

**MARTENS ET AL., FOR DATA REPOSITORY**

**U/Pb geochronology of Devonian and older Paleozoic beds in the southeastern Maya Block, Central America: its affinity with Peri-Gondwanan terranes**

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**INTRODUCTION**

Supplementary data presented here include concentration and isotopic ratios for U/Pb zircon ages performed by Laser Ablation ICP-MS. An overview of the technique employed for the single crystal laser ablation ICP multicollector mass spectrometric technique (LA-ICP-MS) at the Arizona Laserchron Center is included.

**ANALYTICAL TECHNIQUES**

After crushing and pulverizing samples, zircon grains were concentrated by Wilfley ® shaking table, Frantz ® isodynamic separator, methylene iodide and hand picking. Final zircon concentrates were sieved and grains >40 µm were selected for analysis.

Zircon unknowns and standards were mounted on the center of 1 inch phenolic O-rings and polished to expose grain interiors. Analyzed detrital zircons were selected

randomly. Each measurement cycle consisted of one 20s integration on every centered peak with the laser off for background counts, twenty 1s integrations during mineral blasting, and ~30s of purging. Zircons were ablated with a New Wave Research DUV193 ArF Excimer laser (wavelength = 193 nm). The laser beam was operated with ~32mJ energy (at 23kV), pulse rate of 9Hz, and spot size of 35 $\mu$ m or 50  $\mu$ m depending on size and complexity of zircons. The generated pit was ~10  $\mu$ m deep. Ablated material was carried in helium gas into an Isoprobe ICPMS from GV Instruments. U, Th and Pb isotopes were analyzed simultaneously in static mode using Faraday collectors for  $^{238}\text{U}$ ,  $^{232}\text{U}$ ,  $^{208}\text{Pb}$ ,  $^{207}\text{Pb}$  and  $^{206}\text{Pb}$ , and using an ion counter for  $^{204}\text{Pb}$ . Contributions to the 204 mass by Hg were removed by subtracting background counts. Common Pb corrections were calculated from  $^{204}\text{Pb}$  measurements and assuming an initial isotopic composition according to the Pb evolution curve by Stacey and Kramers (1975).

Fragments of NIST 610 trace element glass were analyzed with every sample to determine concentrations of U and Th. Five Sri Lanka zircon standards (564 $\pm$ 4 Ma, 2-sigma error) were analyzed before each sample and once every five unknowns. Corrections for Th/U, Pb/U and (minor) Pb/Pb fractionation were carried out by comparison to the moving-average of 6 standards. Due to increment in inter-element fractionation with pit depth by as much as 5%, a least-squares fit through the measured values was performed to calculate the initial value. Grains that showed >10% change in isotopic ratio during analysis, possibly due to age zoning, were discarded from the study.

Systematic errors were propagated separately, and include uncertainty of standard age, calibration correction of standard, composition of common Pb, and U decay constant. Values selected for concordia and probability density plots were  $^{206}\text{Pb}/^{207}\text{Pb}$  age for samples older than 900 Ma, and  $^{206}\text{Pb}/^{238}\text{U}$  age for younger zircons. Analysis with >5% discordance, high  $^{206}\text{Pb}/^{238}\text{U}$  or  $^{206}\text{Pb}/^{207}\text{Pb}$  errors (>10%) were considered unreliable and were disregarded.

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Table DR1. Concentrations, isotopic ratios and ages of zircon.

U ( P P m )	$^{206}\text{Pb}$ / $^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*/$ $^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*/$ $^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*/$ $^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*/$ $^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*/$ $^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
1 4 4	3177	1.38	0.4663 3	6.8	0.05679	3.9	0.56	356 .1	13.3	388.7	22.0	587.6	122. 4	<b>356.1</b>	13.3
3 0 5	5352	1.01	0.5012 7	3.2	0.06124	1.6	0.52	383 .2	6.1	412.6	10.7	580.3	58.4	<b>383.2</b>	6.1
7 5	2765	1.11	0.5198 8	7.1	0.06297	4.6	0.64	393 .7	17.4	425.1	24.7	599.1	118. 0	<b>393.7</b>	17.4
9 0	3518	0.74	0.4976 7	3.6	0.06358	1.2	0.35	397 .4	4.8	410.1	12.0	482.6	73.5	<b>397.4</b>	4.8
1 0 4	2963	1.45	0.5127 8	3.7	0.06394	1.2	0.32	399 .5	4.6	420.3	12.6	536.0	75.9	<b>399.5</b>	4.6
1 0 0	3536	1.24	0.5239 3	8.4	0.06403	2.3	0.28	400 .1	9.1	427.8	29.3	579.9	175. 3	<b>400.1</b>	9.1
2 2 3	9559	0.96	0.4949 9	2.0	0.06425	1.2	0.59	401 .4	4.5	408.3	6.7	447.2	35.6	<b>401.4</b>	4.5
1 0 7 7	7823	0.80	0.5376 1	9.4	0.06427	3.8	0.40	401 .6	14.7	436.8	33.4	627.4	186. 1	<b>401.6</b>	14.7
1 2 1	5082	1.08	0.4995 8	5.6	0.06442	1.0	0.18	402 .5	3.9	411.4	18.9	462.0	121. 7	<b>402.5</b>	3.9
2 0 9	3518	1.31	0.5766 7	13.3	0.06454	4.7	0.35	403 .2	18.2	462.3	49.4	768.1	262. 9	<b>403.2</b>	18.2
1 9 8	10211	0.91	0.4880 7	3.3	0.06484	2.5	0.76	405 .0	10.0	403.6	11.1	395.7	48.1	<b>405.0</b>	10.0
7 7	3359	1.18	0.5194 7	6.3	0.06496	1.6	0.26	405 .7	6.4	424.8	21.8	529.5	133. 3	<b>405.7</b>	6.4
5 7 1	18034	0.75	0.5026 6	3.1	0.06505	2.6	0.84	406 .3	10.3	413.5	10.6	454.2	37.5	<b>406.3</b>	10.3
7 3 2	26116	1.09	0.4945 4	2.9	0.06515	2.7	0.94	406 .9	10.5	408.0	9.6	414.3	22.4	<b>406.9</b>	10.5
9 0 0	4993	1.15	0.5588 1	7.5	0.06517	6.0	0.81	407 .0	23.7	450.7	27.1	680.6	94.4	<b>407.0</b>	23.7
1 7 7	6649	1.01	0.5079 4	3.3	0.06588	1.3	0.39	411 .3	5.2	417.1	11.4	449.2	67.9	<b>411.3</b>	5.2
7	12718	0.94	0.5163	3.7	0.06602	3.5	0.92	412	13.8	422.7	12.9	480.7	31.5	<b>412.2</b>	13.8

