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DATA REPOSITORY ITEM 2009118

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3 THERMODYNAMIC MODELLING

Abiogenic endmember compositions for Nisyros have been computed from equation (4)
considering the following temperature dependencies for f_{H2O} of 2 m NaCl solutions and K 3,
respectively:

7
$$\log f_{H_2O} = 5.462 - 2047/T$$
 (S1)

8
$$\log K_3 = 10.5 - (5150 + 310*n)/T$$
 (S2)

9 where T is in K a nd n the number of carbon atoms in etha ne and propane, respectively
10 (Chiodini et al., 2001; Taran and Giggenbach, 2003).

11 Carbon iso tope data for CH₄ and CO₂ reflect hydrocarbon formation temperatures of 340 \pm 12 10°C (Tab le 1). A t these temperatures, the r edox conditions of the b i-phase hy drothermal 13 system can be constrained considering gas concentration data of the fumaroles. For the period 14 from 1990-2002, molar ratios (X) of redox pairs CO/CO₂, H₂/H₂O and CH₄/CO₂ indicate that 15 redox conditions at 340 °C closely correspond to the FeO-FeO_{1.5} buffer (Chiodini and Marini, 1998; Marini and Fie big, 2005), for which $log(X_{H_2}/X_{H_2O})$ is -2.82, roughly independent of 16 temperature (Giggenbach, 1987). X_{CO}/X_{CO_2} and X_{CH_4}/X_{CO_2} ratios were also measured for the 17 18 fumaroles sampled in this study and are indistinguishable from values observed for the period 19 1990-2002 (Table 1S). This agreement indicates that no significant change in redox 20 conditions took place between 1990 and 2007. The f_{CO_2} at the t emperature of m ethane 21 formation can be constrained from molar ratios of CO and H₂ using equation S3 (Chiodini & 22 Marini, 19 98), along with g as concentration da ta and methane formation temperatures 23 reported by Fiebig et al. (2007):

24
$$\log f_{CO_2} = -2.485 + 2248/T - \log(X_{H_2}/X_{CO}) + \log f_{H_2O}$$

26 At Nisyros, f_{CO_2} is ~1bar (Table 1S), such that $log f_{CO_2}$ in equation (4) can be neglected.

27 MIXING TRENDS DISPLAYED IN FIGURE 1

28 Hydrocarbon distribution ratios of C1/C2 and C2/C3 are given through

29
$$C_i/C_{i+1} = (nC_{i,ab} + nC_{i,\alpha})/(nC_{i+1,ab} + nC_{i+1,\alpha})$$
 (S4)

- 30 with nC_{ab} and nC_{α} denoting the moles of alkane hydrocarbons with carbon numbers i and i+1,
- 31 predicted by thermodynamics according to equation (4) (ab) and by rando m breakage or
- 32 linkage of C-bonds (α), respectively. The Schulz-Flory distribution factor α is defined by

33
$$\alpha = nC_{i+1,\alpha}/nC_{i,\alpha}$$
(S5)

The mole fraction of abiogenic equilibrium alkanes with C-numbers i and i+1 is represented
by Y according to

36
$$Y_{i+1/i} = nC_{i+1,ab}/ nC_{i,}$$

37 (S6)

Values for Y can be computed fr om equation (4). If react ion (5) a pplies for abiogen ic hydrocarbon production, only m ethane is g enerated and Y beco mes 0. F or a give n chain length, molar fractions of hydrocarbons generated through random break age or linkage (X_{α}) or through abiogenic processes $(X_{a^{-}})$ are interlinked through

42
$$X_{b} = 1 - X_{\alpha} = nC_{a}/nC = (1 - nC_{\alpha}/nC)$$
 (S7)

43 Considering equation (S4) to (S7), it can be derived for C1/C2 and C2/C3 ratios

44
$$C1/C2 = 1/((1 - X_{\alpha})*Y_{2/1} + \alpha * X_{\alpha})$$
 (S8)

45
$$C_2/C_3 = ((1 - X_\alpha)^* Y_{2/1} + \alpha^* X_\alpha)/((1 - X_\alpha)^* Y_{2/1}^* Y_{3/2} + \alpha^* \alpha^* X_\alpha)$$
 (S9)

46

47 **TABLE**

48 Table DR1. Molar ratios, X, of gas components contained in dry gas samples and comparison of

- 49 X_{CH_4}/X_{CO_2} and X_{CO}/X_{CO_2} ratios obtained in 2007 with those characteristic for the 12 y ear
- 50 period (1990-2002; Marini & Fiebig, 2005). Also given are $log f_{CO_2}$ values characteristic for

51 the Nisyros bi-phase hydrothermal system, which were calculated according to equation S3

52 and temperatures derived from carbon isotope partitioning between CO_2 and CH_4 (see Table

53 1).

54

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Sample	$X(CO_2)$	X(CH ₄)	X(CO)	$X(H_2)$	$log(CO/CO_2)$	$log(CO/CO_2)_{12yr}$	$log(CH_4/CO_2)$	$log(CH_4/CO_2)_{12yr}$	logf(CO ₂)
Polybotes Mikros (PP9S)	743300	1759	9.0	16000	-4.9	-4.8 to -5.5	-2.6	-2.5 to -3.0	0.0
Stefanos (S4)	791500	4400	2.2	6200	-5.6	-5.4 to -6.1	-2.3	-2.1 to -2.6	-0.1
Phlegeton (A)	809300	805	2.1	9230	-5.6	-5.3 to -6.0	-3.0	-2.4 to -3.2	-0.3