## Expanded Methods

## Imaging

Quartz crystals bearing melt inclusions were selected randomly for tomographic imaging from crystal separates. All imaging was conducted on the GSECARS-13 bending magnet beamline of the Advanced Photon Source (APS) at Argonne National Laboratory (Chicago, IL), following the procedures of Pamukcu et al. (2013). The data provided here were obtained from five Ohakuri-Mamaku (OHK, MAM) ignimbrite crystals (Bégué et al., 2014), fifteen phase 10 (ORN-067) and five phase 1 (P1577) airfall Oruanui crystals (Wilson, 2001), and thirteen Bishop crystals (BB08: airfall F6/F7, BC17: ignimbrite Ig2E, F815: airfall F8; Wilson and Hildreth, 1997).

To compare melt inclusion faceting times and growth rates with those from Ti diffusion chronometry, we made measurements using both methods on a subset of Ohakuri-Mamaku crystals. Initially, $\sim 80$ quartz crystals were selected randomly from Ohakuri-Mamaku pumice clasts and imaged with tomography. After inspecting these tomograms, we selected $\sim 35$ of the crystals to image for Ti zoning. Crystals were selected based on: (a) if they contained fullyenclosed inclusions of resolvable size (the image processing procedures can only be used on fully-enclosed inclusions $>10$ pixels in diameter), and (b) how many inclusions they contained (we aimed to expose as many inclusions as possible in 2-D sectioning). Each crystal was mounted individually in epoxy (c-axis vertical), sectioned to expose melt inclusions, and imaged with cathodolminescence (CL) on a scanning electron microscope (SEM). We aimed to assess times from boundaries as close to or containing melt inclusions of interest. However, at times imaging revealed complex zoning and artifacts due to unexposed melt inclusions (see below, Fig.

DR4), and we avoided these areas for the sake of obtaining the best possible comparison between faceting and diffusion chronometry. In some cases, melt inclusions of interest were unfortunately polished through, making it difficult or impossible to know which zones contained them. Ultimately, five of the imaged crystals provided useful results for comparison.

Previous work has shown that CL intensity can be a good proxy for Ti contents in quartz (Cherniak et al., 2007; Spear and Wark, 2009; Gualda et al., 2012a; Leeman et al., 2012), and we verified this in a subset of our crystals by comparing CL images with Ti maps obtained by x-ray microprobe on the GSECARS-13 insertion device beamline at APS. We find that the large variations in CL zoning that are most relevant to our time calculations correlate well with Ti ; however, subtle variations (i.e. fine oscillatory zoning) do not (Fig. DR1). Given the correlation between Ti and CL in our samples, and the fact that CL imaging on an SEM provides considerably better spatial resolution than the x-ray microprobe used for Ti mapping, we use CL intensity variations to derive crystallization times.

In CL imaging, the incident electron beam energy constrains both the signal-to-noise ratio (better at higher energy) and smoothing due to electron scattering within the sample (better at lower energy). We find that a 15 kV beam provides sufficient contrast and adequate spatial resolution for the timescales of interest in these crystals (Fig. DR1). We note that unexposed portions of melt inclusions can affect CL intensity, creating noticeably darker or lighter areas inconsistent with other zoning, and we avoided these areas in our analysis (Fig. DR4).

## Melt Inclusion Faceting \& Diffusion Chronometry

To obtain timescale estimates from these two approaches, we use the equations developed and explained in detail by Gualda et al. (2012a; see also Fig. DR1). We use temperatures of $780^{\circ} \mathrm{C}$ (Ohakuri-Mamaku; Bégué et al., 2014), $770^{\circ} \mathrm{C}$ (Oruanui; Allan et al.,
2013) and $750{ }^{\circ} \mathrm{C}$ (Bishop Tuff; Cherniak et al., 2007) for T and to calculate $\mathrm{D}_{\mathrm{Si}}$ and $\mathrm{D}_{\mathrm{Ti}}$ (Baker, 1991; Gualda et al. 2012a). The $\Delta \mathrm{V}$ parameter used for faceting calculations is the total volume of material moved during the faceting process and is calculated from the number of pixels that protrude from an ellipsoid of the same volume, which is determined during image processing. All inclusions used for faceting calculations are fully-enclosed and of resolvable size in tomographic images. For a given Oruanui or Bishop crystal, all inclusions that fulfilled these requirements were assessed. For Ohakuri-Mamaku, the inclusions selected for analysis fulfilled these requirements but were also those exposed when crystals were sectioned after tomographic imaging. This totals to: 15 inclusions from Ohakuri-Mamaku crystals, 44 inclusions from Oruanui crystals, and 107 inclusions from Bishop Tuff crystals.

For time estimates from diffusion chronometry, we collect 11 parallel diffusion profiles (5 on each side of the originally drawn profile) spaced in one pixel increments. We then calculate timescales from each individual profile and an average profile. We remove any individual profiles that appear to be severely affected by aberrations in the image (e.g. extraneous bright or dark pixels - noise) or interact with other features in the crystal that affect intensities (e.g. melt inclusions). We report estimates from the average profile. Boundaries in Ohakuri-Mamaku crystals used for diffusion chronometry were: (a) those that showed distinct CL contrast on either side, as these are correlated with Ti , (b) traceable through much of the image, and (c) not irregular (i.e. not wavy). Ideally, boundaries of zones that contained melt inclusions used for faceting calculations were also assessed.

As noted in the main text, the error calculations for our timescale estimates take a $60^{\circ} \mathrm{C}$ temperature range into account. If the system cools enough that diffusion is unable to proceed (e.g. the system enters the subsolidus realm), the processes being measured will essentially stop.

Our calculations do not take such extreme variations into account; however, in this scenario, the resultant timescales are still maxima for the accumulation of the final eruptible melt-rich magma body, which is what we focus on here. In other words, melt inclusion faceting and diffusional relaxation of compositional profiles will proceed immediately after entrapment and for any time spent at magmatic temperatures. Consequently, the time estimates retrieved from these features would be equal to (no time spent subsolidus) or overestimate (time spent subsolidus) the final accumulation time. If the temperature of the system increased but did not result in resorption of melt inclusions or boundaries, the times we would retrieve would be shorter than the real times; however, we do not see strong indications of such large temperature variations in our crystals (e.g. extremely bright CL areas) that are not accounted for by the $60^{\circ} \mathrm{C}$ temperature range included in the error calculations.

Growth rates were calculated using the calculated time and nearest distance to the crystal edge for a given melt inclusion (determined in 3-D from tomographic images) or zone boundary (determined in 2-D from CL images). In some cases, crystals imaged with tomography were not euhedral, such that the nearest edge to a given melt inclusion calculated by the image processing software was a broken edge of the crystal. We do not include these values in our dataset. In the case of CL images, the nearest edge to a given inclusion or boundary may be one in the third dimension not visible in the 2-D image.

## Rhyolite-MELTS modeling

Rhyolite-MELTS calculations were performed at constant pressure, in equilibrium mode, with oxygen fugacity fixed at the $\mathrm{Ni}-\mathrm{NiO}$ buffer, under water-saturated conditions. Crystallization pressures used for the simulations were based on previous work on these systems, which is summarized by Gualda and Ghiorso (2013).

## REFERENCES CITED

Gualda, G. A. R., and Ghiorso, M. S., 2013, Low pressure origin of high-silica rhyolites: Journal of Geology, v. 121, p. 537-545, doi: 10.1086/671395.

## Example schematic of melt inclusion time plot



Figure DR1. Schematic showing evolution of melt inclusion shape through time. Fully faceted inclusions will lie on the $1: 1$ line, at which the time to achieve full faceting is equal to the time calculated from image processing (i.e., current degree of faceting). At time $=0$, an inclusion will lie on the $x$-axis (no faceting has occurred), and as time passes, the inclusion will move vertically from the initial position on the $x$-axis. The initial position on the $x$-axis is a function of the inclusion size - smaller inclusions will facet more rapidly than large inclusions (less material to diffuse to achieve full faceting), so they will become fully faceted in less time. Equation used to calculate faceting time is from Gualda et al. 2012a.

