, en=enstatite, hu = humites, fo=forsterite, melt=quenched melt, per= periclase, wd  
 159 = wadsleyite, ahyB = anhydrous B.

Run	T (°C)	P (GPa)	Run time (h)	Present phases
<i>Starting Material: 6 MgO, 3 SiO<sub>2</sub>, 1 MgF<sub>2</sub> (mol proportion)</i>				
M-33	1300	1 atm	48	chu+per
M-13	1500	1 atm	96	fo+melt
M-122	1350	1	4	chn, chu, hu
M-12	1500	1	4	fo+melt
M-121	1500	2	4	hu+melt
M-120	1600	2	2	fo +melt
M-65	1500	5	2	chu+melt
M-82	1700	6	4	fo+chu+melt
M-111	1800	6	0.3	fo+melt?
M-24	1500	8,0	4	chu+en
M-83	1700	17	4	hu+chn+en
M-92	1900	17	0.5	fo+en+hu+chu+chn
M-99	1500	19	3	wd+chn
M-97	1700	19	2	wd+melt
<i>Starting Material: 6 MgO, 3 SiO<sub>2</sub>, 0.5 MgF<sub>2</sub>, 0.5 Mg(OH)<sub>2</sub> (mol proportion)</i>				
M-114	1400	10	2	chu+fluid
M-116	1600	10	1	chu+fo+melt+fluid
M-117	1700	10	1	fo(+chu)+melt+fluid

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161 Table DR2 Representative oxide, F and OH concentrations analyzed with EPMA techniques (wt%). \*Number of analyses given in brackets  
 162 after the run number. Uncertainties are given in the brackets after the analysis, b.d.= below detection limit.

Experiment (#)*	F	OH	SiO <sub>2</sub>	MgO	FeO	Al <sub>2</sub> O <sub>3</sub>	CaO	TiO <sub>2</sub>	Total
F-Chondrodite									
M-24 (6)	9.9(3)	-	34.5(3)	58.4(2)	0.04(2)	0.03(1)	0.06(2)	0.04(2)	98.8(3)
F-Clinohumite									
M-65 (20)	5.9(7)	-	37.7(5)	58.4(3)	b.d	b.d	0.03(1)	b.d	99.7(3)
M-92 (2)	6.2	-	37.5	57.7	b.d.	0.07	b.d.	0.04	98.9
F-Humite									
M-92 (1)	7.9	-	36.87	58.2	b.d.	0.05	0.05	0.08	99.8
M-122(31)	8.5(4)		37.2(4)	57.6(4)	b.d.	0.2(2)	b.d.	b.d.	99.8(5)
Clinohumite, 50mol% F <sup>-</sup> , 50mol% OH <sup>-</sup>									
M-116 (11)	3.7(2)	2.3(6)	37.7(2)	58.3(3)	b.d.	0.27(3)	b.d.	b.d.	99.5(3)
M-114 (7)	3.4(3)	1.3(5)	38.2(1)	58.3(1)	b.d.	0.17(4)	b.d.	b.d.	99.2(4)
M-117 (3)	4.6(3)	2.6(7)	37.4(1)	58.2(2)	b.d.	0.22(2)	b.d.	b.d.	99.7(2)

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