GSA Data Repository item 2017070. Analtyical methods, geologic map, monazite and zircon U-Pb Concordia plots, monazite elemental (x-ray) maps, zircon and monazite data tables, whole rock data table, and monazite standards results

- Appendix DR1. Analytical methods
- Figure DR1. Geologic map
- Figure DR2. U-Pb Concordia plot for zircon
- Figure DR3. U-Pb Tera-Wasserburg plot for monazite
- Figure DR4. Elemental maps of monazite
- Figure DR5 LASS Sm-Nd + U-Pb isotope data for monazite reference materials
- Table DR1. LASS Sm-Nd + U-Pb isotope data for monazite grains A, B, and C
- Table DR2. Lu-Hf and U-Pb isotope data for zircon
- Table DR3. Whole rock geochemical and isotope data
- Table DR4. LASS Sm-Nd and U-Pb isotope data for monazite reference materials

Appendix DR1. Sample processing and imaging; U-Pb analytical methods; Sm-Nd-REE analytical methods; whole rock Sm-Nd isotope analytical methods.

#### Sample processing and imaging

Accessory minerals were separated from each sample using standard crushing, heavy liquid, magnetic separation, and hand-picking techniques. The mineral grains were mounted in epoxy and polished to reveal their interiors. The internal zoning was then documented using back-scattered electron (BSE) imaging for monazite, and cathodoluminescence (CL) using a Jeol JXA-8230 SuperProbe at Memorial University of Newfoundland.

X-ray maps were made on selected monazite grains (e.g., grains 2, 20, and 21) using the same Jeol JXA-8230 SuperProbe. The conditions used were 15 kV, 250 nA, W filament, with a focussed beam. The step size for the X-ray maps was  $0.76 \ \mu m \ x \ 0.76 \ \mu m$  with a dwell time of 200 ms per step. The acquisition time for the X-ray maps ranged between 9 and 12 hours. The X-ray maps were processed using the Jeol software.

# LASS analytical methods-monazite

Monazite from the peraluminous granite sample SW-1 was analyzed using the Laser Ablation-Split Stream (LASS) method at Memeorial University of Newfoundland. The main methodology, instrument specifics, and reference material specifics are described in detail in Goudie et al. (2014) and Fisher et al. (2011a), and thus only a few details relevant to the present study are given here. This method involved the ablation of sample and standards using a 20um laser beam (80um beam for LREE glass standard) operated at 6Hz and 6 J/cm<sup>2</sup>. The ablation aerosol was split downstream of the laser cell to direct a portion of the ablated material to a ThermoFinnigan Element2 ICPMS for measurement of U-Th-Pb isotope measurement and to ThermoFinnigan Neptune MC-ICPMS for measurement of Sm-Nd isotope composition (in addition to isotopes of Ce, Eu, and Gd for concentration detemination). Results of quality control standard Mae Klang monazite are presented below. Additionally, the REE elemental ratios of Trebilock monazite, which are treated as unknowns here, are are also presented.

## U-Pb analytical methods-monazite

As discussed in detail in Goudie et al. (2014), the U-Th-Pb isotope composition (age) of unknowns was calibrated to the Trebilcock monazite standard, which was also used as the calibration material for <sup>143</sup>Nd/<sup>144</sup>Nd. Data for both U-Th-Pb and Sm-Nd-REE analyses were processed using the Iolite software package (Paton et. al., (2010, 2011). The Sm-Nd-REE Iolite Data Reduction Scheme is available from the first author.

# **Sm-Nd-REE** analytical methods

<sup>143</sup>Nd/<sup>144</sup>Nd -Due to the reported bias of LA-MC-ICPMS determinations of Nd isotope composition relative to those obtained by thermal ionization mass spectrometry (TIMS), the benchmark technique for Sm-Nd isotope analysis, the reported <sup>143</sup>Nd/<sup>144</sup>Nd presented here is normalized based on interspersed analyses of mineral reference materials (in this case Trebilcock monazite) which have been previously characterized by

replicate TIMS analyses (see Fisher et al., 2011a). The magnitude of this correction is typically less than 0.5 epsilon units. The <sup>143</sup>Nd/<sup>144</sup>Nd results of standard analyses are given in table DR4 below and plotted in Fig. DR5. Normalization is based on the mean of the measured laser ablation analyses according to equation 1:

$$Sample_{corr} = Sample_{meas} * \left(\frac{Std_{true}}{Std_{meas}}\right)$$
 Eqn. 1

<sup>147</sup>Sm/<sup>144</sup>Nd-Correction of the measured <sup>147</sup>Sm/<sup>144</sup>Nd is described in detail in Fisher et al. (2011a), and is corroborated by the close agreement between the  $^{147}$ Sm/ $^{144}$ Nd determined for reference minerals during the course of this study and those determined by ID-TIMS for the same material. Due to the ubiquitous Sm/Nd zoning present in natural minerals, and the difficulty in producing synthetic mineral standards with homogeneous Sm/Nd, quantification of the accuracy and precision of LA-MC-ICPMS measurement of <sup>147</sup>Sm/<sup>144</sup>Nd is difficult. The Trebilcock monazite standard has a relatively restricted range in Sm/Nd, and thus offers a good estimate of the reproducibility of our Sm/Nd measurements (see Fisher et al., 2011a). The <sup>147</sup>Sm/<sup>144</sup>Nd measured for the Trebilcock standard during the course of this study is  $0.2242 \pm 0.0058$ (2SD) which is in agreement with measured TIMS values  $(0.2167 \pm 0.0125)$  and attests to the accuracy of the technique, though the measured values during this study are consistently on the higher end of the TIMS range. We attribute this to using a single piece of this standard with Sm/Nd slightly higher than the mean of the TIMS analyses. The relative standard deviation for Trebilcock monazite analyzed during this study is

~2.5%, which we consider to be a worse case estimate of the reproducibility of this method. As shown in figure DR5 (and Table DR4), our measurements of Trebilcock monazite display homogeneous  $^{143}$ Nd/ $^{144}$ Nd and a relatively restricted range of Sm/Nd in agreement with results from ID-TIMS analyses (Fisher et al., 2011).