Variables in faceting time calculation
R : Ideal gas constant
T : temperature
D: diffusion coefficient for Si in melt
$\mathrm{C}_{0}$ : solubility of a particle of infinite radius
$\sigma$ : surface free energy
$\Omega$ : molar volume of phase of interest
$\Delta \mathrm{V}$ : volume of melt inclusion that is moved in faceting processes (determined from tomography; see text for details)


Figure DR1, continued. Faceting times for individual eruptive units studied


Figure DR1, continued. Time estimates for ORN-067 over a range of temperatures ( $\pm 30^{\circ} \mathrm{C}$ ).


Figure DR2. Quartz zoning, melt inclusion faceting and diffusional relaxation times from an Ohakuri-Mamaku crystal. (A) Titanium map of quartz crystal in (B). (B) CL image of crystal with times from faceting (black melt inclusions) and diffusional relaxation (boundary highlighted by white line). Red box indicates area characterized in (C). (C) Comparison of diffusion profiles obtained from CL images collected with varying beam energies. Dashed lines represent profile portion fit for timescales estimates (noted in yellow).

Figure DR3. Cathodoluminescence images of Ohakuri-Mamaku quartz crystals, with timescale and growth rate estimates from melt inclusion faceting and diffusion chronometry. Scale bars are $200 \mu \mathrm{~m}$.


| D125b_10 | Time (a) | Time (s) | Distance to <br> Nearest Edge <br> (pixel) | Image <br> Resolution <br> $(\boldsymbol{\mu m} /$ pixel $)$ | Distance to <br> Nearest Edge <br> $(\mathbf{m})$ | Growth <br> Rate <br> $(\mathbf{m} / \mathbf{s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MI 15 <br> (tomography) | 16 | $5.05 \times 10^{8}$ | 101.4 | 2.76 | $2.80 \times 10^{-4}$ | $5.55 \times 10^{-13}$ |
| MI 18 | 18 | $5.68 \times 10^{8}$ | 113.5 | 2.76 | $3.13 \times 10^{-4}$ | $5.52 \times 10^{-13}$ |
| (tomography) | 31 |  |  |  |  |  |
| Diffusion <br> Profile <br> (CL image) | 31 | $9.78 \times 10^{8}$ | 32.3 | 2.06 | $6.66 \times 10^{-5}$ | $6.81 \times 10^{-14}$ |

Figure DR3, continued. Cathodoluminescence images of Ohakuri-Mamaku quartz crystals, with timescale and growth rate estimates from melt inclusion faceting and diffusion chronometry. Scale bars are $200 \mu \mathrm{~m}$.


Figure DR3, continued. Cathodoluminescence images of Ohakuri-Mamaku quartz crystals, with timescale and growth rate estimates from melt inclusion faceting and diffusion chronometry. Scale bars are $200 \mu \mathrm{~m}$.


Figure DR3, continued. Cathodoluminescence images of Ohakuri-Mamaku quartz crystals, with timescale and growth rate estimates from melt inclusion faceting and diffusion chronometry. Scale bars are $200 \mu \mathrm{~m}$.

|  |  | 29 a <br> MI2 <br> 30 a <br> 24 a <br> MI3 89 a |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OHK-IGN2_7 | Time (a) | Time (s) | Distance to Nearest Edge (pixel) | Image Resolution ( $\mu \mathrm{m} / \mathrm{pixel}$ ) | Distance to Nearest Edge (m) | Growth Rate (m/s) |
| MI 1 (tomography) | 29 | $9.15 \times 10^{8}$ | 67.8 | 2.76 | $1.87 \times 10^{-4}$ | $2.05 \times 10^{-13}$ |
| MI 2 <br> (tomography) | 30 | $9.46 \times 10^{8}$ | 91.5 | 2.76 | $2.53 \times 10^{-4}$ | $2.67 \times 10^{-13}$ |
| MI 3 (tomography) | 89 | $2.81 \times 10^{9}$ | 89.7 | 2.76 | $2.47 \times 10^{-4}$ | $8.82 \times 10^{-14}$ |
| Diffusion Profile (CL image) | 24 | $7.57 \times 10^{8}$ | 115.4 | 1.89 | $2.18 \times 10^{-4}$ | $2.88 \times 10^{-13}$ |

Figure DR3, continued. Cathodoluminescence images of Ohakuri-Mamaku quartz crystals, with timescale and growth rate estimates from melt inclusion faceting and diffusion chronometry. Scale bars are $200 \mu \mathrm{~m}$.


| FB11-Ma21_4 | Time (a) | Time (s) | Distance to <br> Nearest Edge <br> (pixel) | Image <br> Resolution <br> $(\boldsymbol{\mu m} /$ pixel) | Distance to <br> Nearest Edge <br> $(\mathbf{m})$ | Growth <br> Rate <br> $(\mathbf{m} / \mathbf{s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MI 1 <br> (tomography) | 13 | $4.10 \times 10^{8}$ | 57.3 | 2.76 | $1.58 \times 10^{-4}$ | $3.86 \times 10^{-13}$ |
| MI 2 <br> (tomography) | 14 | $4.42 \times 10^{8}$ | 45.0 | 2.76 | $1.24 \times 10^{-4}$ | $2.18 \times 10^{-13}$ |
| MI 3 <br> (tomography) | 15 | $4.73 \times 10^{8}$ | 69.2 | 2.76 | $1.91 \times 10^{-4}$ | $4.04 \times 10^{-13}$ |
| MI 4 <br> (tomography) | 11 | $3.47 \times 10^{8}$ | 39.7 | 2.76 | $1.10 \times 10^{-4}$ | $3.16 \times 10^{-13}$ |
| MI 5 <br> (tomography) | 54 | $1.70 \times 10^{9}$ | 65.5 | 2.76 | $1.81 \times 10^{-4}$ | $1.06 \times 10^{-13}$ |
| MI 6 <br> (tomography) | 24 | $7.57 \times 10^{8}$ | 66.2 | 2.76 | $1.83 \times 10^{-4}$ | $2.42 \times 10^{-13}$ |
| Diffusion <br> Profile <br> (CL image) | 40 | $1.26 \times 10^{9}$ | 32.3 | 2.06 | $6.66 \times 10^{-5}$ | $5.28 \times 10^{-14}$ |



Figure DR4. CL images and tomogram slices of quartz crystal. (A, B) CL image and tomogram slice, respectively, of the same quartz crystal at approximately the same position in the grain. (C, D) CL images of a quartz crystal successively polished to expose occluded melt inclusion (see region marked by red triangle). Unexposed melt inclusions appear to affect CL intensity in some cases (dark inconsistent swaths, bright halos around melt inclusions). Times from faceting and diffusional relaxation are given in yellow. Scale bars $=200 \mu \mathrm{~m}$.