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U ( P P m )	$^{206}\text{Pb}$ $/^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}$ $/^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $/^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)	
9 4			7					.2								
1 3 7	3954	1.32	0.5459 0	3.7	0.06634	1.9	0.51	414 .1	7.5	442.3	13.2	592.0	68.7	414.1	7.5	
1 1 8	6560	1.07	0.5147 9	4.4	0.06663	2.1	0.47	415 .8	8.3	421.7	15.2	453.8	86.6	415.8	8.3	
4 3	2419	0.61	0.5032 3	10.9	0.06691	1.7	0.16	417 .5	6.9	413.9	37.0	393.6	241. 4	417.5	6.9	
2 1 9	4742	0.89	0.5581 4	9.3	0.06721	6.9	0.74	419 .3	27.9	450.3	33.8	611.7	135. 3	419.3	27.9	
5 6 8	7596	1.64	0.5596 2	7.3	0.06895	6.8	0.94	429 .8	28.4	451.3	26.6	562.2	55.1	429.8	28.4	
1 1 7	5268	0.95	0.5345 9	5.5	0.06909	1.1	0.20	430 .7	4.6	434.9	19.5	457.0	119. 9	430.7	4.6	
3 7 3	21962	0.77	0.5363 2	2.3	0.07005	2.0	0.89	436 .4	8.4	436.0	8.0	433.7	23.4	436.4	8.4	
1 3 3	3207	1.03	0.6229 7	7.0	0.07287	1.3	0.18	453 .4	5.5	491.7	27.4	674.3	148. 1	453.4	5.5	
3 1 6	21951	0.88	1.3772 6	1.9	0.14183	1.5	0.83	855 .0	12.4	879.3	11.0	940.9	21.4	855.0	12.4	
1 0 9	8966	1.65	0.6633 2	2.9	0.08356	2.1	0.71	517 .3	10.3	516.6	11.9	513.7	45.3	517.3	10.3	
2 9 2	29118	0.47	1.1675 5	1.4	0.12904	1.0	0.71	782 .4	7.4	785.5	7.7	794.3	21.0	782.4	7.4	
4 7 7	53777	0.53	1.4626 3	1.5	0.15209	1.1	0.75	912 .7	9.7	915.1	9.1	920.9	20.6	920.9	20.6	
2 4 9	37962	0.26	1.5214 4	1.4	0.15788	1.0	0.71	945 .0	8.8	939.1	8.7	925.2	20.6	925.2	20.6	
7 3	7659	0.81	1.4926 7	2.3	0.15469	1.2	0.54	927 .2	10.7	927.4	14.0	927.8	40.0	927.8	40.0	
3 2 1	32418	0.37	1.4622 3	2.3	0.15150	2.1	0.90	909 .4	17.8	914.9	14.0	928.3	20.6	928.3	20.6	
4 9	6491	0.45	1.5159 6	2.3	0.15657	1.0	0.43	937 .7	8.7	936.8	14.1	934.8	42.7	934.8	42.7	

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U ( P P m )	$^{206}\text{Pb}$ $\text{/}^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $\text{/}^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
1 4 4	20570	0.43	1.5076 3	1.8	0.15540	1.5	0.83	931 .1	12.7	933.5	10.9	939.0	20.6	<b>939.0</b>	20.6
1 4 3	20079	0.58	1.5512 3	1.7	0.15973	1.4	0.80	955 .3	12.1	951.0	10.5	941.0	20.7	<b>941.0</b>	20.7
1 3 3	16636	0.97	1.5097 0	1.8	0.15416	1.2	0.70	924 .2	10.8	934.3	10.9	958.2	26.1	<b>958.2</b>	26.1
1 9 3	16427	0.78	1.5047 2	1.6	0.15265	1.0	0.64	915 .8	8.5	932.3	9.5	971.5	24.3	<b>971.5</b>	24.3
6 1	8063	0.54	1.6586 0	1.7	0.16826	1.0	0.59	100 2.5	9.3	992.8	10.7	971.5	27.8	<b>971.5</b>	27.8
6 2	10358	0.70	1.6828 0	2.2	0.17032	1.3	0.59	101 3.9	12.1	1002.0	13.9	976.3	35.9	<b>976.3</b>	35.9
7 0	8571	0.67	1.6174 2	1.8	0.16269	1.5	0.80	971 .7	13.1	977.0	11.4	988.8	22.1	<b>988.8</b>	22.1
1 2 4	17485	0.44	1.6979 4	1.4	0.17039	1.0	0.70	101 4.3	9.4	1007.8	9.1	993.6	20.8	<b>993.6</b>	20.8
1 7 9	22661	0.50	1.6316 2	1.9	0.16356	1.6	0.84	976 .5	14.2	982.5	11.7	995.8	20.4	<b>995.8</b>	20.4
5 8	11259	0.57	1.7559 8	1.7	0.17593	1.1	0.68	104 4.7	11.0	1029.4	10.9	996.9	25.1	<b>996.9</b>	25.1
7 7	12218	0.54	1.7181 6	1.9	0.17213	1.3	0.72	102 3.9	12.6	1015.3	11.9	997.0	26.2	<b>997.0</b>	26.2
1 3 3	20352	0.61	1.6951 8	2.1	0.16972	1.9	0.88	101 0.6	17.5	1006.7	13.6	998.3	20.4	<b>998.3</b>	20.4
1 2 6	17679	0.53	1.6541 6	1.9	0.16559	1.6	0.85	987 .8	14.7	991.1	12.0	998.6	20.4	<b>998.6</b>	20.4
7 6	10187	1.12	1.6730 9	2.0	0.16735	1.3	0.63	997 .5	11.6	998.4	12.7	1000.2	31.6	<b>1000. 2</b>	31.6
1 5 6	21554	0.56	1.7271 6	1.5	0.17273	1.0	0.67	102 7.2	9.5	1018.7	9.6	1000.5	22.4	<b>1000. 5</b>	22.4
2 3 8	36496	0.48	1.7467 8	1.5	0.17453	1.1	0.74	103 7.0	10.6	1026.0	9.7	1002.4	20.3	<b>1002. 4</b>	20.3
6 3	8353	0.36	1.7132 4	1.8	0.17092	1.1	0.64	101 7.2	10.6	1013.5	11.3	1005.5	27.5	<b>1005. 5</b>	27.5
1 5 6	25943	0.40	1.7375 0	1.4	0.17325	1.0	0.71	103 0.0	9.5	1022.5	9.1	1006.6	20.3	<b>1006. 6</b>	20.3