**Ce/Gd and Eu/Eu\*-** A single data acquisition comprises the measurement of a number of Nd isotopes (143, 144, 145, 146) and Sm isotopes (147, 149) along with isotopes of Ce (142), Eu (153), and Gd (155). In order to determine the relative abundance of each element the signal intensity (in volts) is measured for the Ce, Eu, and Gd isotopes above as well as <sup>146</sup>Nd and <sup>149</sup>Sm. These voltages are then abundance normalized using the following isotopic abundances <sup>142</sup>Ce (11.08%), <sup>146</sup>Nd (17.19%), <sup>149</sup>Sm (11.30%), <sup>153</sup>Eu (52.20%), and <sup>155</sup>Gd (15.65%). With the exception <sup>142</sup>Ce, all other isotopes are interference-free. The isobaric interference of <sup>142</sup>Nd on <sup>142</sup>Ce is mathematically corrected using the measured <sup>146</sup>Nd and a <sup>142</sup>Nd/<sup>146</sup>Nd of 1.5782 (Eqn. 2 and 3).

$$^{142}Ce(v)_{calculated} = total142(v) - {}^{142}Nd(v)_{calculated} \qquad \text{Eqn. 2}$$

$$^{142}Nd(v)_{calculated} = {}^{146}Nd(v)_{measured} * \left(\frac{{}^{142}Nd}{{}^{146}Nd}_{true}\right) \qquad \text{Eqn. 3}$$

**Ce/Gd** is determined using the resulting Ce and Gd abundance normalized REE voltages. These data are then further normalized to the LREE glass described in Fisher et al., 2011a. This normalization theoretically corrects for both instrumental drift (though drift was negligible (<1%) during the course of this study and thus normalization was

based on the mean of the standards) as well as differential ablation yields of the individual elements. The LREE glass has been characterized for its Ce (23,200 ppm) and Gd (3470 ppm) content, and therefore Ce/Gd (6.69), by solution ICPMS. Normalization is done using Eqn. 1 above .

**Eu/Eu\*** is a measure of the deviation of the actual Eu content of a material to that expected from a linear fit to neighboring REE's Sm and Gd, with each element normalized to chondritic (CN) abundances (Eqn. 4).

$$Eu / Eu^* = \frac{Eu_{CN}}{(Sm_{CN} * Gd_{CN})^{0.5}}$$
 Eqn. 4

The chondrite normalization for the abundance normalized voltages of Sm, Eu, and Gd is done by dividing the these voltages by the chondritic concentration of these elements (all expressed in ppm) using the values of McDonough and Sun (1995). The resulting Eu/Eu\* is further normalized to the Eu/Eu\* (similarly calculated) determined in the LREE glass. Table 5 in Fisher et al. (2011a) summarizes a comparison of this approach to that of a 'typical' LA-ICPMS measurement (ie., normalized to a glass standard with further internal normalization done by electron microprobe elemental concentration analyses of a major mineral- see Jackson et al. (1992) for details). The data for each of the mineral standards analyzed during this study agree well with those of the Fisher et al. (2011a) study.

#### LASS quality control standard

Twenty-two analyses of the Mae Klang monazite (used here as a quality control standard) yielded a mean <sup>143</sup>Nd/<sup>144</sup>Nd of 0.512641 ± 28 (2SD) and a <sup>147</sup>Sm/<sup>144</sup>Nd range of 0.0867 to 0.1146, both of which are in excellent agreement with the ID-TIMS values presented by Fisher et al. (2011a) (mean <sup>143</sup>Nd/<sup>144</sup>Nd = 0.512646 ± 10 (2SD); range of <sup>147</sup>Sm/<sup>144</sup>Nd 0.0870 to 0.1209). Simultaneous U-Th-Pb age determinations yielded a <sup>207</sup>Pb-corrected weighted mean <sup>206</sup>Pb/<sup>238</sup>U age of 26.8 ± 0.3 Ma (2 $\sigma$ ), and a weighted mean <sup>208</sup>Pb/<sup>232</sup>Th age of 27.1 ± 0.2 Ma (2 $\sigma$ ), both of which are in agreement with the ID-TIMS age of 26.8 ± 0.5 Ma determined by Dunning et al. (1995).

## Whole rock Sm-Nd isotope analytical methods

Whole rock powder for SW-1 was dissolved in Savilex© Teflon beakers using an 8 ml (4:1) mixture of 29 M HF – 15 M HNO<sub>3</sub>. Prior to acid digestion, a mixed <sup>150</sup>Nd/<sup>149</sup>Sm spike was added. After five days of digestion, the solution was evaporated to dryness and then taken up in a saturated solution of 6 M HCl and H<sub>3</sub>BO<sub>3</sub> (boric acid) for at least 24 hours. Addition of boric acid ensured that any remaining solid fluorides were converted to soluble chlorides (Mulcahy et al., 2009). The sample was then evaporated to dryness and re-dissolved in 2.5 M HCL. Bulk rare earth elements (REE) were then isolated using cation exchange resin AG-50W-X8, H+ form, 200-400 mesh. This solution was then dried and taken up in 0.18 M HCl and loaded on a second column containing Eichrom© Ln resin (50-100 mesh) to isolate Sm and Nd from the other REE. All reagents were distilled and the average total chemical blank measured at the MUN TIMS laboratory was less than 100 pg for Nd and therefore considered negligible. Thus no blank correction was performed

Samarium and Nd concentrations and the Nd isotopic composition was determined using a multi-collector Finnigan Mat 262 mass spectrometer in static for concentration determination, and dynamic mode for Nd isotopic composition determination. Instrumental mass fractionation of Sm and Nd isotopes was corrected using a Raleigh law relative to  ${}^{146}$ Nd/ ${}^{144}$ Nd = 0.7219 and  ${}^{152}$ Sm/ ${}^{147}$ Sm = 1.783. The reported values were adjusted to the JNdi-1 standard ( $^{143}$ Nd/ $^{144}$ Nd = 0.512115. Tanaka et al., 2000). During the course of this study JNdi-1 yield a mean  $^{143}$ Nd/ $^{144}$ Nd = 0.512101 ± 16 (2SD, n=40). Five analyses of USGS whole rock reference material BRC-2 were run during the course of this study. Each analysis comprised a separate dissolution and thus provides the best estimate of the reproducibility of an individual whole rock analysis. The mean values of BCR-2 are as follows where the relative two standard deviations of the mean are given in percent in parenthesis;  $^{143}Nd/^{144}Nd = 0.512636 (0.0025\%)$ ;  $^{147}$ Sm/ $^{144}$ Nd = 0.1384 (0.25%); Nd ppm=27.7 (0.7%); Sm = 6.34 (0.6%). These values are in excellent agreement with recent determinations made in other laboratories (eg., Razcek et al., 2001; Razcek et al., 2003; Schmitz et al., 2004; Weis et al., 2006). The analytical uncertainty given for Nd isotopic ratios is the in-run precision expressed as two standard error of the mean (2SE) and is typically <0.002%.