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P1577_4
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|  | $\Delta \mathrm{V}$ | $\mathrm{um}^{3}$ | $\mathrm{m}^{3}$ | T (K) | $\Delta t(s)$ | $\Delta \mathrm{t}$ ( $\mathbf{y r}$ ) | Distance to Nearest Edge (m) | Growth Rate (m/s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MI1 | 1226.51 | $2.61 \mathrm{E}+04$ | $2.61 \mathrm{E}-14$ | 1043.15 | $2.27 \mathrm{E}+09$ | 72 | $2.13 \mathrm{E}-04$ | $9.41 \mathrm{E}-14$ |
| MI4 | 190.00 | $4.04 \mathrm{E}+03$ | $4.04 \mathrm{E}-15$ | 1043.15 | $3.54 \mathrm{E}+09$ | 112 |  |  |
| MI11 | 26.00 | $5.53 \mathrm{E}+02$ | $5.53 \mathrm{E}-16$ | 1043.15 | $1.96 \mathrm{E}+09$ | 62 | $1.12 \mathrm{E}-04$ | $5.71 \mathrm{E}-14$ |

P1577_6

|  | $\boldsymbol{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\boldsymbol{\Delta t}(\mathbf{s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| MI3 | 315.666 | $6.71 \mathrm{E}+03$ | $6.71 \mathrm{E}-15$ | 1043.15 | $5.84 \mathrm{E}+08$ |
| MI8 | 6041.18 | $1.28 \mathrm{E}+05$ | $1.28 \mathrm{E}-13$ | 1043.15 | $1.12 \mathrm{E}+10$ |
| MI9 | 568.501 | $1.21 \mathrm{E}+04$ | $1.21 \mathrm{E}-14$ | 1043.15 | $1.05 \mathrm{E}+09$ |
| MI10 | 298.5 | $6.34 \mathrm{E}+03$ | $6.34 \mathrm{E}-15$ | 1043.15 | $5.52 \mathrm{E}+08$ |


| $\Delta \mathbf{t} \mathbf{( y r})$ |  |  |
| :---: | :---: | :---: |
| $\mathbf{1 9}$ | $1.04 \mathrm{E}-04$ | $4.48 \mathrm{E}-13$ |
| $\mathbf{3 5 4}$ | $1.90 \mathrm{E}-04$ | $4.25 \mathrm{E}-14$ |
| $\mathbf{3 3}$ | $1.80 \mathrm{E}-04$ | $4.28 \mathrm{E}-13$ |
| $\mathbf{1 7}$ | $1.77 \mathrm{E}-04$ | $8.00 \mathrm{E}-13$ |

## P1577_8

|  | $\boldsymbol{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t}(\mathbf{s})$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| MI2 | 516.83 | $1.10 \mathrm{E}+04$ | $1.10 \mathrm{E}-14$ | 1043.15 | $9.56 \mathrm{E}+08$ |
| MI5 | 305.50 | $6.49 \mathrm{E}+03$ | $6.49 \mathrm{E}-15$ | 1043.15 | $5.65 \mathrm{E}+08$ |
| MI8 | 802.67 | $1.71 \mathrm{E}+04$ | $1.71 \mathrm{E}-14$ | 1043.15 | $1.48 \mathrm{E}+09$ |
| MI9 | 593.00 | $1.26 \mathrm{E}+04$ | $1.26 \mathrm{E}-14$ | 1043.15 | $1.10 \mathrm{E}+09$ |


| $\Delta \mathbf{t}(\mathbf{y r})$ |  |  |
| :---: | :---: | :---: |
| $\mathbf{3 0}$ |  |  |
| $\mathbf{1 8}$ |  |  |
| $\mathbf{4 7}$ | $2.20 \mathrm{E}-04$ | $2.01 \mathrm{E}-13$ |

## P1577_12

MI1

| $\Delta \mathbf{V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\boldsymbol{\Delta t}(\mathbf{s})$ |
| :---: | :---: | :---: | :---: | :---: |
| 669.16 | $1.42 \mathrm{E}+04$ | $1.42 \mathrm{E}-14$ | 1043.15 | $1.24 \mathrm{E}+09$ |

$\Delta t(\mathbf{y r})$
39
8.79E-05
7.10E-14

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|  | $\Delta \mathbf{V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t}(\mathbf{s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| MI1 | 332.67 | $7.07 \mathrm{E}+03$ | $7.07 \mathrm{E}-15$ | 1043.15 | $6.15 \mathrm{E}+08$ |
| MI5 | 352.67 | $7.50 \mathrm{E}+03$ | $7.50 \mathrm{E}-15$ | 1043.15 | $6.52 \mathrm{E}+08$ |
| MI6 | 536.00 | $1.14 \mathrm{E}+04$ | $1.14 \mathrm{E}-14$ | 1043.15 | $9.91 \mathrm{E}+08$ |
| MI10 | 334.17 | $7.10 \mathrm{E}+03$ | $7.10 \mathrm{E}-15$ | 1043.15 | $6.18 \mathrm{E}+08$ |
| MI11 | 503.34 | $1.07 \mathrm{E}+04$ | $1.07 \mathrm{E}-14$ | 1043.15 | $9.31 \mathrm{E}+08$ |
| MI12 | 296.17 | $6.29 \mathrm{E}+03$ | $6.29 \mathrm{E}-15$ | 1043.15 | $5.48 \mathrm{E}+08$ |
| MI13 | 162.67 | $3.46 \mathrm{E}+03$ | $3.46 \mathrm{E}-15$ | 1043.15 | $3.01 \mathrm{E}+08$ |
| MI14 | 1679.33 | $3.57 \mathrm{E}+04$ | $3.57 \mathrm{E}-14$ | 1043.15 | $3.11 \mathrm{E}+09$ |
| MI17 | 292.50 | $6.22 \mathrm{E}+03$ | $6.22 \mathrm{E}-15$ | 1043.15 | $5.41 \mathrm{E}+08$ |
| MI19 | 290.50 | $6.17 \mathrm{E}+03$ | $6.17 \mathrm{E}-15$ | 1043.15 | $5.37 \mathrm{E}+08$ |
| MI20 | 416.00 | $8.84 \mathrm{E}+03$ | $8.84 \mathrm{E}-15$ | 1043.15 | $7.69 \mathrm{E}+08$ |
| MI22 | 1657.17 | $3.52 \mathrm{E}+04$ | $3.52 \mathrm{E}-14$ | 1043.15 | $3.07 \mathrm{E}+09$ |
| MI24 | 1565.50 | $3.33 \mathrm{E}+04$ | $3.33 \mathrm{E}-14$ | 1043.15 | $2.90 \mathrm{E}+09$ |
| MI25 | 157.00 | $3.34 \mathrm{E}+03$ | $3.34 \mathrm{E}-15$ | 1043.15 | $2.90 \mathrm{E}+08$ |
| MI26 | 841.84 | $1.79 \mathrm{E}+04$ | $1.79 \mathrm{E}-14$ | 1043.15 | $1.56 \mathrm{E}+09$ |

$\Delta t(\mathbf{y r})$
19
21
31
20
30
17
10
98
17
17
24
97
92
9
49

| $1.98 \mathrm{E}-04$ | $3.22 \mathrm{E}-13$ |
| :--- | :--- |
| $1.57 \mathrm{E}-04$ | $2.42 \mathrm{E}-13$ |
| $2.00 \mathrm{E}-04$ | $2.02 \mathrm{E}-13$ |
| $1.98 \mathrm{E}-04$ | $3.21 \mathrm{E}-13$ |
| $1.44 \mathrm{E}-04$ | $1.55 \mathrm{E}-13$ |
| $1.15 \mathrm{E}-04$ | $2.10 \mathrm{E}-13$ |
| $2.82 \mathrm{E}-04$ | $9.39 \mathrm{E}-13$ |
| $1.25 \mathrm{E}-04$ | $4.04 \mathrm{E}-14$ |
| $1.20 \mathrm{E}-04$ | $2.21 \mathrm{E}-13$ |
| $1.20 \mathrm{E}-04$ | $2.23 \mathrm{E}-13$ |
| $9.10 \mathrm{E}-05$ | $1.18 \mathrm{E}-13$ |
| $7.50 \mathrm{E}-05$ | $2.45 \mathrm{E}-14$ |
| $2.36 \mathrm{E}-04$ | $8.17 \mathrm{E}-14$ |
| $1.35 \mathrm{E}-04$ | $4.65 \mathrm{E}-13$ |
| $1.35 \mathrm{E}-04$ | $8.67 \mathrm{E}-14$ |