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1 2 3	18197	0.47	1.6905 7	1.5	0.16850	1.0	0.66	100 3.8	9.3	1005.0	9.7	1007.4	23.3	1007. 4	23.3
1 9 5	24835	0.48	1.6656 8	1.4	0.16599	1.0	0.71	990 .0	9.2	995.5	9.0	1007.7	20.3	1007. 7	20.3
9 1 9	97083	0.05	1.7013 3	1.8	0.16941	1.5	0.83	100 8.9	13.7	1009.0	11.3	1009.4	20.3	1009. 4	20.3
2 1 2	30899	0.43	1.7237 6	1.4	0.17158	1.0	0.71	102 0.8	9.4	1017.4	9.1	1010.1	20.3	1010. 1	20.3
6 5	9168	0.40	1.6835 0	2.6	0.16755	1.7	0.64	998 .6	15.6	1002.3	16.8	1010.4	41.1	1010. 4	41.1
1 5 6	17496	0.27	1.7316 9	2.6	0.17227	2.4	0.92	102 4.6	22.7	1020.4	16.7	1011.3	20.5	1011. 3	20.5
1 0 5	15899	0.51	1.7464 8	1.5	0.17369	1.1	0.75	103 2.4	11.0	1025.9	9.9	1011.9	20.4	1011. 9	20.4
1 0 3	15365	0.53	1.7021 0	2.2	0.16927	1.9	0.88	100 8.1	18.0	1009.3	14.1	1011.9	21.3	1011. 9	21.3
1 1 8	13855	0.49	1.6490 6	1.7	0.16399	1.3	0.78	978 .9	12.2	989.2	10.8	1012.0	21.6	1012. 0	21.6
4 7	5845	0.49	1.6922 6	2.1	0.16826	1.8	0.86	100 2.5	17.0	1005.6	13.5	1012.3	21.6	1012. 3	21.6
1 6 4	28978	0.47	1.7959 6	1.7	0.17823	1.3	0.80	105 7.3	13.0	1044.0	10.9	1016.2	20.3	1016. 2	20.3
1 1 0	15118	0.64	1.7604 4	1.7	0.17458	1.4	0.81	103 7.3	13.4	1031.0	11.3	1017.7	20.8	1017. 7	20.8
1 9 2	23918	0.34	1.7306 4	2.0	0.17160	1.8	0.87	102 0.9	16.5	1020.0	13.0	1017.9	20.3	1017. 9	20.3
4 0	5970	0.52	1.7095 9	2.5	0.16950	1.8	0.69	100 9.3	16.4	1012.1	16.2	1018.1	36.8	1018. 1	36.8
1 2 0	16800	0.42	1.6927 9	1.5	0.16770	1.0	0.67	999 .4	9.3	1005.8	9.5	1019.8	22.3	1019. 8	22.3
7 6	11352	0.45	1.7631 3	1.9	0.17462	1.1	0.61	103 7.5	11.0	1032.0	12.1	1020.3	29.8	1020. 3	29.8
1 9 6	25123	0.67	1.7151 0	1.4	0.16967	1.0	0.71	101 0.3	9.4	1014.2	9.1	1022.7	20.3	1022. 7	20.3
7	12139	0.38	1.7282	2.0	0.17093	1.7	0.86	101	15.7	1019.1	12.5	1023.1	20.4	1023. 2	20.4

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4			9					7.3							1	
1 3 6	20896	0.45	1.6920 4	1.8	0.16729	1.5	0.83	997 .2	14.0	1005.5	11.6	1023.8	20.4	1023. 8	20.4	
4 5	7326	0.94	1.6932 4	2.4	0.16694	1.2	0.50	995 .2	10.8	1006.0	15.0	1029.5	41.3	1029. 5	41.3	
1 1 5	18389	0.47	1.7411 5	1.8	0.17164	1.5	0.84	102 1.2	14.6	1023.9	11.9	1029.7	20.3	1029. 7	20.3	
1 5 1	20937	0.42	1.6951 1	1.4	0.16684	1.0	0.72	994 .7	9.6	1006.7	9.2	1032.9	20.3	1032. 9	20.3	
1 1 9	10789	0.63	1.7882 3	2.0	0.17577	1.6	0.81	104 3.8	15.8	1041.2	13.2	1035.6	24.3	1035. 6	24.3	
9 2	12666	0.35	1.8382 0	2.1	0.17976	1.8	0.87	106 5.7	17.5	1059.2	13.5	1045.9	20.4	1045. 9	20.4	
6 1	8946	0.43	1.7332 1	2.6	0.16940	2.3	0.86	100 8.8	21.2	1020.9	17.0	1047.0	27.4	1047. 0	27.4	
3 0	4789	0.77	1.7875 6	4.8	0.17425	2.8	0.59	103 5.5	26.8	1040.9	31.0	1052.3	77.5	1052. 3	77.5	
8 8	11166	1.16	1.7975 2	2.5	0.17516	2.2	0.87	104 0.5	21.0	1044.6	16.3	1053.0	24.8	1053. 0	24.8	
5 4	7896	0.77	1.8379 6	3.4	0.17899	2.6	0.77	106 1.5	25.7	1059.1	22.4	1054.3	43.6	1054. 3	43.6	
6 9 4	82403	0.37	1.8856 2	2.5	0.18336	2.3	0.92	108 5.3	23.0	1076.0	16.7	1057.3	20.1	1057. 3	20.1	
4 4	6941	0.46	1.7607 4	2.5	0.17101	1.9	0.73	101 7.7	17.5	1031.1	16.5	1059.8	35.0	1059. 8	35.0	
7 1	9792	1.39	1.8455 4	1.5	0.17626	1.1	0.73	104 6.5	10.6	1061.8	9.8	1093.5	20.3	1093. 5	20.3	
1 3 3	12070	0.55	1.9569 9	1.4	0.18537	1.0	0.72	109 6.2	10.5	1100.9	9.7	1110.0	20.2	1110. 0	20.2	
2 4 2	33187	0.41	1.9705 1	1.4	0.18657	1.0	0.71	110 2.8	10.1	1105.5	9.5	1110.8	20.0	1110. 8	20.0	
5 5 9	82179	0.25	2.0151 5	1.8	0.19021	1.5	0.82	112 2.5	15.0	1120.6	12.0	1117.0	20.0	1117. 0	20.0	
8 1	11974	0.49	2.0579 7	1.6	0.19214	1.0	0.63	113 3.0	10.4	1134.9	10.9	1138.7	24.8	1138. 7	24.8	
2 4 7	45356	0.41	2.1012 9	2.4	0.19597	2.2	0.91	115 3.6	23.6	1149.2	16.8	1140.9	19.9	1140. 9	19.9	