## Zircon U-Th-Pb analytical methods

Zircon U-Pb geochronology and scanning ion imaging was performed using a CAMECA IMS1280 large geometry ion microprobe at the Nordsim facility, NRM. Geochronological analyses follow routine protocols outlined by Whitehouse et al. (1999) and Whitehouse and Kamber (2005). A ca. 4.5 nA, -13 kV  $O_2^-$  primary beam (imaged

aperture of 150  $\mu$ m corresponding to a spot diameter on the sample of ca. 15  $\mu$ m) was used to generate +10 kV secondary ions which were admitted to the mass spectrometer and detected in a peak-hopping sequence using a single ion-counting electron multiplier. The mass spectrometer was operated at a mass resolution (M/ $\Delta$ M) of 5400, sufficient to separate all species of interest from molecular interferences. Each analysis comprised a 90 second pre-sputter to remove the Au-coating and allow the secondary beam to stabilize, centering of the secondary beam in the field aperture, energy optimization in the 45 eV energy window, mass calibration adjustment using the <sup>90</sup>Zr<sub>2</sub><sup>16</sup>O peak, and 12 cycles through the species of interest. Groups of analyses were performed in fully automated sequences, regularly interspersing standard analyses with those of the sample zircon grains. Data reduction utilized an in-house developed suite of software. Pb-isotope ratios were corrected for common Pb estimated from measured <sup>204</sup>Pb assuming the present-day terrestrial Pb isotope composition estimated from the model of Stacey and Kramers (1975); where the <sup>204</sup>Pb count was statistically insignificant relative to the longterm background on the EM, no correction was applied. U/Pb ratios were calibrated using an empirical power-law relationship between <sup>206</sup>Pb/<sup>238</sup>U and <sup>238</sup>U<sup>16</sup>O<sub>2</sub>/<sup>238</sup>U assuming the 1065 Ma age of the 91500 zircon (Wiedenbeck et al., 1995). Age calculations assume the decay constant recommendations of Steiger and Jäger (1975) and utilize the routines of Isoplot-Ex (Ludwig, 2004).

#### Zircon Lu-Hf analytical methods

Following SIMS analysis of the U-Pb-Th ages, zircons were analyzed for their Lu-Hf isotope composition at Memorial University of Newfoundland. Analyses were done using a ThermoFinnigan Neptune MC-ICPMS coupled to a Geolas Pro 193 nm Ar-F excimer laser operating at 10Hz, 5 J/cm<sup>2</sup>, and a 50 um diameter spot size. The cup configuration, analytical methodology, and data reduction protocol are described in detail in Fisher et al. (2011b).

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**Figure DR1.** Geologic map of the Late Cretaceous Old Woman-Puite Range batholith, southeastern California. Star denotes sample location of SW-1 discussed in this study. Modified after Foster et al., 1992. PR-Painted Rock pluton, OW-Old Woman pluton, SW- Sweetwater Wash pluton, LD-Lazy Daisy pluton, EP -East Puite pluton, NP-North Puite pluton.



Figure DR2. Tera-Wasserburg plot of SW-1 monazite grains A, B, and C.



**Figure DR3.** U-Pb age data for SW-1 zircon samples. a) concordia plot of inherited zircon cores ; b) Tera-Wasserburg plot of magmatic zircon; c) weighted mean <sup>207</sup>Pb corrected <sup>206</sup>Pb/<sup>238</sup>U agesof magmatic zircon; d) representative cathodoluminesence images (CL) of zircon crystals in sample SW-1, along with initial ɛHf values calculated at the prefered age (U/Pb age for Cretaceous zircon; Pb/Pb age for Proterozoic zircon), laser spot size is 50µm in all images.



**Figure DR4.** Compositional (elemental) x-ray maps for the monazite grains A, B, and C



**Figure DR5.** a) Reproducibility of Mae Klang and Trebilcock monazite Nd-standards for <sup>143</sup>Nd/<sup>144</sup>Nd and <sup>147</sup>Sm/<sup>144</sup>Nd compared to ID-TIMS analyses (in grey box). Note that Trebilock analyses are self-normalized for <sup>143</sup>Nd/<sup>144</sup>Nd, but not for <sup>147</sup>Sm/<sup>144</sup>Nd. b) Reproducibility of <sup>143</sup>Nd/<sup>144</sup>Nd for the Mae Klang Nd-standard compared to ID-TIMS, note reproducibility is ~0.5 epsilson units (2SD). c) Reproducibility of Mae Klang and Trebilcock monazite Nd-standards for Ce/Gd vs. Eu/Eu\*. d) Tera-Wasserburg diagram of concurrent U-Pb age results from the Mae Klang monazite; ID-TIMS age 26.8 Ma (Dunning et al., 1995)