ORN-067_4

|  | $\boldsymbol{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t}(\mathbf{s})$ | $\Delta \mathbf{t}(\mathbf{y r})$ |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MI1 | 468.17 | $9.95 \mathrm{E}+03$ | $9.95 \mathrm{E}-15$ | 1043.15 | $8.66 \mathrm{E}+08$ | $\mathbf{2 7}$ | $1.38 \mathrm{E}-04$ | $1.59 \mathrm{E}-13$ |
| MI3 | 377.67 | $8.03 \mathrm{E}+03$ | $8.03 \mathrm{E}-15$ | 1043.15 | $6.99 \mathrm{E}+08$ | $\mathbf{2 2}$ | $1.34 \mathrm{E}-04$ | $1.92 \mathrm{E}-13$ |

## ORN-067_5

|  | $\Delta \mathbf{V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t}(\mathbf{s})$ | $\Delta \mathbf{t}(\mathbf{y r})$ |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MI2 | 330.50 | $7.02 \mathrm{E}+03$ | $7.02 \mathrm{E}-15$ | 1043.15 | $6.11 \mathrm{E}+08$ | $\mathbf{1 9}$ | $1.22 \mathrm{E}-04$ | $2.00 \mathrm{E}-13$ |
| MI3 | 1938.67 | $4.12 \mathrm{E}+04$ | $4.12 \mathrm{E}-14$ | 1043.15 | $3.59 \mathrm{E}+09$ | $\mathbf{1 1 4}$ | $2.43 \mathrm{E}-04$ | $6.79 \mathrm{E}-14$ |
| MI4 | 280.67 | $5.97 \mathrm{E}+03$ | $5.97 \mathrm{E}-15$ | 1043.15 | $5.19 \mathrm{E}+08$ | $\mathbf{1 6}$ | $1.07 \mathrm{E}-04$ | $2.06 \mathrm{E}-13$ |
| MI6 | 145.17 | $3.09 \mathrm{E}+03$ | $3.09 \mathrm{E}-15$ | 1043.15 | $2.69 \mathrm{E}+08$ | $\mathbf{9}$ | $2.30 \mathrm{E}-04$ | $8.57 \mathrm{E}-13$ |
| MI7 | 1759.15 | $3.74 \mathrm{E}+04$ | $3.74 \mathrm{E}-14$ | 1043.15 | $3.25 \mathrm{E}+09$ | $\mathbf{1 0 3}$ | $2.21 \mathrm{E}-04$ | $6.78 \mathrm{E}-14$ |


| MI8 | 412.00 | $8.76 \mathrm{E}+03$ | $8.76 \mathrm{E}-15$ | 1043.15 | $7.62 \mathrm{E}+08$ | $\mathbf{2 4}$ | $8.50 \mathrm{E}-05$ | $1.12 \mathrm{E}-13$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MI10 | 352.67 | $7.50 \mathrm{E}+03$ | $7.50 \mathrm{E}-15$ | 1043.15 | $6.52 \mathrm{E}+08$ | $\mathbf{2 1}$ | $1.02 \mathrm{E}-04$ | $1.56 \mathrm{E}-13$ |

ORN-067_6

|  | $\boldsymbol{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\mathbf{\Delta t}(\mathbf{s})$ | $\boldsymbol{\Delta t}(\mathbf{y r})$ |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MI1 | 351.16 | $7.46 \mathrm{E}+03$ | $7.46 \mathrm{E}-15$ | 1043.15 | $6.50 \mathrm{E}+08$ | $\mathbf{2 1}$ | $1.06 \mathrm{E}-04$ | $1.63 \mathrm{E}-13$ |
| M12 | 150.17 | $3.19 \mathrm{E}+03$ | $3.19 \mathrm{E}-15$ | 1043.15 | $2.78 \mathrm{E}+08$ | $\mathbf{9}$ | $8.68 \mathrm{E}-05$ | $3.13 \mathrm{E}-13$ |
| MI3 | 183.33 | $3.90 \mathrm{E}+03$ | $3.90 \mathrm{E}-15$ | 1043.15 | $3.39 \mathrm{E}+08$ | $\mathbf{1 1}$ | $8.93 \mathrm{E}-05$ | $2.64 \mathrm{E}-13$ |
| MI4 | 203.33 | $4.32 \mathrm{E}+03$ | $4.32 \mathrm{E}-15$ | 1043.15 | $3.76 \mathrm{E}+08$ | $\mathbf{1 2}$ | $8.91 \mathrm{E}-05$ | $2.37 \mathrm{E}-13$ |
| MI5 | 187.50 | $3.99 \mathrm{E}+03$ | $3.99 \mathrm{E}-15$ | 1043.15 | $3.47 \mathrm{E}+08$ | $\mathbf{1 1}$ | $1.01 \mathrm{E}-04$ | $2.91 \mathrm{E}-13$ |

ORN-067_11

|  | $\boldsymbol{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t}(\mathbf{s})$ | $\Delta \mathbf{t}(\mathbf{y r})$ |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | ---: |
| MI2 | 134.67 | $2.86 \mathrm{E}+03$ | $2.86 \mathrm{E}-15$ | 1043.15 | $2.49 \mathrm{E}+08$ | $\mathbf{8}$ | $7.98 \mathrm{E}-05$ | $3.21 \mathrm{E}-13$ |
| MI4 | 140.50 | $2.99 \mathrm{E}+03$ | $2.99 \mathrm{E}-15$ | 1043.15 | $2.60 \mathrm{E}+08$ | $\mathbf{8}$ | $6.99 \mathrm{E}-05$ | $2.69 \mathrm{E}-13$ |

ORN-067_15

|  | $\Delta \mathbf{V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t}(\mathbf{s})$ | $\Delta \mathbf{t}(\mathbf{y r})$ |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | ---: |
| MI3 | 223.17 | $4.74 \mathrm{E}+03$ | $4.74 \mathrm{E}-15$ | 1043.15 | $4.13 \mathrm{E}+08$ | $\mathbf{1 3}$ | $1.06 \mathrm{E}-04$ | $2.57 \mathrm{E}-13$ |

