

## Methods

### *Sample preparation*

In order to use the FTIR technique, the melt inclusions need to be quenched to glass. Olivine crystals were hand-picked under a binocular stereomicroscope. The crystal concentrate was put in refractive index oil ( $n = 1.67$ , close to that of olivine) in order to view the inclusions within the crystals. Crystals containing uncracked and fully enclosed inclusions were hand-picked under a binocular stereomicroscope and put in another oil-filled glass container to be described and photographed for documentation.

Crystals containing glass inclusions were mounted in acetone-soluble cement on microscope slides. Doubly polished crystal wafers (with inclusions exposed on both sides) were ground by hand using water-rinsed 600 grit paper and then polished with 6- $\mu\text{m}$  and 1- $\mu\text{m}$  diamond paste. Once the first side of the inclusion was polished the slide was warmed and the crystal was flipped. The grinding and polishing procedure was then repeated for the second side. The intersection of the inclusion on both sides needs to be parallel and well polished to ensure constant sample thickness. Uniform sample thickness was monitored during grinding and polishing by observing the distribution of interference colors in the crystal when viewed under crossed-polars. The doubly-polished crystal was then removed from the slide by dissolving the cement in acetone and cleaned with more acetone.

### *Infrared spectroscopy*

A Thermo Nicolet Nexus 670 Fourier Transform Infrared (FTIR) spectrometer interfaced with a Continuum IR microscope was used to determine the concentrations of  $\text{H}_2\text{O}$  and  $\text{CO}_2$  in the glass inclusions. The analyses were performed by placing a wafered olivine host crystal with an inclusion on an NaCl window. Then, depending on the size of the doubly intersected inclusion, the IR aperture was adjusted so it was totally contained within the inclusion and avoided the inclusion boundaries. Two individual spectra were taken on different areas of each inclusion.

Band assignments for dissolved  $\text{H}_2\text{O}$  and carbonate in basaltic glass are based on Dixon et al. (1995). Quantitative measurements of dissolved total  $\text{H}_2\text{O}$ , molecular  $\text{H}_2\text{O}$ , and carbonate ( $\text{CO}_3^{2-}$ ) were obtained using Beer's Law:

$$C = \frac{MA}{\rho d \epsilon}$$

where  $C$  is the concentration (weight fraction) of the absorbing species,  $M$  is the molecular weight of  $H_2O$  (18.02) or  $CO_2$  (44.00),  $A$  is the absorbance intensity of the band of interest,  $\rho$  is room temperature density of the glass (calculated from a simple summation of partial molar volumes following Luhr, 2001),  $d$  is the thickness of the glass wafer, and  $\epsilon$  is the molar absorption coefficient. The thickness of each inclusion was measured by mounting the edge of the doubly polished crystal wafer on the tip of a needle using crystal bond. The crystal wafer was then immersed into a cylindrical glass well filled with refractive index oil ( $n = 1.67$ ). The crystal wafer could then be rotated and viewed parallel to its flat dimension under a microscope. Using a microscope with a calibrated eye piece, the thickness of the inclusion was measured with an accuracy of  $\pm 1$  to  $\pm 5 \mu m$  depending on how close to the edge of the crystal the inclusion was.

Total dissolved  $H_2O$  was measured using the intensity of the band centered at  $3550 \text{ cm}^{-1}$ , which corresponds to the fundamental O-H stretching vibration. On a printed copy of the spectra the background was drawn as a smooth curve and graphically subtracted from the peak height to measure the absorbance intensity of the  $3550 \text{ cm}^{-1}$  band. The total dissolved water contents were calculated using a molar absorption coefficient of  $63 \pm 3 \text{ L/mol cm}$  from Ihinger et al. (1994).