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<td>EulEr:<br/>2.143<br/>0.154<br/>0.155<br/>0.155<br/>0.155<br/>0.151<br/>0.155<br/>0.151<br/>0.155<br/>0.151<br/>0.155<br/>0.151<br/>0.155<br/>0.151<br/>0.155<br/>0.151<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0.155<br/>0</td> 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<td>Diradom/<br/>52<br/>52<br/>53<br/>54<br/>56<br/>56<br/>56<br/>56<br/>56<br/>56<br/>56<br/>56<br/>57<br/>52<br/>55<br/>56<br/>56<br/>56<br/>56<br/>56<br/>56<br/>56<br/>56<br/>56<br/>56<br/>56<br/>56</td> <td><math display="block">\begin{array}{c} \begin{array}{c} 0 \\ \hline \\ 0 \\ \hline \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\</math></td> <td>1997 00
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<td>122<br/>(a. 003)<br/>(a. 003)<br/>(b. 003)</td> <td>Page         D           Page         D           0.0121         D           0.0121         D           0.0121         D           0.0121         D           0.0120         D           0.0121         D           0.0121         D           0.0118         D           0.0121         D           0.01221         D           0.01221         D           0.01220         D           0.01221         D           0.01220         D           0.01221         D           0.0122         D           0.0122         D           0.0122         D           0.0123         D           0.0124         D           0.0125         D           0.0129         D           0.0129         D           0.0120         D           0.01217         D           0.0126         D           0.0126         D           0.0126         D           0.0126         D           0.0126         D           0.0126         D     &lt;</td> <td>112<br/>0.0502<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.0503<br/>0.050</td>
<td>hbc<br/>0.062<br/>0.062<br/>0.062<br/>0.070<br/>0.070<br/>0.070<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.070<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.071<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.072<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.075<br/>0.0750<br/>0.0750000000000</td> 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70<br/>21,200<br/>22,200<br/>24,200<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,2400<br/>24,24000<br/>24,24000<br/>24,24000<br/>24,24000<br/>24,</td> 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   | 0015         0.0121           0027         0.9202           0027         0.9202           0016         0.0101           0017         0.9202           0010         0.1102           0027         0.9202           0020         0.0101           0022         0.1044           0022         0.1044           0022         0.1044           0021         0.1044           0021         0.1044           0021         0.1044           0021         0.1044           0021         0.1044           0021         0.1044           0022         0.1044           0025         0.1082           0026         0.0055           0026         0.0055           0026         0.0055           0026         0.0154           0026         0.0154           0026         0.0154           0026         0.0154           0027         0.1084           0028         0.1022           0029         0.1044           00201         0.1222           00202         0.1044           00203<           | 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| 0.53         0.0017           0.13         0.0017           0.240         0.0017           0.240         0.0017           0.240         0.0017           0.240         0.0018           0.240         0.0018           0.240         0.0018           0.240         0.0018           0.240         0.0018           0.240         0.0018           0.241         0.0018           0.241         0.0019           0.241         0.0019           0.241         0.0019           0.241         0.0019           0.242         0.0016           0.243         0.0019           0.244         0.0019           0.243         0.0019           0.244         0.0019           0.243         0.0016           0.244         0.0016           0.244         0.0016           0.244         0.0016           0.244         0.0016           0.244         0.0016           0.244         0.0016           0.244         0.0016           0.244         0.0016           0.244         0.0016   | 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Table DR2. Lu-Hf and U-Pb isotope data for SW1 zircons