F815-x1827

|  | $\boldsymbol{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t} \mathbf{( \mathbf { s } )}$ | $\mathbf{\Delta t} \mathbf{( \mathbf { y r } )}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M15 | 574.50 | $1.22 \mathrm{E}+04$ | $1.22 \mathrm{E}-14$ | 1023.15 | $1.38 \mathrm{E}+09$ | $\mathbf{4 4}$ | $1.58 \mathrm{E}-04$ | $1.14 \mathrm{E}-13$ |
| MI6 | 39.00 | $8.29 \mathrm{E}+02$ | $8.29 \mathrm{E}-16$ | 1023.15 | $9.40 \mathrm{E}+07$ | $\mathbf{3}$ | $2.60 \mathrm{E}-04$ | $2.77 \mathrm{E}-12$ |
| MI7 | 515.50 | $1.10 \mathrm{E}+04$ | $1.10 \mathrm{E}-14$ | 1023.15 | $1.24 \mathrm{E}+09$ | $\mathbf{3 9}$ | $2.28 \mathrm{E}-04$ | $1.84 \mathrm{E}-13$ |
| M18 | 319.67 | $6.79 \mathrm{E}+03$ | $6.79 \mathrm{E}-15$ | 1023.15 | $7.70 \mathrm{E}+08$ | $\mathbf{2 4}$ |  |  |
| MI9 | 168.50 | $3.58 \mathrm{E}+03$ | $3.58 \mathrm{E}-15$ | 1023.15 | $4.06 \mathrm{E}+08$ | $\mathbf{1 3}$ |  |  |
| MI12 | 1874.33 | $3.98 \mathrm{E}+04$ | $3.98 \mathrm{E}-14$ | 1023.15 | $4.52 \mathrm{E}+09$ | $\mathbf{1 4 3}$ | $3.52 \mathrm{E}-04$ | $7.79 \mathrm{E}-14$ |
| MI14 | 329.00 | $6.99 \mathrm{E}+03$ | $6.99 \mathrm{E}-15$ | 1023.15 | $7.93 \mathrm{E}+08$ | $\mathbf{2 5}$ | $2.89 \mathrm{E}-04$ | $3.65 \mathrm{E}-13$ |
| MI15 | 888.66 | $1.89 \mathrm{E}+04$ | $1.89 \mathrm{E}-14$ | 1023.15 | $2.14 \mathrm{E}+09$ | $\mathbf{6 8}$ | $5.01 \mathrm{E}-04$ | $2.34 \mathrm{E}-13$ |
| MI16 | 262.17 | $5.57 \mathrm{E}+03$ | $5.57 \mathrm{E}-15$ | 1023.15 | $6.32 \mathrm{E}+08$ | $\mathbf{2 0}$ | $5.09 \mathrm{E}-04$ | $8.07 \mathrm{E}-13$ |
| MI17 | 1181.34 | $2.51 \mathrm{E}+04$ | $2.51 \mathrm{E}-14$ | 1023.15 | $2.85 \mathrm{E}+09$ | $\mathbf{9 0}$ | $4.47 \mathrm{E}-04$ | $1.57 \mathrm{E}-13$ |
| MI18 | 2462.66 | $5.23 \mathrm{E}+04$ | $5.23 \mathrm{E}-14$ | 1023.15 | $5.93 \mathrm{E}+09$ | $\mathbf{1 8 8}$ | $2.64 \mathrm{E}-04$ | $4.94 \mathrm{E}-13$ |
| MI19 | 221.50 | $4.71 \mathrm{E}+03$ | $4.71 \mathrm{E}-15$ | 1023.15 | $5.34 \mathrm{E}+08$ | $\mathbf{1 7}$ |  |  |
| MI21 | 130.50 | $2.77 \mathrm{E}+03$ | $2.77 \mathrm{E}-15$ | 1023.15 | $3.14 \mathrm{E}+08$ | $\mathbf{1 0}$ |  |  |
| MI22 | 1057.50 | $2.25 \mathrm{E}+04$ | $2.25 \mathrm{E}-14$ | 1023.15 | $2.55 \mathrm{E}+09$ | $\mathbf{8 1}$ | $3.39 \mathrm{E}-04$ | $1.33 \mathrm{E}-13$ |
| MI24 | 106.17 | $2.26 \mathrm{E}+03$ | $2.26 \mathrm{E}-15$ | 1023.15 | $2.56 \mathrm{E}+08$ | $\mathbf{8}$ | $3.40 \mathrm{E}-04$ | $4.17 \mathrm{E}-13$ |
| MI25 | 338.84 | $7.20 \mathrm{E}+03$ | $7.20 \mathrm{E}-15$ | 1023.15 | $8.17 \mathrm{E}+08$ | $\mathbf{2 6}$ | $2.98 \mathrm{E}-04$ | $1.38 \mathrm{E}-13$ |
| MI26 | 895.33 | $1.90 \mathrm{E}+04$ | $1.90 \mathrm{E}-14$ | 1023.15 | $2.16 \mathrm{E}+09$ | $\mathbf{6 8}$ |  |  |

F815-x1830

|  | $\boldsymbol{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t}(\mathbf{s})$ | $\Delta \mathbf{t}(\mathbf{y r})$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M12 | 540.50 | $1.15 \mathrm{E}+04$ | $1.15 \mathrm{E}-14$ | 1023.15 | $1.30 \mathrm{E}+09$ | $\mathbf{4 1}$ | $1.89 \mathrm{E}-04$ | $1.45 \mathrm{E}-13$ |
| MI4 | 6495.28 | $1.38 \mathrm{E}+05$ | $1.38 \mathrm{E}-13$ | 1023.15 | $1.57 \mathrm{E}+10$ | $\mathbf{4 9 6}$ | $2.06 \mathrm{E}-04$ | $1.32 \mathrm{E}-14$ |
| MI11 | 222.17 | $4.72 \mathrm{E}+03$ | $4.72 \mathrm{E}-15$ | 1023.15 | $5.35 \mathrm{E}+08$ | $\mathbf{1 7}$ | $2.11 \mathrm{E}-04$ | $3.95 \mathrm{E}-13$ |
| MI12 | 435.00 | $9.25 \mathrm{E}+03$ | $9.25 \mathrm{E}-15$ | 1023.15 | $1.05 \mathrm{E}+09$ | $\mathbf{3 3}$ | $2.20 \mathrm{E}-04$ | $2.10 \mathrm{E}-13$ |

## F815-x1831

|  | $\boldsymbol{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t}(\mathbf{s})$ | $\boldsymbol{\Delta t}(\mathbf{y r})$ |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M13 | 205.17 | $4.36 \mathrm{E}+03$ | $4.36 \mathrm{E}-15$ | 1023.15 | $4.94 \mathrm{E}+08$ | $\mathbf{1 6}$ | $2.03 \mathrm{E}-04$ | $4.11 \mathrm{E}-13$ |
| MI7 | 517.00 | $1.10 \mathrm{E}+04$ | $1.10 \mathrm{E}-14$ | 1023.15 | $1.25 \mathrm{E}+09$ | $\mathbf{3 9}$ | $1.73 \mathrm{E}-04$ | $1.39 \mathrm{E}-13$ |
| MI8 | 1691.83 | $3.60 \mathrm{E}+04$ | $3.60 \mathrm{E}-14$ | 1023.15 | $4.08 \mathrm{E}+09$ | $\mathbf{1 2 9}$ | $2.20 \mathrm{E}-04$ | $5.41 \mathrm{E}-14$ |
| MI9 | 1925.83 | $4.09 \mathrm{E}+04$ | $4.09 \mathrm{E}-14$ | 1023.15 | $4.64 \mathrm{E}+09$ | $\mathbf{1 4 7}$ |  |  |
| MI13 | 2738.03 | $5.82 \mathrm{E}+04$ | $5.82 \mathrm{E}-14$ | 1023.15 | $6.60 \mathrm{E}+09$ | $\mathbf{2 0 9}$ | $1.69 \mathrm{E}-04$ | $2.56 \mathrm{E}-14$ |
| M114 | 277.83 | $5.91 \mathrm{E}+03$ | $5.91 \mathrm{E}-15$ | 1023.15 | $6.70 \mathrm{E}+08$ | $\mathbf{2 1}$ | $1.53 \mathrm{E}-04$ | $2.29 \mathrm{E}-13$ |


| MI15 | 216.00 | $4.59 \mathrm{E}+03$ | $4.59 \mathrm{E}-15$ | 1023.15 | $5.21 \mathrm{E}+08$ | $\mathbf{1 6}$ | $1.20 \mathrm{E}-04$ | $2.31 \mathrm{E}-13$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MI18 | 1209.33 | $2.57 \mathrm{E}+04$ | $2.57 \mathrm{E}-14$ | 1023.15 | $2.91 \mathrm{E}+09$ | $\mathbf{9 2}$ | $3.43 \mathrm{E}-04$ | $1.18 \mathrm{E}-13$ |
| MI19 | 990.34 | $2.10 \mathrm{E}+04$ | $2.10 \mathrm{E}-14$ | 1023.15 | $2.39 \mathrm{E}+09$ | $\mathbf{7 6}$ | $2.47 \mathrm{E}-04$ | $1.04 \mathrm{E}-13$ |
| MI20 | 124.17 | $2.64 \mathrm{E}+03$ | $2.64 \mathrm{E}-15$ | 1023.15 | $2.99 \mathrm{E}+08$ | $\mathbf{9}$ | $1.37 \mathrm{E}-04$ | $4.59 \mathrm{E}-13$ |
| MI21 | 354.00 | $7.52 \mathrm{E}+03$ | $7.52 \mathrm{E}-15$ | 1023.15 | $8.53 \mathrm{E}+08$ | $\mathbf{2 7}$ | $1.89 \mathrm{E}-04$ | $2.22 \mathrm{E}-13$ |
| M122 | 323.50 | $6.88 \mathrm{E}+03$ | $6.88 \mathrm{E}-15$ | 1023.15 | $7.80 \mathrm{E}+08$ | $\mathbf{2 5}$ | $1.82 \mathrm{E}-04$ | $2.33 \mathrm{E}-13$ |
| MI25 | 196.17 | $4.17 \mathrm{E}+03$ | $4.17 \mathrm{E}-15$ | 1023.15 | $4.73 \mathrm{E}+08$ | $\mathbf{1 5}$ | $4.47 \mathrm{E}-04$ | $9.46 \mathrm{E}-13$ |
| M126 | 260.33 | $5.53 \mathrm{E}+03$ | $5.53 \mathrm{E}-15$ | 1023.15 | $6.27 \mathrm{E}+08$ | $\mathbf{2 0}$ |  |  |
| MI28 | 130.33 | $2.77 \mathrm{E}+03$ | $2.77 \mathrm{E}-15$ | 1023.15 | $3.14 \mathrm{E}+08$ | $\mathbf{1 0}$ | $5.02 \mathrm{E}-05$ | $1.60 \mathrm{E}-13$ |
| MI29 | 212.83 | $4.52 \mathrm{E}+03$ | $4.52 \mathrm{E}-15$ | 1023.15 | $5.13 \mathrm{E}+08$ | $\mathbf{1 6}$ | $2.52 \mathrm{E}-04$ | $4.91 \mathrm{E}-13$ |
| MI32 | 1077.01 | $2.29 \mathrm{E}+04$ | $2.29 \mathrm{E}-14$ | 1023.15 | $2.60 \mathrm{E}+09$ | $\mathbf{8 2}$ | $1.90 \mathrm{E}-04$ | $7.33 \mathrm{E}-14$ |