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U ( P P m )	$^{206}\text{Pb}$ $/^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $/^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
3 6 5	45971	0.62	2.1398 3	1.4	0.19842	1.0	0.71	116 6.8	10.7	1161.8	9.8	1152.3	19.9	1152. 3	19.9
1 5 2	24790	0.39	2.0959 7	2.6	0.19404	2.4	0.92	114 3.2	25.1	1147.5	17.8	1155.5	19.9	1155. 5	19.9
4 6 2	9683	0.54	1.8302 5	2.9	0.16755	2.7	0.94	998 .6	25.3	1056.4	19.2	1177.7	20.3	1177. 7	20.3
7 7	14972	0.96	2.1924 6	1.4	0.19991	1.0	0.71	117 4.8	10.7	1178.6	9.9	1185.6	19.8	1185. 6	19.8
1 7 1	31922	0.78	2.2145 6	1.5	0.20190	1.1	0.75	118 5.5	12.1	1185.7	10.5	1185.9	19.8	1185. 9	19.8
4 9	8176	0.75	2.2019 5	3.7	0.20074	3.5	0.96	117 9.3	37.8	1181.7	25.5	1186.0	20.3	1186. 0	20.3
1 7 4	27936	0.79	2.2067 5	1.7	0.20056	1.3	0.80	117 8.3	14.2	1183.2	11.6	1192.1	19.8	1192. 1	19.8
4 5 8	77749	0.20	2.2903 2	1.7	0.20804	1.3	0.80	121 8.4	15.0	1209.3	11.9	1193.1	19.7	1193. 1	19.7
2 6 2	41193	0.80	2.3213 8	1.4	0.20985	1.0	0.71	122 8.0	11.2	1218.8	10.0	1202.7	19.7	1202. 7	19.7
1 9 5	33982	1.20	2.2762 6	1.4	0.20541	1.0	0.71	120 4.3	11.0	1205.0	10.0	1206.1	19.7	1206. 1	19.7
8 8	13166	0.83	2.2475 6	1.5	0.20249	1.1	0.74	118 8.7	12.0	1196.0	10.5	1209.3	19.7	1209. 3	19.7
1 1 0	19875	1.12	2.3213 5	1.4	0.20877	1.0	0.71	122 2.3	11.1	1218.8	10.0	1212.8	19.7	1212. 8	19.7
3 0 9	35472	0.89	2.2917 3	1.4	0.20597	1.0	0.71	120 7.3	11.0	1209.7	10.0	1214.1	19.7	1214. 1	19.7
4 5 4	74197	0.11	2.4196 6	1.4	0.21630	1.0	0.71	126 2.3	11.5	1248.5	10.2	1224.6	19.6	1224. 6	19.6
1 7 4	20547	0.51	2.2828 5	1.5	0.20391	1.1	0.74	119 6.3	12.2	1207.0	10.6	1226.2	19.7	1226. 2	19.7
2 1 3	27661	0.45	2.3347 5	1.5	0.20803	1.1	0.74	121 8.3	12.3	1222.9	10.6	1231.0	19.6	1231. 0	19.6
1 6 3	31475	0.39	2.4339 9	1.4	0.21652	1.0	0.71	126 3.5	11.5	1252.7	10.2	1234.2	19.6	1234. 2	19.6

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U ( P P m )	$^{206}\text{Pb}$ $/^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $/^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
9 4	18471	0.59	2.4803 0	2.1	0.22032	1.9	0.88	128 3.6	21.7	1266.3	15.4	1237.1	19.9	1237. 1	19.9
3 6 8	41606	0.58	2.4250 8	2.0	0.21299	1.6	0.80	124 4.7	18.4	1250.1	14.6	1259.2	23.8	1259. 2	23.8
1 3 1	23715	1.14	2.4822 6	1.4	0.21751	1.0	0.71	126 8.7	11.5	1266.9	10.2	1263.8	19.6	1263. 8	19.6
4 0 1	72050	0.57	2.5532 9	2.3	0.22139	2.1	0.90	128 9.2	24.0	1287.4	16.7	1284.3	19.5	1284. 3	19.5
3 8 6	59868	0.46	2.5596 7	3.4	0.22175	3.2	0.96	129 1.1	37.9	1289.2	24.7	1286.0	19.5	1286. 0	19.5
1 2 5	21636	0.88	2.6371 0	1.4	0.22675	1.0	0.71	131 7.4	11.9	1311.1	10.4	1300.6	19.5	1300. 6	19.5
1 9 9	11636	0.53	2.6633 0	2.5	0.22778	2.3	0.92	132 2.8	27.9	1318.3	18.8	1311.0	19.9	1311. 0	19.9
2 4 5	42205	0.51	2.8520 0	2.1	0.23396	1.9	0.88	135 5.2	23.2	1369.3	16.1	1391.4	19.2	1391. 4	19.2
2 5 6	63127	0.47	3.2620 8	1.7	0.25737	1.4	0.81	147 6.4	17.9	1472.1	13.1	1465.9	19.0	1465. 9	19.0
1 9 3	34624	0.47	3.3938 4	1.4	0.26366	1.0	0.71	150 8.6	13.5	1503.0	11.1	1495.1	18.9	1495. 1	18.9
2 5 5	42151	0.49	3.5224 4	1.4	0.26837	1.0	0.71	153 2.5	13.6	1532.3	11.2	1531.9	18.8	1531. 9	18.8
4 2 3	94536	0.21	3.5513 1	1.9	0.26894	1.6	0.85	153 5.4	22.0	1538.7	15.0	1543.2	18.8	1543. 2	18.8
1 6 2	39110	0.52	3.5535 2	2.6	0.26872	2.4	0.93	153 4.3	33.3	1539.2	20.9	1545.9	18.8	1545. 9	18.8
6 7	17831	0.59	3.6903 1	2.1	0.27592	1.8	0.87	157 0.8	25.2	1569.3	16.6	1567.2	19.2	1567. 2	19.2
1 9 8	3696	0.64	3.7403 0	4.3	0.26550	2.4	0.56	151 7.9	33.1	1580.0	34.7	1664.0	66.2	1664. 0	66.2
9 6	20096	0.69	4.5067 8	3.1	0.30851	3.0	0.95	173 3.4	44.9	1732.2	25.9	1730.8	18.4	1730. 8	18.4
2 4 6	20543	0.81	0.8072 4	2.0	0.09681	1.7	0.86	595 .7	9.8	600.9	9.0	620.7	21.7	595.7	9.8