Table DR2. Lu-HI and U-Pb lootope data for SW1 zircons																														
																			207-corr											
_	<sup>176</sup> Hf/ <sup>177</sup> Hf	2SE	<sup>176</sup> Lu/ <sup>177</sup> Hf	2SE	<sup>136</sup> Yb/ <sup>177</sup> Hf	2SE	<sup>128</sup> Hf/ <sup>177</sup> Hf	2SE	<sup>176</sup> Hf/ <sup>177</sup> Hf(i)	eHf(t) <sup>1</sup>	2SE	eHf(73Ma) <sup>1</sup>	<sup>207</sup> Pb/ <sup>235</sup> U	1SE	<sup>266</sup> Pb/ <sup>238</sup> U	1SE	rho	<sup>207</sup> Pb/ <sup>206</sup> Pb	1SE	<sup>207</sup> Pb/ <sup>206</sup> Pb age	1SE	<sup>207</sup> Pb/ <sup>225</sup> U age	1SE	<sup>206</sup> Pb/ <sup>228</sup> U age	1SE	age (Ma)	1SE	U (ppm)	Th (ppm)	Th/U
SW1_b	0.282369	0.000021	0.000494	0.000034	0.012792	0.000947	1.467237	0.000031	0.282369	-13.1	0.8	-	0.05624	11.78	0.0112	1.29	0.10946	0.03653	11.71	nd	291.4	55.6	6.4	71.6	0.9	72.6	0.9	120	106	0.89
SW1_13	0.282317	0.000028	0.000472	0.000012	0.015219	0.000217	1.467264	0.000035	0.282316	-15.1	1.0	-	0.04717	12.79	0.0105	0.94	0.07354	0.03257	12.76	nd	336.6	46.8	5.9	67.4	0.6	68.6	0.6	132	66	0.50
SW1_83	0.282320	0.000019	0.000251	0.000005	0.006833	0.000175	1.467236	0.000035	0.282320	-14.9	0.7		0.05708	15.04	0.0109	1.30	0.08622	0.03800	14.98	nd	357.3	56.4	8.3	69.8	0.9	70.7	0.9	66	49	0.75
SW1_h	0.282319	0.000031	0.000729	0.000068	0.018318	0.001727	1.467273	0.000050	0.282318	-15.0	1.1		no data	no data	0.0106	1.81	no data	nd	nd	nd	nd	nd	nd	68.2	1.2	70.4	1.2	19	21	1.11
SW1_76	0.282276	0.000030	0.000569	0.000013	0.016623	0.000338	1.467246	0.000043	0.282275	-16.4	1.1		0.06332	7.10	0.0111	1.01	0.14170	0.04142	7.03	nd	169.5	62.3	4.3	71.1	0.7	71.6	0.8	34	51	1.50
SW1_f	0.282427	0.000021	0.001422	0.000134	0.034405	0.003241	1.467231	0.000039	0.282425	-11.1	0.8		0.05979	5.78	0.0110	1.35	0.23273	0.03936	5.62	nd	140.4	59.0	3.3	70.6	0.9	71.4	1.0	224	79	0.35
SW1_74r	0.282347	0.000024	0.001386	0.000068	0.040932	0.001994	1.467247	0.000040	0.282346	-13.9	0.9	-	0.06203	6.27	0.0113	0.81	0.12907	0.03977	6.22	nd	153.9	61.1	3.7	72.5	0.6	73.2	0.6	103	128	1.24
SW1_e	0.282378	0.000029	0.000651	0.000043	0.017868	0.001094	1.467250	0.000044	0.282377	-12.8	1.0	-	0.05367	11.44	0.0112	1.26	0.10989	0.03473	11.37	nd	291.8	53.1	5.9	71.8	0.9	73.0	0.9	109	56	0.51
SW1_a	0.282314	0.000029	0.001003	0.000082	0.027416	0.002329	1.467264	0.000043	0.282312	-15.1	1.0		no data	no data	0.0110	2.13	no data	nd	nd	nd	nd	nd	nd	70.5	1.5	73.4	1.2	50	120	2.40
SW1_112	0.282273	0.000033	0.000848	0.000023	0.029242	0.000892	1.467237	0.000050	0.282272	-16.5	1.2		0.07265	4.54	0.0115	0.77	0.16899	0.04590	4.48	nd	104.7	71.2	3.1	73.6	0.6	73.7	0.6	144	147	1.02
SW1_130	0.282357	0.000021	0.001338	0.000041	0.042354	0.001715	1.467217	0.000041	0.282356	-13.5	0.8		0.07509	1.78	0.0116	0.67	0.37643	0.04688	1.65	nd	39.0	73.5	1.3	74.5	0.5	74.5	0.5	884	351	0.40
SW1_107	0.282326	0.000038	0.001128	0.000039	0.032918	0.000549	1.467276	0.000075	0.282324	-14.6	1.3		0.08113	9.94	0.0117	0.99	0.10001	0.05014	9.89	nd	214.8	79.2	7.6	75.2	0.7	75.0	0.8	82	96	1.17