Dissolved carbonate was measured from the  $1515$  and  $1430 \text{ cm}^{-1}$  absorbance bands, which correspond to distorted asymmetric stretching of carbonate groups (Ihinger et al. 1994). Because the shape of the background in the region of the carbonate doublet is complex, it is necessary to subtract a carbonate-free reference spectrum to obtain a flat background (Dixon et al. 1995). We measured absorbance intensities of the  $1515$  and  $1430 \text{ cm}^{-1}$  bands using a peak-fitting program that fits the sample spectrum with a straight line, a spectrum for a  $CO_2$ -free basaltic glass, a pure  $1630 \text{ cm}^{-1}$  band for molecular  $H_2O$ , and a pure carbonate doublet (unpublished program by S. Newman). The molar absorption coefficient of carbonate in basaltic glass is compositionally dependent and was derived using the average composition of the inclusions and the linear equation reported in Dixon & Pan (1995). The dissolved carbonate content was calculated using a molar absorption coefficient of  $370 \text{ L/mol cm}$ .

Based on replicate analyses, precision ( $2\sigma$ ) for total  $H_2O$  is  $<13\%$  (relative) and  $<12\%$  for  $CO_2$ . Accuracy for these techniques is estimated to be  $\pm 10\%$  for total  $H_2O$  and  $\pm 20\%$  for  $CO_2$  (Dixon and Clague, 2001).

### *Electron microprobe analysis*

The olivine-hosted melt inclusions were analyzed for major elements, S, F, and Cl using a Cameca SX-100 electron microprobe at the University of Oregon. An accelerating voltage of 15 kV, a 10 nA beam current, and a beam diameter of 10  $\mu\text{m}$  were used along with a combination of glass and mineral standards. Between one and five separate spots were analyzed per inclusion depending on the inclusion size. The average and  $1\sigma$  values for each inclusion are given in Appendix Table 1. A second run measured the composition of the olivine adjacent to the inclusions. These analyses were conducted on the JEOL JXA-8900R electron microprobe in the Laboratorio Universitario de Petrología at the Universidad Nacional Autónoma de México, using a focus beam, an accelerating voltage of 15 kV, and 20 nA beam current.

### *Correction for post-entrapment crystallization and Fe diffusive loss*

Melt inclusion compositions were corrected for post-entrapment crystallization of olivine along the walls of the inclusion and Fe loss from the inclusion to the olivine host. Original microprobe and FTIR analytical values before any correction are given in Appendix Table 2. The correction for post-entrapment crystallization involved adding 0.1% increments of equilibrium olivine back into each melt inclusion until the inclusion composition was in equilibrium with the olivine host. A value of 0.3 was used for the Fe-Mg exchange coefficient ( $K_D = (\text{Mg}/\text{Fe}^{2+})_{\text{melt}}/(\text{Mg}/\text{Fe}^{2+})_{\text{olivine}}$ ). Correction for Fe loss involved adding FeO back into each melt inclusion until the  $\text{FeO}^T$  of the inclusion was restored to the MgO vs.  $\text{FeO}^T$  trend of whole rock data (Witter et al., 2005) from Popocatepetl (see Danyushevsky et al., 2000). After correction for Fe loss, the calculated amounts of post-entrapment crystallization were 0.4 to 25.2 wt.%.

### *Volcanic gas compositions and fluxes*

Mass ratios and fluxes of major gas components that have been measured for Popocatepetl are reported in Appendix Table 3.

### *Calculation of gas compositions in equilibrium with basaltic melts as a function of pressure*

To construct Figure 3, we calculated the  $\text{CO}_2/\text{SO}_2$  mass ratios of gases in equilibrium with basaltic melt as a function of pressure beneath Popocatepetl volcano using the vapor-melt partitioning model of Scaillet and Pichavant (2005). Input parameters for the calculation