F815-xl013

|  | $\boldsymbol{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t} \mathbf{( s )}$ | $\boldsymbol{\Delta t} \mathbf{( \mathbf { y r } )}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MI2 | 2209.83 | $4.70 \mathrm{E}+04$ | $4.70 \mathrm{E}-14$ | 1023.15 | $5.33 \mathrm{E}+09$ | $\mathbf{1 6 9}$ | $2.91 \mathrm{E}-04$ | $5.48 \mathrm{E}-14$ |
| MI8 | 106.67 | $2.27 \mathrm{E}+03$ | $2.27 \mathrm{E}-15$ | 1023.15 | $2.57 \mathrm{E}+08$ | $\mathbf{8}$ | $1.73 \mathrm{E}-04$ | $6.73 \mathrm{E}-13$ |
| MI10 | 234.00 | $4.97 \mathrm{E}+03$ | $4.97 \mathrm{E}-15$ | 1023.15 | $5.64 \mathrm{E}+08$ | $\mathbf{1 8}$ | $4.60 \mathrm{E}-04$ | $8.03 \mathrm{E}-13$ |
| MI12 | 238.00 | $5.06 \mathrm{E}+03$ | $5.06 \mathrm{E}-15$ | 1023.15 | $5.74 \mathrm{E}+08$ | $\mathbf{1 8}$ | $4.60 \mathrm{E}-04$ | $8.03 \mathrm{E}-13$ |
| MI13 | 1209.84 | $2.57 \mathrm{E}+04$ | $2.57 \mathrm{E}-14$ | 1023.15 | $2.92 \mathrm{E}+09$ | $\mathbf{9 2}$ | $2.66 \mathrm{E}-04$ | $9.12 \mathrm{E}-14$ |
| MI14 | 351.67 | $7.47 \mathrm{E}+03$ | $7.47 \mathrm{E}-15$ | 1023.15 | $8.47 \mathrm{E}+08$ | $\mathbf{2 7}$ | $3.49 \mathrm{E}-04$ | $4.13 \mathrm{E}-13$ |
| MI16 | 366.33 | $7.79 \mathrm{E}+03$ | $7.79 \mathrm{E}-15$ | 1023.15 | $8.83 \mathrm{E}+08$ | $\mathbf{2 8}$ | $3.49 \mathrm{E}-04$ | $3.96 \mathrm{E}-13$ |
| MI18 | 416.83 | $8.86 \mathrm{E}+03$ | $8.86 \mathrm{E}-15$ | 1023.15 | $1.00 \mathrm{E}+09$ | $\mathbf{3 2}$ | $4.88 \mathrm{E}-04$ | $4.86 \mathrm{E}-13$ |
| MI19 | 247.50 | $5.26 \mathrm{E}+03$ | $5.26 \mathrm{E}-15$ | 1023.15 | $5.96 \mathrm{E}+08$ | $\mathbf{1 9}$ | $5.64 \mathrm{E}-04$ | $9.47 \mathrm{E}-13$ |
| MI25 | 159.33 | $3.39 \mathrm{E}+03$ | $3.39 \mathrm{E}-15$ | 1023.15 | $3.84 \mathrm{E}+08$ | $\mathbf{1 2}$ | $3.99 \mathrm{E}-04$ | $1.04 \mathrm{E}-12$ |
| M127 | 93.00 | $1.98 \mathrm{E}+03$ | $1.98 \mathrm{E}-15$ | 1023.15 | $2.24 \mathrm{E}+08$ | $\mathbf{7}$ | $5.36 \mathrm{E}-04$ | $2.39 \mathrm{E}-12$ |
| MI28 | 259.67 | $5.52 \mathrm{E}+03$ | $5.52 \mathrm{E}-15$ | 1023.15 | $6.26 \mathrm{E}+08$ | $\mathbf{2 0}$ | $5.84 \mathrm{E}-04$ | $9.34 \mathrm{E}-13$ |
| MI29 | 887.99 | $1.89 \mathrm{E}+04$ | $1.89 \mathrm{E}-14$ | 1023.15 | $2.14 \mathrm{E}+09$ | $\mathbf{6 8}$ | $4.49 \mathrm{E}-04$ | $2.10 \mathrm{E}-13$ |
| MI30 | 318.83 | $6.78 \mathrm{E}+03$ | $6.78 \mathrm{E}-15$ | 1023.15 | $7.68 \mathrm{E}+08$ | $\mathbf{2 4}$ | $5.73 \mathrm{E}-04$ | $7.47 \mathrm{E}-13$ |
| MI31 | 563.83 | $1.20 \mathrm{E}+04$ | $1.20 \mathrm{E}-14$ | 1023.15 | $1.36 \mathrm{E}+09$ | $\mathbf{4 3}$ | $3.81 \mathrm{E}-04$ | $2.81 \mathrm{E}-13$ |
| M132 | 100.17 | $2.13 \mathrm{E}+03$ | $2.13 \mathrm{E}-15$ | 1023.15 | $2.41 \mathrm{E}+08$ | $\mathbf{8}$ | $3.78 \mathrm{E}-04$ | $1.57 \mathrm{E}-12$ |
| MI34 | 137.83 | $2.93 \mathrm{E}+03$ | $2.93 \mathrm{E}-15$ | 1023.15 | $3.32 \mathrm{E}+08$ | $\mathbf{1 1}$ | $4.34 \mathrm{E}-04$ | $1.31 \mathrm{E}-12$ |
| MI35 | 170.00 | $3.61 \mathrm{E}+03$ | $3.61 \mathrm{E}-15$ | 1023.15 | $4.10 \mathrm{E}+08$ | $\mathbf{1 3}$ | $3.59 \mathrm{E}-04$ | $8.76 \mathrm{E}-13$ |
| MI37 | 281.17 | $5.98 \mathrm{E}+03$ | $5.98 \mathrm{E}-15$ | 1023.15 | $6.78 \mathrm{E}+08$ | $\mathbf{2 1}$ | $4.67 \mathrm{E}-04$ | $6.90 \mathrm{E}-13$ |
| MI38 | 165.67 | $3.52 \mathrm{E}+03$ | $3.52 \mathrm{E}-15$ | 1023.15 | $3.99 \mathrm{E}+08$ | $\mathbf{1 3}$ | $3.92 \mathrm{E}-04$ | $9.82 \mathrm{E}-13$ |
| MI39 | 88.17 | $1.87 \mathrm{E}+03$ | $1.87 \mathrm{E}-15$ | 1023.15 | $2.12 \mathrm{E}+08$ | $\mathbf{7}$ | $1.45 \mathrm{E}-04$ | $6.84 \mathrm{E}-13$ |
| MI43 | 378.83 | $8.05 \mathrm{E}+03$ | $8.05 \mathrm{E}-15$ | 1023.15 | $9.13 \mathrm{E}+08$ | $\mathbf{2 9}$ | $1.05 \mathrm{E}-04$ | $1.16 \mathrm{E}-13$ |
| MI48 | 1108.83 | $2.36 \mathrm{E}+04$ | $2.36 \mathrm{E}-14$ | 1023.15 | $2.67 \mathrm{E}+09$ | $\mathbf{8 5}$ | $1.01 \mathrm{E}-04$ | $3.79 \mathrm{E}-14$ |