SW1_134	0.282418	0.000023	0.000945	0.000015	0.030901	0.000829	1.467240	0.000035	0.282417	-11.4	0.8	-	0.07486	1.52	0.0118	0.66	0.43668	0.04615	1.37	nd	38.1	73.3	1.1	75.4	0.5	75.5	0.5	969	102	0.11
SW1_72	0.282311	0.000031	0.000629	0.000000	0.018356	0.000143	1.467279	0.000049	0.282298	6.9	1.1	-15.2	1.91459	1.50	0.1846	0.67	0.44529	0.07524	1.34	1074.9	26.7	1086.2	10.0	1091.8	6.7			40	26	0.66
SW1_47c	0.282223	0.000030	0.000933	0.000016	0.023778	0.000241	1.467275	0.000051	0.282200	8.5	1.1	-18.3	2.33417	0.95	0.2008	0.66	0.69115	0.08433	0.69	1300.1	13.4	1222.7	6.8	1179.4	7.1			116	51	0.44
SW1_58	0.281820	0.000023	0.000609	0.000007	0.019337	0.000371	1.467275	0.000038	0.281805	-5.4	0.8	-32.6	1.88608	1.45	0.1620	0.66	0.45442	0.08446	1.29	1303.2	24.9	1076.2	9.7	967.6	5.9			56	67	1.19
SW1_195	0.281844	0.000029	0.000650	0.000052	0.018807	0.001492	1.467278	0.000037	0.281825	-0.1	1.0	-31.7	3.23346	1.88	0.2502	1.32	0.70425	0.09372	1.33	1502.5	25.0	1465.2	14.7	1439.6	17.1			23	18	0.78
SW1_25	0.281888	0.000034	0.000806	0.000025	0.026212	0.001139	1.467291	0.000054	0.281864	2.3	1.2	-30.1	3.34982	0.87	0.2529	0.68	0.77379	0.09606	0.55	1549.0	10.3	1492.7	6.8	1453.5	8.8			187	143	0.77
SW1_d	0.282163	0.000025	0.000533	0.000035	0.013218	0.000998	1.467248	0.000040	0.282148	12.7	0.9	-20.4	3.71122	1.37	0.2781	1.15	0.83958	0.09680	0.74	1563.4	13.9	1573.8	11.0	1581.6	16.1			80	31	0.39
SW1_j	0.281851	0.000021	0.000538	0.000057	0.014294	0.001453	1.467252	0.000037	0.281834	1.8	0.8	-31.5	1.27340	1.42	0.0948	1.26	0.88652	0.09739	0.66	1574.8	12.2	833.9	8.1	584.0	7.0			390	85	0.22
SW1_g	0.282033	0.000034	0.000686	0.000018	0.017708	0.000401	1.467241	0.000033	0.282012	9.5	1.2	-25.0	3.93227	1.57	0.2836	1.16	0.73917	0.10057	1.05	1634.6	19.5	1620.3	12.8	1609.4	16.5			35	18	0.53
SW1_33	0.282090	0.000030	0.001066	0.000027	0.031751	0.000529	1.467181	0.000046	0.282057	11.3	1.1	-23.0	2.84766	0.86	0.2046	0.72	0.83554	0.10095	0.47	1641.7	8.7	1368.2	6.5	1199.9	7.8			211	101	0.48
SW1_61	0.281829	0.000029	0.000814	0.000028	0.025112	0.001273	1.467236	0.000041	0.281804	2.4	1.0	-32.2	3.84720	0.70	0.2759	0.68	0.96857	0.10115	0.18	1645.3	3.2	1602.7	5.7	1570.5	9.5			1244	689	0.55
SW1_74c	0.282095	0.000031	0.000503	0.000032	0.015048	0.000942	1.467236	0.000045	0.282079	12.2	1.1	-22.8	3.40024	0.76	0.2434	0.69	0.91404	0.10130	0.31	1648.1	5.7	1504.5	6.0	1404.6	8.8			653	45	0.07
SW1_18	0.281816	0.000029	0.000783	0.000014	0.026060	0.000238	1.467257	0.000052	0.281791	2.2	1.0	-32.7	3.90346	0.88	0.2783	0.68	0.76919	0.10174	0.56	1656.0	10.4	1614.4	7.1	1582.7	9.5			107	132	1.23
SW1_81	0.281854	0.000027	0.001390	0.000032	0.036763	0.000670	1.467241	0.000032	0.281810	2.9	1.0	-31.4	3.89076	0.70	0.2770	0.68	0.96094	0.10189	0.19	1658.8	3.6	1611.8	5.7	1576.0	9.5			779	127	0.16
SW1_184	0.281809	0.000023	0.000462	0.000011	0.012115	0.000276	1.467229	0.000039	0.281794	2.5	0.8	-32.9	4.40476	1.71	0.3123	1.42	0.83022	0.10229	0.95	1666.1	17.5	1713.2	14.2	1752.1	21.8			34	27	0.78
<sup>1</sup> obif is dotor	minod writes the	o CHILID para	motors of Rou	vior at al. (20	108)																									

<sup>1</sup>EHF is determined using the CHUR parameters of Bouvier et al. (2008)