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U ( P P m )	$^{206}\text{Pb}$ $/^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $/^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
2 3 6	24443	1.02	1.1790 3	2.0	0.13078	1.7	0.87	792 .3	12.9	790.9	11.0	786.7	21.0	<b>792.3</b>	12.9
1 9	2220	1.01	1.4753 9	4.1	0.15265	1.6	0.38	915 .8	13.4	920.3	24.7	931.3	77.4	<b>931.3</b>	77.4
9 1 6	17153	0.46	1.5759 6	1.6	0.16297	1.2	0.75	973 .3	11.1	960.8	10.2	932.3	22.2	<b>932.3</b>	22.2
3 7	5747	0.46	1.5768 7	3.1	0.15951	1.0	0.32	954 .1	8.9	961.1	19.5	977.4	60.6	<b>977.4</b>	60.6
3 6	5747	0.58	1.6424 1	2.4	0.16608	1.7	0.70	990 .5	15.7	986.6	15.4	978.1	35.5	<b>978.1</b>	35.5
7 0	10225	0.66	1.6586 1	1.7	0.16718	1.0	0.60	996 .5	9.7	992.8	11.0	984.7	28.1	<b>984.7</b>	28.1
1 6 9	23710	0.34	1.7225 3	1.6	0.17358	1.2	0.78	103 1.8	11.9	1017.0	10.3	985.1	20.4	<b>985.1</b>	20.4
3 2	5082	0.93	1.6561 3	3.8	0.16667	1.0	0.27	993 .7	9.4	991.9	24.2	987.9	74.9	<b>987.9</b>	74.9
9 1	14592	0.61	1.6333 9	3.1	0.16433	2.0	0.64	980 .8	17.9	983.2	19.4	988.5	48.1	<b>988.5</b>	48.1
3 4	5660	1.18	1.6191 8	2.6	0.16279	1.6	0.60	972 .3	14.0	977.7	16.2	989.8	41.9	<b>989.8</b>	41.9
1 6 4	25816	0.48	1.7040 6	1.8	0.17129	1.5	0.84	101 9.2	14.5	1010.1	11.8	990.3	20.4	<b>990.3</b>	20.4
8 7	13043	1.08	1.6537 7	1.6	0.16618	1.0	0.63	991 .0	9.2	991.0	10.0	990.9	24.8	<b>990.9</b>	24.8
5 7	9518	0.37	1.6581 8	2.5	0.16653	1.6	0.64	993 .0	14.5	992.7	15.5	992.0	38.2	<b>992.0</b>	38.2
3 1 3	47749	0.47	1.6792 6	1.4	0.16848	1.0	0.71	100 3.8	9.3	1000.7	9.0	994.0	20.3	<b>994.0</b>	20.3
2 3 0	34361	0.52	1.6590 7	1.6	0.16640	1.2	0.77	992 .2	11.0	993.0	9.9	994.7	20.4	<b>994.7</b>	20.4
9 4	14910	0.45	1.6506 6	2.1	0.16553	1.8	0.85	987 .4	16.3	989.8	13.2	995.0	22.1	<b>995.0</b>	22.1
2 6 4	33038	0.93	1.7097 4	1.4	0.17143	1.0	0.71	102 0.0	9.4	1012.2	9.1	995.4	20.4	<b>995.4</b>	20.4
2 1 4	33477	0.35	1.7327 2	1.5	0.17366	1.2	0.76	103 2.2	11.0	1020.8	9.8	996.2	20.3	<b>996.2</b>	20.3
1 4 0	20241	1.12	1.7156 6	1.7	0.17194	1.3	0.77	102 2.8	12.2	1014.4	10.7	996.3	21.4	<b>996.3</b>	21.4

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U ( P P m )	$^{206}\text{Pb}$ $\text{/}^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $\text{/}^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
1 1 2	17397	0.34	1.6817 8	1.4	0.16851	1.0	0.71	100 3.9	9.3	1001.7	9.0	996.8	20.4	<b>996.8</b>	20.4
6 0	9251	0.50	1.7170 1	1.5	0.17191	1.0	0.65	102 2.6	9.5	1014.9	9.9	998.3	23.9	<b>998.3</b>	23.9
8 8	14842	0.90	1.6792 8	2.2	0.16805	1.7	0.77	100 1.4	15.5	1000.7	13.9	999.2	28.5	<b>999.2</b>	28.5
2 0 9	31259	0.45	1.6797 7	1.8	0.16802	1.4	0.82	100 1.2	13.3	1000.9	11.2	1000.2	20.4	<b>1000.</b> 2	20.4
9 0	13322	0.33	1.7704 7	1.9	0.17686	1.6	0.85	104 9.8	15.6	1034.7	12.3	1002.9	20.4	<b>1002.</b> 9	20.4
3 1 4	46616	0.40	1.6569 8	1.6	0.16541	1.2	0.78	986 .8	11.4	992.2	10.1	1004.3	20.3	<b>1004.</b> 3	20.3
1 3 8	22088	0.52	1.7138 5	1.7	0.17106	1.4	0.81	101 7.9	13.1	1013.7	11.0	1004.6	20.3	<b>1004.</b> 6	20.3
1 4 9	24372	0.62	1.7020 9	1.8	0.16986	1.4	0.82	101 1.4	13.5	1009.3	11.2	1004.9	20.3	<b>1004.</b> 9	20.3
7 3	11772	0.75	1.6687 5	1.7	0.16650	1.0	0.60	992 .8	9.2	996.7	10.6	1005.3	27.0	<b>1005.</b> 3	27.0
1 6 7 8	91827	0.52	1.7265 4	1.4	0.17219	1.0	0.71	102 4.2	9.5	1018.5	9.1	1006.2	20.3	<b>1006.</b> 2	20.3
1 4 6	20865	0.46	1.6698 4	3.9	0.16652	3.8	0.97	992 .9	34.8	997.1	24.9	1006.4	20.6	<b>1006.</b> 4	20.6
8 4	13460	0.79	1.7393 8	1.5	0.17344	1.1	0.73	103 1.0	10.5	1023.2	9.7	1006.6	20.8	<b>1006.</b> 6	20.8
9 2	15814	0.51	1.6632 9	1.8	0.16583	1.3	0.74	989 .1	12.1	994.6	11.4	1006.8	24.8	<b>1006.</b> 8	24.8
5 0	8382	0.44	1.6750 3	2.4	0.16696	2.1	0.89	995 .3	19.6	999.1	15.1	1007.3	21.5	<b>1007.</b> 3	21.5
1 7 7	27637	0.45	1.7036 4	1.4	0.16977	1.0	0.71	101 0.8	9.4	1009.9	9.1	1007.8	20.3	<b>1007.</b> 8	20.3
7 5	11866	0.62	1.6837 4	2.4	0.16777	2.0	0.85	999 .8	18.6	1002.4	15.0	1008.1	24.9	<b>1008.</b> 1	24.9
1 4 5	21199	0.41	1.6965 3	1.4	0.16898	1.0	0.71	100 6.5	9.3	1007.2	9.0	1008.8	20.3	<b>1008.</b> 8	20.3
2 3 8	33403	0.27	1.7453 0	1.6	0.17383	1.3	0.78	103 3.2	12.1	1025.4	10.4	1008.9	20.3	<b>1008.</b> 9	20.3