BC17-Ia15_42

|  | $\boldsymbol{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t}(\mathbf{s})$ | $\boldsymbol{\Delta t}(\mathbf{y r})$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MI2 | 298.00 | $6.33 \mathrm{E}+03$ | $6.33 \mathrm{E}-15$ | 1023.15 | $7.18 \mathrm{E}+08$ | $\mathbf{2 3}$ | $1.38 \mathrm{E}-04$ | $1.92 \mathrm{E}-13$ |
| MI3 | 272.67 | $5.80 \mathrm{E}+03$ | $5.80 \mathrm{E}-15$ | 1023.15 | $6.57 \mathrm{E}+08$ | $\mathbf{2 1}$ | $9.01 \mathrm{E}-05$ | $1.37 \mathrm{E}-13$ |
| MI4 | 487.00 | $1.04 \mathrm{E}+04$ | $1.04 \mathrm{E}-14$ | 1023.15 | $1.17 \mathrm{E}+09$ | $\mathbf{3 7}$ | $8.98 \mathrm{E}-05$ | $7.66 \mathrm{E}-14$ |
| MI5 | 199.67 | $4.24 \mathrm{E}+03$ | $4.24 \mathrm{E}-15$ | 1023.15 | $4.81 \mathrm{E}+08$ | $\mathbf{1 5}$ | $1.30 \mathrm{E}-04$ | $2.71 \mathrm{E}-13$ |
| MI12 | 366.50 | $7.79 \mathrm{E}+03$ | $7.79 \mathrm{E}-15$ | 1023.15 | $8.83 \mathrm{E}+08$ | $\mathbf{2 8}$ | $9.67 \mathrm{E}-05$ | $1.10 \mathrm{E}-13$ |
| MI13 | 178.17 | $3.79 \mathrm{E}+03$ | $3.79 \mathrm{E}-15$ | 1023.15 | $4.29 \mathrm{E}+08$ | $\mathbf{1 4}$ | $1.09 \mathrm{E}-04$ | $2.55 \mathrm{E}-13$ |
| MI17 | 540.50 | $1.15 \mathrm{E}+04$ | $1.15 \mathrm{E}-14$ | 1023.15 | $1.30 \mathrm{E}+09$ | $\mathbf{4 1}$ |  |  |
| MI20 | 166.79 | $3.55 \mathrm{E}+03$ | $3.55 \mathrm{E}-15$ | 1023.15 | $4.02 \mathrm{E}+08$ | $\mathbf{1 3}$ | $2.19 \mathrm{E}-04$ | $5.46 \mathrm{E}-13$ |
| MI22 | 388.50 | $8.26 \mathrm{E}+03$ | $8.26 \mathrm{E}-15$ | 1023.15 | $9.36 \mathrm{E}+08$ | $\mathbf{3 0}$ | $1.23 \mathrm{E}-04$ | $1.32 \mathrm{E}-13$ |
| MI24 | 295.17 | $6.27 \mathrm{E}+03$ | $6.27 \mathrm{E}-15$ | 1023.15 | $7.11 \mathrm{E}+08$ | $\mathbf{2 3}$ | $9.79 \mathrm{E}-05$ | $1.38 \mathrm{E}-13$ |

BC17-Ia15_43

|  | $\mathbf{y}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t}(\mathbf{s})$ | $\Delta \mathbf{t}(\mathbf{y r})$ |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MI2 | 3111.83 | $6.61 \mathrm{E}+04$ | $6.61 \mathrm{E}-14$ | 1023.15 | $7.50 \mathrm{E}+09$ | $\mathbf{2 3 8}$ | $2.50 \mathrm{E}-04$ | $3.34 \mathrm{E}-14$ |
| M13 | 2072.99 | $4.41 \mathrm{E}+04$ | $4.41 \mathrm{E}-14$ | 1023.15 | $5.00 \mathrm{E}+09$ | $\mathbf{1 5 8}$ | $2.03 \mathrm{E}-04$ | $4.06 \mathrm{E}-14$ |


| MI8 | 780.67 | $1.66 \mathrm{E}+04$ | $1.66 \mathrm{E}-14$ | 1023.15 | $1.88 \mathrm{E}+09$ | $\mathbf{6 0}$ | $2.58 \mathrm{E}-04$ | $1.37 \mathrm{E}-13$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MI9 | 610.84 | $1.30 \mathrm{E}+04$ | $1.30 \mathrm{E}-14$ | 1023.15 | $1.47 \mathrm{E}+09$ | $\mathbf{4 7}$ | $1.27 \mathrm{E}-04$ | $8.64 \mathrm{E}-14$ |
| MI19 | 166.83 | $3.55 \mathrm{E}+03$ | $3.55 \mathrm{E}-15$ | 1023.15 | $4.02 \mathrm{E}+08$ | $\mathbf{1 3}$ |  |  |
| MI21 | 396.34 | $8.42 \mathrm{E}+03$ | $8.42 \mathrm{E}-15$ | 1023.15 | $9.55 \mathrm{E}+08$ | $\mathbf{3 0}$ |  |  |

BC17-Ia15_44

|  | $\boldsymbol{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t}(\mathbf{s})$ | $\Delta \mathbf{t}(\mathbf{y r})$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MI2 | 718.50 | $1.53 \mathrm{E}+04$ | $1.53 \mathrm{E}-14$ | 1023.15 | $1.73 \mathrm{E}+09$ | $\mathbf{5 5}$ |  |  |
| MI3 | 220.50 | $4.69 \mathrm{E}+03$ | $4.69 \mathrm{E}-15$ | 1023.15 | $5.31 \mathrm{E}+08$ | $\mathbf{1 7}$ |  |  |
| MI4 | 205.00 | $4.36 \mathrm{E}+03$ | $4.36 \mathrm{E}-15$ | 1023.15 | $4.94 \mathrm{E}+08$ | $\mathbf{1 6}$ | $1.22 \mathrm{E}-04$ | $2.47 \mathrm{E}-13$ |
| MI7 | 798.50 | $1.70 \mathrm{E}+04$ | $1.70 \mathrm{E}-14$ | 1023.15 | $1.92 \mathrm{E}+09$ | $\mathbf{6 1}$ | $1.23 \mathrm{E}-04$ | $6.42 \mathrm{E}-14$ |
| MI11 | 588.67 | $1.25 \mathrm{E}+04$ | $1.25 \mathrm{E}-14$ | 1023.15 | $1.42 \mathrm{E}+09$ | $\mathbf{4 5}$ | $1.28 \mathrm{E}-04$ | $9.01 \mathrm{E}-14$ |
| MI12 | 439.17 | $9.33 \mathrm{E}+03$ | $9.33 \mathrm{E}-15$ | 1023.15 | $1.06 \mathrm{E}+09$ | $\mathbf{3 4}$ |  |  |
| MI13 | 485.00 | $1.03 \mathrm{E}+04$ | $1.03 \mathrm{E}-14$ | 1023.15 | $1.17 \mathrm{E}+09$ | $\mathbf{3 7}$ | $2.84 \mathrm{E}-04$ | $2.43 \mathrm{E}-13$ |
| MI14 | 310.33 | $6.60 \mathrm{E}+03$ | $6.60 \mathrm{E}-15$ | 1023.15 | $7.48 \mathrm{E}+08$ | $\mathbf{2 4}$ | $2.53 \mathrm{E}-04$ | $3.39 \mathrm{E}-13$ |
| MI15 | 417.33 | $8.87 \mathrm{E}+03$ | $8.87 \mathrm{E}-15$ | 1023.15 | $1.01 \mathrm{E}+09$ | $\mathbf{3 2}$ |  |  |
| MI17 | 762.84 | $1.62 \mathrm{E}+04$ | $1.62 \mathrm{E}-14$ | 1023.15 | $1.84 \mathrm{E}+09$ | $\mathbf{5 8}$ | $1.91 \mathrm{E}-04$ | $1.04 \mathrm{E}-13$ |
| MI20 | 265.83 | $5.65 \mathrm{E}+03$ | $5.65 \mathrm{E}-15$ | 1023.15 | $6.41 \mathrm{E}+08$ | $\mathbf{2 0}$ | $1.79 \mathrm{E}-04$ | $2.80 \mathrm{E}-13$ |
| MI21 | 889.50 | $1.89 \mathrm{E}+04$ | $1.89 \mathrm{E}-14$ | 1023.15 | $2.14 \mathrm{E}+09$ | $\mathbf{6 8}$ | $1.82 \mathrm{E}-04$ | $8.51 \mathrm{E}-14$ |