are melt composition, temperature, pressure, dissolved H<sub>2</sub>O and S contents, and oxygen fugacity. For composition, we used the average value for the melt inclusions reported in Table 1. We assumed a constant temperature of 1140 °C based on the average of the calculated melt inclusion temperatures in Table 1. We assumed that dissolved H<sub>2</sub>O varied as a function of pressure according to a second order polynomial fit to the melt inclusion H<sub>2</sub>O vs. pressure data, but we excluded from the regression the 3 inclusions shown in Fig. 2 that have low H<sub>2</sub>O but relatively high CO<sub>2</sub>. For the melt S contents, the melt inclusion data show evidence for only minor S loss by degassing until lower pressures (~150 MPa), as evidenced by relatively constant S/K<sub>2</sub>O. This is similar to the conclusions of Spilliaert et al. (2006), who used melt inclusion data from Etna to show that degassing of S began at pressures below ~140 MPa. Thus, for simplicity, we assumed that the melts contained 2000 ppm S at pressures down to 150 MPa. Below that pressure, we varied S linearly with pressure such that S decreased to 700 ppm at 1 MPa pressure, based on the lower S contents of the melt inclusions trapped at ≤40 MPa. Although these simplifying assumptions about the behavior of S are a bit ad hoc, they are consistent with the melt inclusion S and pressure data, and small variations in the way that S varies with pressure will not substantially change the curves shown in Figure 3.

The oxygen fugacity of the basaltic endmember at Popocatepetl is estimated to be NNO+1 based on whole rock and mineral chemical data and thermodynamic modeling (Witter et al., 2005), and the uncertainty in this estimate is probably about ±0.5 log units in  $f_{O_2}$ . Accordingly, we calculated gas compositions for a range of  $f_{O_2}$  from NNO+0.5 to NNO+1.5. Because the  $f_{O_2}$  has a strong effect on the mole fraction of SO<sub>2</sub> in the gas phase, the uncertainty in oxygen fugacity represents the largest uncertainty in our gas composition calculations. Thus the range in oxygen fugacities shown by the 3 curves in Figure 3 shows the uncertainty in our method.

Using these parameters, we varied the pressure and used the model of Scaillet and Pichavant (2005) to calculate the SO<sub>2</sub> fugacity in the gas phase and then converted that to SO<sub>2</sub> mole fractions using the Redlich-Kwong equation of state. Equilibrium thermodynamic calculations using standard state data for gas components show that over the range of temperature, pressure, H<sub>2</sub>O content and oxygen fugacity, SO<sub>2</sub> is the dominant S species in the vapor phase, and thus we have ignored the contribution of H<sub>2</sub>S to the total S contents of the vapor.

Using the H<sub>2</sub>O+CO<sub>2</sub> solubility model of Papale et al. (2006), we computed the proportions of H<sub>2</sub>O and CO<sub>2</sub> in the gas phase based on our melt inclusion data. The results

suggest that most inclusions were in equilibrium with vapor having 50 to 60 mol% CO<sub>2</sub>, with an average of 56 mol% (this average again excludes one inclusion from Table 1 with low H<sub>2</sub>O and high CO<sub>2</sub>). Using this result together with the SO<sub>2</sub> mole fractions calculated as describe above, we renormalized the data such that the mole fractions of H<sub>2</sub>O, CO<sub>2</sub>, and SO<sub>2</sub> in the gas phase summed to 1.

To construct Figure 4, we used the methods (equations 1-4) described in Giggenbach (1997) based on Henry's law solubility constants, as follows. The effects of vapor exsolution on the concentration,  $c$ , of a magmatic volatile component,  $i$ , transferred to the vapor phase,  $v$ , or remaining in the melt,  $m$ , can be described in terms of the Henry's Law constant,  $K_{i,T}$ , in mg/kg bar, and the dimensionless mass/volume, Ostwald-type distribution coefficient,  $Q_{i,T} = c_{i,v} / c_{i,m}$ . The two are related through:

$$K_{i,T} = c_{i,m} / P_i = 10^6 MW_i / (\rho_m RT Q_{i,T})$$

Where  $c_{i,m}$  is the concentration of volatile component  $i$  in the melt,  $P_i$  is the partial pressure of component  $i$  in the vapor phase,  $MW_i$  is the molecular weight of component  $i$ ,  $\rho_m$  is the density of the melt,  $R$  is the gas constant (82.05 cm<sup>3</sup> bar/K mol), and  $T$  is the temperature. By use of mass balance and the assumptions that vapor-melt separation is a single-step, closed-system process and that the gases behave ideally, the total pressure,  $P_t$ , generated by the initial concentrations  $c_{i,0}$  of the volatile components in the melt corresponds to:

$$P_t = \sum (c_{i,0} / (R_v Q_{i,T} + 1) K_{i,T})$$

Where  $R_v$  is the vapor/melt volume ratio. Because of the increasingly large non-ideal behavior of CO<sub>2</sub> with increasing pressure and the large contribution of CO<sub>2</sub> to the total pressure of the system, we accounted for the non-ideality of CO<sub>2</sub> using fugacity coefficients calculated with the Redlich-Kwong equation of state. For melt exsolution in a closed system (no loss of volatiles),  $R_v$  is related to the vesicularity,  $V_v$ , in %, through:

$$V_v = 100 R_v / (1 + R_v)$$

The fraction  $x_{i,m}$  of the volatile component  $i$  remaining in the melt is given by:

$$x_{i,m} = c_{i,m} / c_{i,0} = 1 / (R_v Q_{i,T} + 1).$$

We used values of  $K_{i,T}$  and  $Q_{i,T}$  calculated with the model of Newman and Lowenstern (2002) for H<sub>2</sub>O and CO<sub>2</sub>, from experimental data of Webster et al. (1999) for Cl, and from experimental data of Jugo et al. (2005) for S.

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Table DR1.

	n		SiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	FeO <sup>T</sup>	MgO	CaO	Na <sub>2</sub> O	K <sub>2</sub> O	TiO <sub>2</sub>	MnO	P <sub>2</sub> O <sub>5</sub>	F	S	Cl	TOTAL
M28-2 gr5	3	Average	51.92	18.11	4.81	4.52	8.76	4.47	1.02	1.24	0.08	0.25	0.03	0.19	0.09	95.48
		1 Std. Dev.	0.61	0.12	0.10	0.06	0.47	0.07	0.04	0.09	0.06	0.00	0.03	0.01	0.00	
M28-2 gr6	3	Average	51.48	19.10	3.86	4.23	9.07	5.31	1.10	1.43	0.08	0.31	0.12	0.22	0.10	96.41
		1 Std. Dev.	0.25	0.19	0.11	0.09	0.36	0.12	0.01	0.02	0.01	0.02	0.15	0.01	0.01	
M28-2 gr7	3	Average	50.96	20.03	3.69	3.99	9.30	5.20	1.13	1.32	0.07	0.28	0.33	0.20	0.09	96.60
		1 Std. Dev.	0.47	0.17	0.12	0.10	0.41	0.36	0.02	0.03	0.04	0.00	0.37	0.00	0.00	
M29-6	1		51.71	18.63	3.79	3.36	8.69	5.72	1.06	1.45	0.07	0.30	0.06	0.23	0.11	95.20
M48-5 gr1-2	3	Average	52.43	21.91	4.04	4.77	5.58	6.52	1.48	1.22	0.10	0.32	0.09	0.10	0.12	98.69
		1 Std. Dev.	0.21	0.11	0.02	0.03	0.58	0.07	0.05	0.06	0.02	0.02	0.06	0.00	0.00	
M48-5 gr2-1	1		52.46	18.95	3.91	2.74	9.03	5.53	1.20	1.38	0.05	0.26	0.20	0.20	0.09	96.02
M48-5 gr3old	3	Average	56.13	23.23	2.32	2.10	5.04	9.88	1.87	0.59	0.06	0.39	0.05	0.06	0.15	101.86
		1 Std. Dev.	0.29	0.22	0.01	0.01	0.50	0.21	0.02	0.02	0.04	0.01	0.05	0.00	0.01	
M48-5 gr5	5	Average	52.45	18.01	4.38	3.96	9.41	5.20	1.10	1.36	0.06	0.30	0.07	0.18	0.08	96.56
		1 Std. Dev.	0.35	0.29	0.10	0.23	0.22	0.29	0.03	0.08	0.03	0.03	0.06	0.01	0.00	
M53-51 gr1-1	4	Average	52.18	18.66	4.41	4.18	9.10	5.31	1.07	1.35	0.09	0.32	0.09	0.21	0.08	97.06
		1 Std. Dev.	0.48	0.17	0.07	0.12	0.22	0.29	0.03	0.06	0.02	0.04	0.01	0.00	0.00	