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U ( P P m )	$^{206}\text{Pb}$ $/^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $/^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
102	16635	0.50	1.66241	1.8	0.16539	1.4	0.82	986.7	13.2	994.3	11.1	1011.2	20.5	1011.2	20.5
161	23912	0.74	1.69150	1.4	0.16813	1.0	0.70	100.18	9.3	1005.3	9.1	1013.0	20.4	1013.0	20.4
63	9145	0.50	1.63290	2.3	0.16227	1.5	0.65	969.4	13.7	983.0	14.7	1013.5	35.9	1013.5	35.9
56	8991	0.58	1.74590	1.8	0.17345	1.4	0.79	103.11	13.8	1025.6	11.8	1014.0	23.0	1014.0	23.0
60	7355	0.74	1.66550	3.0	0.16544	2.3	0.76	987.0	20.7	995.5	18.9	1014.3	39.2	1014.3	39.2
222	31718	0.70	1.73781	1.4	0.17258	1.0	0.71	102.6.3	9.5	1022.7	9.1	1014.8	20.3	1014.8	20.3
136	22829	0.36	1.76178	1.4	0.17479	1.0	0.71	103.8.5	9.8	1031.5	9.3	1016.8	20.3	1016.8	20.3
108	17889	0.42	1.68884	2.8	0.16732	2.6	0.92	997.3	24.0	1004.3	18.1	1019.6	22.6	1019.6	22.6
219	40992	0.37	1.77556	1.8	0.17590	1.5	0.83	104.4.6	14.4	1036.6	11.7	1019.7	20.3	1019.7	20.3
105	16606	0.35	1.68686	1.6	0.16708	1.0	0.61	996.0	9.2	1003.6	10.5	1020.1	26.4	1020.1	26.4
70	13250	0.43	1.64524	1.9	0.16294	1.5	0.81	973.1	13.8	987.7	12.0	1020.3	22.8	1020.3	22.8
113	18375	0.38	1.74207	1.4	0.17249	1.0	0.70	102.5.8	9.5	1024.2	9.2	1020.8	20.5	1020.8	20.5
148	21608	0.37	1.75859	2.4	0.17400	2.2	0.91	103.4.1	21.1	1030.3	15.7	1022.3	20.4	1022.3	20.4
257	20519	0.55	1.73399	2.1	0.17131	1.9	0.88	101.9.3	17.7	1021.2	13.7	1025.3	20.4	1025.3	20.4
201	29619	0.43	1.69653	1.9	0.16758	1.6	0.84	998.8	14.5	1007.2	11.9	1025.6	20.2	1025.6	20.2
64	10034	0.47	1.73414	1.7	0.17121	1.0	0.59	101.8.8	9.4	1021.3	11.0	1026.7	28.0	1026.7	28.0
62	5889	1.21	1.66977	1.7	0.16449	1.0	0.60	981.7	9.1	997.1	10.5	1031.1	26.8	1031.1	26.8
120	11252	0.95	1.69142	1.5	0.16662	1.0	0.69	993.5	9.2	1005.3	9.3	1031.2	21.3	1031.2	21.3

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U ( P P m )	$^{206}\text{Pb}$ $\text{/}^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $\text{/}^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
1 2 0	19458	0.38	1.6867 3	1.9	0.16599	1.4	0.71	990 .0	12.4	1003.5	12.1	1033.2	26.9	1033. 2	26.9
5 3	7795	0.54	1.7932 9	2.6	0.17646	1.0	0.38	104 7.6	9.7	1043.0	17.0	1033.4	48.5	1033. 4	48.5
5 6	8888	0.72	1.7454 5	2.4	0.17121	2.0	0.83	101 8.8	19.2	1025.5	15.8	1039.8	27.3	1039. 8	27.3
1 5 9	17008	0.60	1.6977 8	2.1	0.16644	1.0	0.49	992 .5	9.6	1007.7	13.6	1041.0	37.5	1041. 0	37.5
1 7 5	31040	0.45	1.7909 2	1.7	0.17514	1.4	0.82	104 0.4	13.5	1042.2	11.3	1045.9	20.2	1045. 9	20.2
1 6 5	26442	0.81	1.7803 1	2.2	0.17352	1.9	0.88	103 1.5	18.1	1038.3	14.0	1052.7	20.2	1052. 7	20.2
1 1 0	16458	0.45	1.8048 3	1.6	0.17549	1.0	0.61	104 2.3	9.6	1047.2	10.6	1057.5	25.9	1057. 5	25.9
2 9 3	43314	0.29	1.9036 6	1.5	0.18473	1.2	0.76	109 2.8	11.8	1082.4	10.2	1061.5	20.1	1061. 5	20.1
2 5	4401	0.40	1.7341 3	4.1	0.16696	1.0	0.25	995 .3	9.6	1021.3	26.7	1077.3	80.7	1077. 3	80.7
1 6 8	24381	0.35	1.9044 1	1.9	0.18195	1.6	0.85	107 7.6	16.3	1082.6	12.8	1092.7	20.1	1092. 7	20.1
1 4 0	10559	0.32	2.0110 3	5.3	0.18683	4.6	0.86	110 4.2	46.8	1119.2	36.2	1148.6	53.1	1148. 6	53.1
5 2	1940	0.99	1.7209 5	4.2	0.15953	2.6	0.60	954 .2	22.7	1016.4	27.3	1152.9	67.4	1152. 9	67.4
1 0 2	6024	0.50	1.8113 5	5.6	0.16780	1.0	0.19	100 0.0	9.7	1049.6	36.6	1154.2	109. 1	1154. 2	109.1
1 5 0	25456	0.54	2.1263 9	1.4	0.19616	1.0	0.71	115 4.7	10.6	1157.4	9.8	1162.5	19.9	1162. 5	19.9
7 7	15027	0.43	2.1226 4	1.6	0.19434	1.0	0.62	114 4.9	10.5	1156.2	11.2	1177.5	25.2	1177. 5	25.2
1 9 3	32705	0.39	2.2175 8	1.4	0.20038	1.0	0.71	117 7.4	10.8	1186.6	9.9	1203.5	19.7	1203. 5	19.7
3 7 3	60573	0.42	2.3645 4	1.6	0.21302	1.2	0.77	124 4.9	13.7	1232.0	11.2	1209.4	19.7	1209. 4	19.7
6 5	13284	1.32	2.3081 2	1.6	0.20700	1.0	0.61	121 2.8	11.1	1214.8	11.6	1218.2	25.6	1218. 2	25.6