BC17-Ia15_45

|  | $\Delta \mathbf{V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\boldsymbol{\Delta t}(\mathbf{s})$ | $\Delta \mathbf{t}(\mathbf{y r})$ |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M13 | 542.17 | $1.15 \mathrm{E}+04$ | $1.15 \mathrm{E}-14$ | 1023.15 | $1.31 \mathrm{E}+09$ | $\mathbf{4 1}$ | $2.47 \mathrm{E}-04$ | $1.89 \mathrm{E}-13$ |
| MI5 | 151.17 | $3.21 \mathrm{E}+03$ | $3.21 \mathrm{E}-15$ | 1023.15 | $3.64 \mathrm{E}+08$ | $\mathbf{1 2}$ |  |  |

BB08-21b_1

|  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | ---: |
| MI9 | $\boldsymbol{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\boldsymbol{\Delta t}(\mathbf{s})$ | $\Delta \mathbf{t}(\mathbf{y r})$ |  |  |
| MI11 | 155.33 | $3.30 \mathrm{E}+03$ | $3.30 \mathrm{E}-15$ | 1023.15 | $3.74 \mathrm{E}+08$ | $\mathbf{1 2}$ |  |  |
| MI14 | 182.33 | $3.88 \mathrm{E}+03$ | $3.88 \mathrm{E}-15$ | 1023.15 | $4.39 \mathrm{E}+08$ | $\mathbf{1 4}$ | $2.67 \mathrm{E}-04$ | $6.08 \mathrm{E}-13$ |
| MI29 | 174.33 | $3.71 \mathrm{E}+03$ | $3.71 \mathrm{E}-15$ | 1023.15 | $4.20 \mathrm{E}+08$ | $\mathbf{1 3}$ |  |  |
|  | 611.50 | $1.30 \mathrm{E}+04$ | $1.30 \mathrm{E}-14$ | 1023.15 | $1.47 \mathrm{E}+09$ | $\mathbf{4 7}$ | $1.62 \mathrm{E}-04$ | $1.10 \mathrm{E}-13$ |
| BB08-21b_2 |  |  |  |  |  |  |  |  |
|  | $\mathbf{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\boldsymbol{\Delta t}(\mathbf{s})$ | $\Delta \mathbf{t}(\mathbf{y r})$ |  |  |
| MI1 | 124.17 | $2.64 \mathrm{E}+03$ | $2.64 \mathrm{E}-15$ | 1023.15 | $2.99 \mathrm{E}+08$ | $\mathbf{9}$ |  |  |
| MI3 | 2214.83 | $4.71 \mathrm{E}+04$ | $4.71 \mathrm{E}-14$ | 1023.15 | $5.34 \mathrm{E}+09$ | $\mathbf{1 6 9}$ | $2.39 \mathrm{E}-04$ | $4.48 \mathrm{E}-14$ |

BB08-21b_20a

|  | $\Delta \mathbf{V}$ | $\mathbf{u m}^{3}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t}(\mathbf{s})$ | $\Delta \mathbf{t}(\mathbf{y r})$ |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M13 | 3562.48 | $7.57 \mathrm{E}+04$ | $7.57 \mathrm{E}-14$ | 1023.15 | $8.58 \mathrm{E}+09$ | $\mathbf{2 7 2}$ | $2.74 \mathrm{E}-04$ | $3.20 \mathrm{E}-14$ |

BB08-21b_20b

|  | $\mathbf{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\boldsymbol{\Delta t}(\mathbf{s})$ | $\boldsymbol{\Delta t} \mathbf{t} \mathbf{( \mathbf { r } )}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | ---: |
| MI7 | 510.17 | $1.08 \mathrm{E}+04$ | $1.08 \mathrm{E}-14$ | 1023.15 | $1.23 \mathrm{E}+09$ | $\mathbf{3 9}$ | $2.32 \mathrm{E}-04$ | $1.88 \mathrm{E}-13$ |
| MI9 | 257.67 | $5.48 \mathrm{E}+03$ | $5.48 \mathrm{E}-15$ | 1023.15 | $6.21 \mathrm{E}+08$ | $\mathbf{2 0}$ | $2.52 \mathrm{E}-04$ | $4.05 \mathrm{E}-13$ |
| MI10 | 1140.66 | $2.42 \mathrm{E}+04$ | $2.42 \mathrm{E}-14$ | 1023.15 | $2.75 \mathrm{E}+09$ | $\mathbf{8 7}$ | $1.32 \mathrm{E}-04$ | $4.82 \mathrm{E}-14$ |

BB08-21b_22

|  | $\boldsymbol{\Delta V}$ | $\mathbf{u m}^{\mathbf{3}}$ | $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{T}(\mathbf{K})$ | $\Delta \mathbf{t}(\mathbf{s})$ | $\boldsymbol{\Delta t} \mathbf{t} \mathbf{y r})$ |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MI1 | 334.50 | $7.11 \mathrm{E}+03$ | $7.11 \mathrm{E}-15$ | 1023.15 | $8.06 \mathrm{E}+08$ | $\mathbf{2 6}$ |  |  |
| MI3 | 454.67 | $9.66 \mathrm{E}+03$ | $9.66 \mathrm{E}-15$ | 1023.15 | $1.10 \mathrm{E}+09$ | $\mathbf{3 5}$ |  |  |
| MI6 | 230.17 | $4.89 \mathrm{E}+03$ | $4.89 \mathrm{E}-15$ | 1023.15 | $5.55 \mathrm{E}+08$ | $\mathbf{1 8}$ |  |  |
| MI8 | 244.00 | $5.19 \mathrm{E}+03$ | $5.19 \mathrm{E}-15$ | 1023.15 | $5.88 \mathrm{E}+08$ | $\mathbf{1 9}$ | $2.09 \mathrm{E}-04$ | $3.56 \mathrm{E}-13$ |
| MI9 | 135.50 | $2.88 \mathrm{E}+03$ | $2.88 \mathrm{E}-15$ | 1023.15 | $3.27 \mathrm{E}+08$ | $\mathbf{1 0}$ |  |  |
| M110 | 500.83 | $1.06 \mathrm{E}+04$ | $1.06 \mathrm{E}-14$ | 1023.15 | $1.21 \mathrm{E}+09$ | $\mathbf{3 8}$ | $1.64 \mathrm{E}-04$ | $1.36 \mathrm{E}-13$ |