Analyte	SW-1	Unit	Detection Limit
SiO2	73.06	%	0.01
AI2O3	15.36	%	0.01
Fe2O3(1)	1.89	%	0.01
MaO	0.03	%o	0.001
CaO	1 72	%	0.01
Na2O	3 76	%	0.01
K20	3.93	%	0.01
TiO2	0.136	%	0.001
P2O5	0.06	%	0.01
LOI	0.43	%	
lotal	100.7	%	0.01
SC	3	ppm	1
V	8	npm	5
Cr	260	maa	20
Co	28	ppm	1
Ni	120	ppm	20
Cu	10	ppm	10
Zn	50	ppm	30
Ga	20	ppm	1
Ge	1.5 < 5	pm	0.5
Rb	131	npm	1
Sr	474	ppm	2
Ŷ	21.4	ppm	0.5
Zr	169	ppm	1
Nb	23	ppm	0.2
Mo	5	ppm	2
Ag	0.6	ppm	0.5
iii Sn	< 0.1 5	ppm	0.1
Sb	< 0.2	ppm	0.2
Cs	3.4	ppm	0.1
Ва	1483	ppm	3
La	37.6	ppm	0.05
Ce	72.9	ppm	0.05
Pr	7.93	ppm	0.01
Sm	20.7	ppm	0.05
Eu	0.924	ppm	0.005
Gd	3.89	ppm	0.01
Tb	0.63	ppm	0.01
Dy	3.87	ppm	0.01
Ho	0.8	ppm	0.01
Er	2.37	ppm	0.01
Yh	2 43	npm	0.005
Lu	0.368	ppm	0.002
Hf	4.4	ppm	0.1
Та	5.43	ppm	0.01
W	295	ppm	0.5
ll Dh	0.57	ppm	0.05
Bi	0.4	ppm	01
Th	13.6	ppm	0.05
U	2.17	ppm	0.01
Sm (ppm) Nd (ppm)	5.08 28 86		
	_0.00		
<sup>14</sup> ′Sm/ <sup>144</sup> Nd <sup>143</sup> Nd/ <sup>144</sup> Nd 2SE	0.1064 0.511778 0.000007		
εNd <sub>73Ma</sub> 1 Eu/Eu* Ce/Gd	-15.8 0.61 18.7		

Table DR3. Whole rock major and trace element geochemistry.

 $^{1}\epsilon_{\scriptscriptstyle Nd}$  values calculated using CHUR values of Bouvier et al., (2008).

#### Table DR4. Sm-Nd and U-Pb isotope results for Trebilcock monazite

147 146			measured		measured					
Analysis	<sup>147</sup> Sm (V)	<sup>146</sup> Nd (V)	<sup>143</sup> Nd/ <sup>144</sup> Nd	2SE	<sup>145</sup> Nd/ <sup>144</sup> Nd	2SE	<sup>147</sup> Sm/ <sup>144</sup> Nd	2SE	Eu/Eu*	Ce/Gd
Treb_1	0.47	1.39	0.512581	0.000027	0.348436	0.000016	0.2248	0.0003	0.019	5.913
Treb 2	0.43	1.30	0.512544	0.000033	0.348382	0.000014	0.2250	0.0003	0.019	5.934
Treb 3	0.44	1.33	0.512578	0.000034	0.348398	0.000014	0.2240	0.0003	0.019	6.039
Treb 4	0.42	1.29	0.512506	0.000038	0.348403	0.000020	0.2243	0.0003	0.019	6.044
Treb 5	0.40	1.23	0.512563	0.000034	0.348413	0.000019	0.2232	0.0004	0.019	6.116
Treb 6	0.41	1.26	0.512548	0.000034	0.348383	0.000016	0.2239	0.0002	0.019	5.992
Treb 7	0.40	1.22	0.512570	0.000025	0.348384	0.000015	0.2237	0.0003	0.019	6.038
Treb 8	0.41	1.27	0.512533	0.000029	0.348435	0.000020	0.2202	0.0003	0.019	6.164
Treb 9	0.42	1.29	0.512562	0.000043	0.348425	0.000018	0.2230	0.0003	0.019	5.996
Treb 10	0.40	1.24	0.512540	0.000031	0.348430	0.000021	0.2195	0.0003	0.019	6.150
Treb 11	0.41	1.28	0.512544	0.000021	0.348447	0.000018	0.2192	0.0002	0.019	6.136
Treb 12	0.37	1.13	0.512555	0.000036	0.348434	0.000017	0.2212	0.0004	0.019	6.042
Treb 13	0.57	1.73	0.512547	0.000033	0.348459	0.000027	0.2221	0.0001	0.019	5.893
Treb 14	0.41	1.25	0.512527	0.000032	0.348425	0.000020	0.2218	0.0005	0.019	5,985
Treb 15	0.39	1.18	0.512538	0.000032	0.348439	0.000023	0.2204	0.0004	0.019	6.030
Treb 16	0.37	1.14	0.512564	0.000034	0.348442	0.000018	0.2205	0.0004	0.019	6.023
Treb 17	0.41	1.25	0.512535	0.000044	0.348430	0.000013	0.2210	0.0002	0.019	5.883
Treb 18	0.35	1.09	0.512515	0.000031	0.348463	0.000015	0.2201	0.0005	0.019	6.023
Treb 19	0.35	1.10	0.512530	0.000028	0.348449	0.000016	0.2164	0.0003	0.019	6.156
Treb 20	0.35	1.10	0 512543	0.000034	0 348459	0.000024	0.2201	0.0003	0.019	5 940
Treb 21	0.32	1.00	0.512556	0.000032	0.348433	0.000018	0.2189	0.0005	0.019	6.004
Treb 22	0.36	1 11	0 512505	0.000024	0 348439	0.000015	0 2169	0.0004	0.019	5 996
Treb 23	0.37	1 15	0.512558	0.000031	0 348441	0.000017	0.2103	0.0003	0.019	5.973
1105_25	0.57	1.15	0.512550	0.000031	0.510111	0.000017	0.2172	0.0002	0.015	5.575
Treh 1	0.53	1 59	0 512526	0 000045	0 348445	0 000022	0 2257	0 0002	0.019	5 657
Treb 2	0.46	1.55	0.512528	0.000030	0.348452	0.000022	0.2237	0.0002	0.019	5.899
Treb 3	0.51	1.56	0.512520	0.000040	0.348437	0.000020	0.2223	0.0003	0.019	5.855
Treb 4	0.48	1.30	0.512555	0.000028	0 348437	0.000018	0.2223	0.0003	0.019	5.870
Treb 5	0.50	1.53	0.512555	0.000020	0 348440	0.000018	0.2212	0.0003	0.019	5 913
Treb 6	0.46	1 39	0.512501	0.000035	0 348444	0.000020	0.2245	0.0005	0.019	5.515
Treb 7	0.40	1.33	0.512520	0.000042	0.348478	0.000020	0.2245	0.0003	0.019	5 769
Treb 8	0.45	1 38	0 512553	0.000031	0 348445	0.000014	0 2247	0.0004	0.019	5 703
Treb 9	0.47	1.30	0 512533	0.000039	0 348437	0.000014	0 2247	0.0005	0.019	5.716
Treb 10	0.41	1.72	0.512544	0.000027	0 348420	0.000010	0.2252	0.0003	0.019	5 641
Treb 11	0.47	1.23	0.512520	0.000035	0 348433	0.000015	0.2255	0.0005	0.019	5 632
Treb 12	0.46	1.45	0.512535	0.000033	0.348433	0.000013	0.2255	0.0003	0.019	5.032
Treb 13	0.43	1.35	0.512555	0.000038	0.348443	0.000013	0.2255	0.0003	0.019	5 581
Treb 14	0.43	1.30	0.512512	0.000030	0.348427	0.000021	0.2230	0.0004	0.019	5.869
Treb 15	0.44	1.31	0.512514	0.000031	0.348436	0.000017	0.2214	0.0004	0.019	5.005
Treb 16	0.44	1.37	0.512550	0.000020	0.348435	0.000010	0.2225	0.0003	0.019	5.625
Treb 17	0.40	1.42	0.512504	0.000030	0.348423	0.000017	0.2251	0.0004	0.019	5 864
Treb 18	0.42	1.31	0.512555	0.000027	0.348439	0.000020	0.2210	0.0003	0.019	5 737
Treb 19	0.43	1.45	0.512555	0.000027	0.348450	0.000015	0.2232	0.0007	0.019	5 810
Treb 20	0.43	1.55	0.512550	0.000030	0.348431	0.000010	0.2210	0.0003	0.019	5.815
Treb_20	0.41	1.20	0.512541	0.000031	0.348433	0.000020	0.2214	0.0004	0.019	5 631
Trob 22	0.43	1.30	0.512525	0.000032	0.348431	0.000018	0.2238	0.0003	0.019	5.031
Treb 23	0.44	1.37	0.512549	0.000037	0.348424	0.000014	0.2214	0.0004	0.019	5.785
Treb 24	0.47	1.42	0.512510	0.000033	0.340432	0.000017	0.2243	0.0013	0.019	5.370
Treb 25	0.33	1.71	0.512557	0.000033	0.346435	0.000010	0.2214	0.0001	0.019	5.705
Troh 26	0.42	1.20	0.512554	0.000028	0.340441	0.000019	0.2231	0.0011	0.019	5.710
Trob 27	0.40	1 47	0.312318		0.340434	0.000010	0.2237	0.0005	0.019	5.576
Treh 29	0.40	1.42 1.27	0.312362	0.000057	0.340432	0.000016	0.2234	0.0005	0.018	5.507
Trob 20	0.44	1.34	0.512527	0.000037	0.346440	0.000010	0.2233	0.0004	0.019	5.362
1160_23	0.47	1.45	0.312345	0.000035	0.340433	0.000011	0.2200	0.0003	0.018	5.514