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U ( P P m )	$^{206}\text{Pb}$ $\text{/}^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $\text{/}^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
3 4 5	67415	0.38	2.4327 4	1.4	0.21729	1.0	0.72	126 7.6	11.8	1252.3	10.3	1226.2	19.6	1226. 2	19.6
3 5 2	74874	0.43	2.2943 9	1.4	0.20452	1.0	0.71	119 9.6	10.9	1210.6	10.0	1230.2	19.6	1230. 2	19.6
1 7 0	29956	0.36	2.4258 2	2.2	0.21572	1.9	0.89	125 9.2	22.2	1250.3	15.7	1234.9	19.6	1234. 9	19.6
1 3 3	25810	0.81	2.3659 8	2.2	0.20966	2.0	0.89	122 7.0	21.9	1232.4	15.7	1241.8	19.7	1241. 8	19.7
8 5	2348	0.43	2.0098 8	5.6	0.17708	1.7	0.30	105 1.0	16.1	1118.9	38.1	1253.1	105. 0	1253. 1	105.0
1 2 4	27086	0.62	2.6871 2	2.5	0.22922	2.3	0.91	133 0.4	27.3	1324.9	18.4	1316.0	19.4	1316. 0	19.4
2 7 9	45671	1.07	2.9560 3	1.7	0.24043	1.4	0.81	138 9.0	17.3	1396.4	13.0	1407.8	19.2	1407. 8	19.2
1 3 8	26810	0.58	3.1212 5	2.3	0.24942	2.0	0.90	143 5.5	26.2	1437.9	17.4	1441.6	19.1	1441. 6	19.1
1 3 1	35055	0.57	3.2035 3	2.0	0.25347	1.7	0.86	145 6.4	22.1	1458.0	15.2	1460.4	19.0	1460. 4	19.0
4 4	9471	1.59	3.2068 4	1.7	0.25189	1.0	0.58	144 8.2	13.0	1458.8	13.4	1474.2	26.9	1474. 2	26.9
1 7 3	44575	0.23	3.1597 4	1.8	0.24777	1.6	0.84	142 7.0	19.9	1447.4	14.3	1477.5	19.0	1477. 5	19.0
7 6	15993	0.73	3.3113 0	1.7	0.25897	1.0	0.58	148 4.5	13.3	1483.7	13.4	1482.5	26.4	1482. 5	26.4
8 7	20630	0.89	3.3986 5	1.4	0.26376	1.0	0.71	150 9.1	13.5	1504.1	11.1	1497.1	18.9	1497. 1	18.9
3 1 0	55523	0.49	3.3464 2	1.4	0.25946	1.0	0.71	148 7.1	13.3	1492.0	11.1	1498.9	18.9	1498. 9	18.9
6 9	18432	0.26	3.4995 5	1.8	0.27105	1.5	0.83	154 6.1	20.7	1527.1	14.3	1500.8	18.9	1500. 8	18.9
2 4	5486	0.53	3.3749 7	3.1	0.25952	1.1	0.36	148 7.4	14.8	1498.6	24.2	1514.5	54.2	1514. 5	54.2
8 7	20786	0.15	3.3915 9	2.6	0.25600	2.4	0.93	146 9.3	32.1	1502.5	20.7	1549.5	18.8	1549. 5	18.8
2 4 5	58016	0.35	3.8233 6	2.1	0.28460	1.8	0.87	161 4.5	25.6	1597.7	16.5	1575.6	18.7	1575. 6	18.7

## DR2009238

U ( P P m )	$^{206}\text{Pb}$ $\text{/}^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $\text{/}^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
2 4 5	29131	1.26	4.0935 9	2.0	0.29243	1.7	0.86	165 3.7	24.8	1653.0	16.1	1652.2	18.6	1652. 2	18.6
1 4 8	38860	0.55	5.1679 5	3.2	0.33267	3.0	0.95	185 1.3	48.4	1847.4	27.0	1842.9	18.1	1842. 9	18.1
1 4 5	37693	0.88	5.4454 4	1.8	0.34448	1.4	0.82	190 8.2	23.8	1892.0	15.0	1874.3	18.0	1874. 3	18.0
6 0 2	21166	0.54	0.4856 0	1.4	0.06313	1.0	0.70	394 .6	3.8	401.9	4.7	443.9	22.7	394.6	3.8
4 6 9	6960	1.03	0.5296 6	7.1	0.06411	5.1	0.71	400 .6	19.7	431.6	25.0	600.7	108. 1	400.6	19.7
3 5 7	13618	0.58	0.5146 8	4.6	0.06415	4.0	0.87	400 .8	15.4	421.6	15.8	536.9	50.3	400.8	15.4
3 6 4	3839	0.68	0.5581 3	6.6	0.06428	3.6	0.55	401 .6	14.1	450.3	24.0	707.2	117. 2	401.6	14.1
2 0 0	8282	0.42	0.5002 5	4.0	0.06451	2.6	0.66	403 .0	10.3	411.9	13.6	461.8	66.9	403.0	10.3
4 9 4	22258	0.52	0.5142 7	2.6	0.06529	1.5	0.57	407 .7	5.8	421.3	8.8	496.4	46.2	407.7	5.8
2 9 9	11708	0.35	0.4913 6	3.6	0.06533	2.8	0.79	408 .0	11.2	405.8	12.1	393.7	49.7	408.0	11.2
3 0 0	13053	0.53	0.5022 8	2.1	0.06548	1.3	0.59	408 .9	5.0	413.2	7.2	437.8	38.4	408.9	5.0
2 2 4	10103	0.78	0.5145 8	4.7	0.06548	2.7	0.57	408 .9	10.6	421.5	16.3	491.2	85.8	408.9	10.6
3 4 6	7422	0.80	0.5250 3	3.3	0.06570	1.7	0.53	410 .2	6.9	428.5	11.4	528.2	60.5	410.2	6.9
2 1 0	10014	0.56	0.4988 0	2.9	0.06576	1.7	0.59	410 .5	6.7	410.9	9.7	412.8	51.9	410.5	6.7
4 4 4	9290	0.88	0.5222 8	2.4	0.06577	1.8	0.76	410 .6	7.3	426.7	8.4	514.2	34.5	410.6	7.3
2 8 8	7834	0.52	0.5107 8	5.3	0.06583	3.5	0.66	411 .0	13.9	419.0	18.3	463.2	89.1	411.0	13.9