**Table DR2**

	<b>M28-2 gr5</b>	<b>M28-2 gr6</b>	<b>M28-2 gr7</b>	<b>M29-6</b>	<b>M48-5 gr1-2</b>	<b>M48-5 gr2-1</b>	<b>M48-5 gr3old</b>	<b>M48-5 gr5</b>	<b>M53-51 gr1-1</b>
<b>SiO<sub>2</sub></b>	51.9	51.5	51.0	51.7	52.4	52.5	56.1	52.4	52.2
<b>Al<sub>2</sub>O<sub>3</sub></b>	18.1	19.1	20.0	18.6	21.9	19.0	23.2	18.0	18.7
<b>FeO<sup>T</sup></b>	4.81	3.86	3.69	3.79	4.04	3.91	2.32	4.38	4.41
<b>MgO</b>	4.52	4.23	3.99	3.36	4.77	2.74	2.10	3.96	4.18
<b>CaO</b>	8.76	9.07	9.30	8.69	5.58	9.03	5.04	9.41	9.10
<b>Na<sub>2</sub>O</b>	4.47	5.31	5.20	5.72	6.52	5.53	9.88	5.20	5.31
<b>K<sub>2</sub>O</b>	1.02	1.10	1.13	1.06	1.48	1.20	1.87	1.10	1.07
<b>TiO<sub>2</sub></b>	1.24	1.43	1.32	1.45	1.22	1.38	0.59	1.36	1.35
<b>MnO</b>	0.08	0.08	0.07	0.07	0.10	0.05	0.06	0.06	0.09
<b>P<sub>2</sub>O<sub>5</sub></b>	0.25	0.31	0.28	0.30	0.32	0.26	0.39	0.30	0.32
<b>F</b>	0.03	0.12	0.33	0.06	0.09	0.20	0.05	0.07	0.09
<b>S</b>	0.19	0.22	0.20	0.23	0.10	0.20	0.06	0.18	0.21
<b>Cl</b>	0.09	0.10	0.09	0.11	0.12	0.09	0.15	0.08	0.08
<b>H<sub>2</sub>O</b>	5.3	4.9	2.8	3.1	0.4	2.6	0.5	5.1	3.7
<b>CO<sub>2</sub></b>	2413	2128	1155	959	bdl	950	286	1708	1290
<b>TOTAL</b>	100.77	101.11	99.29	98.10	99.04	98.51	102.25	101.53	100.71

**Table DR3**

	SO <sub>2</sub> (t/d)	CO <sub>2</sub> (t/d)	CO <sub>2</sub> /SO <sub>2</sub>	HCl/SO <sub>2</sub>	SO <sub>2</sub> emmission (Mt)	Ratio method	Reference
May 15, 1995	1300	≤10000	4-8			GASPEC	Goff et al., 2001
June 1995			1-2			LICOR	Gerlach et al., 1997
April 23, 1997	7200	33000	4.6			LICOR	Delgado-Granados unpublished data
June 19 1997	6150	37000	6			LICOR	Delgado-Granados unpublished data
1995 to 1998				0.12*		*	Goff et al., 2001
1995 to 1997					9 Mt	COSPEC	Delgado-Granados et al., 2001
1998	1350	190000	≤140			FTIR	Goff et al., 2001

\* Average from 1995 to 1998 using different ratio methods (alkaline traps, leachate and FTIR)