Table DR4. Sim Nd and U-Pa lootope results for Max Kiang monautin																																		
Analysis	്ട്ന (V)	<sup>os</sup> Nd (V)	""Nd""Nd	25E	""Ndi""Nd	25E	""Sm/""Nd	25E	sNd <sub>une</sub> '	25E	ENd <sub>2764</sub> 4	Eu/Eu*	Ce/Gd	Analysis	<sup>207</sup> Pb/ <sup>230</sup> U	25E	<sup>306</sup> Pb/ <sup>218</sup> U	25E	rho	258U/206Pb	25E	<sup>207</sup> Pb/ <sup>206</sup> Pb	25E	rho	<sup>208</sup> Pb/ <sup>238</sup> Th	2SE	<sup>207</sup> Pb/ <sup>335</sup> U ag	@ 25E	206Pb/258U age	2SE	208Pb/238Th age	25E	Pb/"Pb-age	250
28-Apr																																		
Thai_1	0.15	1.18	0.512640	0.000031	0.348435	0.000017	0.0892	0.0003	0.2	0.6	0.9	0.066	25.310	Thai_1	0.029	0.002	0.0043	0.0002	0.072	232.56	9.19	0.0495	0.0032	0.19527	0.00135	0.00005	28.7	2.3	27.7	1.1	27.2	1.1	400.0	660
Thai_2	0.18	1.12	0.512665	0.000035	0.348412	0.000023	0.1096	0.0005	0.7	0.7	1.4	0.049	17.140	Thai_2	0.030	0.002	0.0043	0.0002	0.118	232.56	9.19	0.0503	0.0032	0.18304	0.00136	0.00005	29.3	2.3	27.7	1.1	27.4	1.0	130.0	440
Thai_3	0.19	1.13	0.512644	0.000038	0.348428	0.000013	0.1142	0.0005	0.3	0.7	0.9	0.049	15.300	Thai_3	0.033	0.003	0.0043	0.0002	-0.100	230.95	9.07	0.0566	0.0033	0.40295	0.00134	0.00005	32.9	2.4	27.8	1.1	27.1	1.0	360.0	110
Thai_4	0.17	1.16	0.512650	0.000040	0.348417	0.000019	0.0991	0.0004	0.4	0.8	1.1	0.057	19.880	Thai_4	0.028	0.002	0.0042	0.0002	0.014	236.97	8.98	0.0487	0.0031	0.26153	0.00135	0.00005	27.7	2.2	27.1	1.0	27.3	1.1	60.0	110
Thai_5	0.18	1.18	0.512633	0.000041	0.348431	0.000021	0.1016	0.0010	0.1	0.8	0.7	0.050	18.550	Thai_5	0.030	0.003	0.0042	0.0002	0.192	240.38	9.82	0.0516	0.0038	0.17475	0.00132	0.00005	29.4	2.6	26.8	1.1	26.6	1.0	210.0	130
Thai_6	0.17	1.17	0.512632	0.000039	0.348405	0.000020	0.0998	0.0009	0.0	0.8	0.7	0.056	19.540	Thai_6	0.028	0.002	0.0044	0.0002	0.080	226.76	9.26	0.0484	0.0032	0.19061	0.00139	0.00005	28.1	2.3	28.4	1.1	28.0	1.1	50.0	440
Thai_7	0.15	1.16	0.512626	0.000030	0.348419	0.000021	0.0885	0.0004	-0.1	0.6	0.6	0.051	24.350	Thai_7	0.030	0.003	0.0043	0.0002	-0.017	234.19	9.87	0.0536	0.0038	0.43793	0.00134	0.00005	29.3	2.4	27.5	1.1	27.1	1.1	200-0	420
Thai_8	0.21	1.29	0.512629	0.000041	0.348432	0.000028	0.1112	0.0007	0.0	0.8	0.6	0.049	15.520	Thai_8	0.029	0.002	0.0045	0.0002	0.018	224.72	9.09	0.0482	0.0033	0.35775	0.00137	0.00005	28.4	2.3	28.6	1.1	27.6	1.1	40:0	669
Thai_9	0.16	1.22	0.512671	0.000032	0.348413	0.000021	0.0867	0.0003	0.8	0.6	1.5	0.064	25.320	Thai_9	0.028	0.002	0.0041	0.0002	0.092	241.55	9.92	0.049	0.0034	0.18248	0.00129	0.00005	27.9	2.3	26.6	1.1	26.1	1.0	70.0	620
Thai_10	0.18	1.22	0.512647	0.000034	0.348402	0.000023	0.0983	0.0009	0.3	0.7	1.0	0.055	19.050																					
29-Apr																																		
Thai_1	0.24	1.59	0.512626	0.000028	0.348419	0.000019	0.1032	0.0010	-0.1	0.5	0.6	0.055	17.940	Thai_1	0.057	0.004	0.0044	0.0001	0.175	227.79	5.19	0.0922	0.006	0.14117	0.00135	0.00003	55.5	3.6	28.2	0.7	27.2	0.6	1160.0	130
Thai_2	0.26	1.69	0.512631	0.000030	0.348414	0.000020	0.1056	0.0014	0.0	0.6	0.7	0.051	17.140	Thai_2	0.029	0.002	0.0042	0.0001	0.038	237.53	6.21	0.051	0.0033	0.27941	0.00132	0.00003	28.6	1.8	27.1	0.7	26.6	0.6	150.0	110
Thai_3	0.20	1.48	0.512638	0.000039	0.348429	0.000021	0.0945	0.0007	0.2	0.8	0.8	0.057	22.330	Thai_3	0.055	0.005	0.0044	0.0001	0.274	226.24	6.14	0.0906	0.0068	unnerer	0.00135	0.00003	53.5	4.2	28.4	0.8	27.3	0.7	2040-0	200
Thai_4	0.22	1.30	0.512640	0.000040	0.348415	0.000019	0.1146	0.0007	0.2	0.8	0.9	0.048	14.400	That_4	0.030	0.002	0.0044	0.0001	-0.031	228.83	5.76	0.0498	0.0031	0.63654	0.00138	0.00003	29.7	1.8	28.1	0.7	27.9	0.6	25040	000
Thai_5	0.22	1.39	0.512613	0.000047	0.348418	0.000020	0.1069	0.0014	-0.3	0.9	0.4	0.052	16.630	Thai_5	0.026	0.002	0.0041	0.0001	-0.039	241.66	5.72	0.0459	0.003	0.24245	0.00130	0.00003	25.5	1.7	26.6	0.6	26.2	0.6	-2010	000
Thai_6	0.21	1.51	0.512655	0.000035	0.348432	0.000020	0.0964	0.0011	0.5	0.7	1.2	0.058	20.290	Thai_6	0.028	0.002	0.0041	0.0001	0.019	246.91	6.10	0.0499	0.0035	0.22622	0.00131	0.00003	27.5	1.8	26.0	0.7	26.4	0.6	2200	920
Thai_7	0.20	1.44	0.512651	0.000022	0.348421	0.000017	0.0939	0.0006	0.4	0.4	1.1	0.057	21.030	Thai_7	0.031	0.003	0.0042	0.0001	0.015	235.85	6.67	0.05.98	0.0044	0.20724	0.00135	0.00003	30.2	2.4	27.3	0.8	27.3	0.7	110.0	1.50
The A	0.18	1.55	0.512634	0.000045	0.348410	0.000027	0.0870	0.0003	0.1	0.9	0.8	0.064	25.520	Thai o	0.030	0.003	0.0041	0.0001	0.022	243.70	0.04	0.0555	0.0047	0.25004	0.00138	0.00003	30.1	2.5	20.2	0.7	27.9	0.7	100.0	140
Their 10	0.19	1.35	0.512047	0.000024	0.348433	0.0000020	0.0920	0.0003	0.5	0.0	1.0	0.060	21.650	The 10	0.031	0.003	0.0041	0.0001	0.056	242.72	6.21	0.0536	0.0044	0.14301	0.00137	0.00004	30.5	2.5	20.5	0.8	27.0	0.8	520.0	140
Their 11	0.19	1.66	0.512624	0.000045	0.249436	0.0000010	0.0865	0.0001	0.5	0.9	1.2	0.055	25 700	Th 11	0.020	0.002	0.0042	0.0001	0.092	227.52	6 77	0.062	0.0034	0.02065	0.00127	0.000004	30.9	2.4	37.1	0.9	17.6	0.7	490.0	440
Their 12	0.10	1.49	0.513649	0.0000325	0.249410	0.0000019	0.0876	0.0002	0.0	0.7	11	0.063	24.040	Th :: 12	0.021	0.002	0.0042	0.0001	0.002	226.96	6.67	0.0522	0.0045	0.202	0.00126	0.00003	21.2	2.6	37.2	0.0	27.0	0.7	420.0	440
al_12	0.19	1.40	0.312043	0.000035	0.348419	0.000020	0.08/6	0.0002	0.4	w.7	***	0.003	44.940		0.031	0.005	0.0042	0.0001	0.00/	A.A.A.60	0.07	0.0038	0.0045	0.000	0.00130	0.00003	31.3	A-3	A7-3	0.8	****	w.7		
				mean 25D	0.512641 0.000028	1																												