## DR2009238

U ( P P m )	$^{206}\text{Pb}$ $\text{/}^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}$ $\text{*}/^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $\text{/}^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
3 9 5	15889	0.78	0.5079 5	1.4	0.06597	1.0	0.70	411 .8	4.0	417.1	4.9	446.2	22.9	<b>411.8</b>	4.0
2 4 4	6094	0.53	0.5446 3	7.3	0.06608	3.6	0.50	412 .5	14.6	441.5	26.1	595.5	136. 9	<b>412.5</b>	14.6
1 8 9	4608	0.77	0.5491 4	9.6	0.06610	4.3	0.45	412 .6	17.3	444.4	34.5	612.7	184. 7	<b>412.6</b>	17.3
3 1 7	7066	1.07	0.5219 0	3.8	0.06610	1.8	0.48	412 .6	7.2	426.4	13.1	501.6	73.0	<b>412.6</b>	7.2
1 9 4	8913	0.38	0.5002 5	3.3	0.06616	1.7	0.50	413 .0	6.6	411.9	11.2	405.8	64.3	<b>413.0</b>	6.6
1 4 0	6978	0.91	0.5106 9	3.2	0.06633	1.1	0.34	414 .0	4.3	418.9	10.8	446.1	65.9	<b>414.0</b>	4.3
3 1 2	9340	1.69	0.5135 0	1.6	0.06647	1.2	0.77	414 .8	4.9	420.8	5.4	453.6	22.5	<b>414.8</b>	4.9
3 0 1	11098	0.41	0.5252 5	7.1	0.06652	6.6	0.93	415 .2	26.6	428.7	25.0	501.8	59.6	<b>415.2</b>	26.6
6 4 6	29320	0.11	0.5110 2	3.2	0.06662	3.0	0.95	415 .8	12.1	419.1	10.9	437.7	22.4	<b>415.8</b>	12.1
5 4 4	15676	1.81	0.5219 8	1.5	0.06716	1.0	0.65	419 .0	4.1	426.5	5.3	467.1	25.6	<b>419.0</b>	4.1
3 4 8	18494	0.55	0.5104 3	1.4	0.06722	1.0	0.70	419 .4	4.1	418.7	4.9	415.3	22.5	<b>419.4</b>	4.1
5 0 6	2335	2.22	0.6059 7	4.3	0.06797	1.0	0.23	423 .9	4.1	481.0	16.3	763.2	87.3	<b>423.9</b>	4.1
1 6 3	7991	0.40	0.5155 9	2.7	0.06822	1.9	0.70	425 .4	7.9	422.2	9.4	404.6	43.5	<b>425.4</b>	7.9
7 2	3660	0.49	0.5287 5	5.3	0.06823	1.7	0.31	425 .5	6.8	431.0	18.5	460.5	111. 0	<b>425.5</b>	6.8
3 3 3	5728	0.26	0.5648 8	8.3	0.06843	2.7	0.33	426 .7	11.3	454.7	30.6	598.9	171. 0	<b>426.7</b>	11.3
5 1 6	24111	0.86	0.5206 3	1.8	0.06877	1.5	0.84	428 .7	6.4	425.6	6.4	408.5	22.4	<b>428.7</b>	6.4
3 4 5	12735	0.09	0.5289 4	7.6	0.06913	7.4	0.97	430 .9	30.7	431.1	26.7	432.0	41.5	<b>430.9</b>	30.7

## DR2009238

U ( P P m )	$\frac{^{206}\text{Pb}}{^{204}\text{Pb}}$	U/Th	$\frac{^{207}\text{Pb}^*}{^{235}\text{U}}$	$\pm$ (%)	$\frac{^{206}\text{Pb}^*}{^{238}\text{U}}$	$\pm$ (%)	Error Corr.	$\frac{^{206}\text{Pb}^*}{^{238}\text{U}}$	$\pm$ (Ma)	$\frac{^{207}\text{Pb}^*}{^{235}\text{U}}$	$\pm$ (Ma)	$\frac{^{206}\text{Pb}^*}{^{207}\text{Pb}^*}$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
4 7 0	11792	0.31	0.5403 7	2.2	0.06933	2.0	0.89	432 .1	8.2	438.7	7.8	473.0	22.3	<b>432.1</b>	8.2
1 6 8	1987	0.89	0.6975 9	15.2	0.06961	6.2	0.41	433 .8	26.0	537.3	63.7	1005.1	284. 1	<b>433.8</b>	26.0
3 7 8	18315	0.78	0.5346 6	1.8	0.06966	1.4	0.75	434 .1	5.8	434.9	6.4	439.2	26.6	<b>434.1</b>	5.8
3 0 2	17543	0.79	0.5365 8	3.2	0.07027	2.8	0.89	437 .8	12.0	436.2	11.4	427.7	33.2	<b>437.8</b>	12.0
3 0 4	2567	1.03	0.6675 7	12.9	0.07028	1.8	0.14	437 .8	7.4	519.2	52.6	895.6	265. 3	<b>437.8</b>	7.4
5 4 4	24360	0.50	0.5355 4	4.1	0.07044	3.9	0.97	438 .8	16.7	435.5	14.4	418.0	22.6	<b>438.8</b>	16.7
5 4 5	24639	0.20	0.5616 0	3.2	0.07048	2.6	0.82	439 .0	11.0	452.6	11.5	521.8	39.6	<b>439.0</b>	11.0
2 4 0	3979	0.88	0.6092 8	10.9	0.07061	3.4	0.31	439 .8	14.3	483.1	42.0	694.0	222. 2	<b>439.8</b>	14.3
2 4 9	6638	0.97	0.5719 5	3.9	0.07140	3.6	0.91	444 .6	15.4	459.3	14.5	533.4	34.9	<b>444.6</b>	15.4
8 1 9	45932	0.38	0.5582 1	2.4	0.07160	2.2	0.91	445 .8	9.3	450.4	8.6	473.6	22.2	<b>445.8</b>	9.3
3 5 1	17441	0.37	0.5616 3	6.5	0.07180	6.3	0.97	447 .0	27.3	452.6	23.7	480.9	33.1	<b>447.0</b>	27.3
3 1 3	15358	0.23	0.5572 0	2.3	0.07276	2.0	0.88	452 .8	8.9	449.7	8.5	433.9	25.0	<b>452.8</b>	8.9
1 2 9	7405	0.67	0.5549 5	3.5	0.07397	2.5	0.72	460 .0	11.2	448.2	12.7	388.1	54.5	<b>460.0</b>	11.2
1 6 1	3373	0.45	0.6778 0	6.7	0.07435	2.8	0.41	462 .3	12.3	525.4	27.6	810.0	128. 4	<b>462.3</b>	12.3
4 6 7	6259	0.27	0.6935 2	5.9	0.07543	2.5	0.42	468 .8	11.4	534.9	24.7	827.9	112. 5	<b>468.8</b>	11.4
2 2 0	8402	0.96	0.6242 1	3.9	0.07582	1.9	0.48	471 .1	8.6	492.5	15.4	593.2	75.0	<b>471.1</b>	8.6
3 5	15672	1.06	0.6014 4	1.8	0.07649	1.3	0.70	475 .1	5.8	478.1	6.9	492.5	28.4	<b>475.1</b>	5.8

## DR2009238

U ( P P m )	$^{206}\text{Pb}$ $/^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}$ $/^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $/^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
5															
2 1 7	6604	0.69	0.6541 1	2.1	0.08071	1.6	0.76	500 .4	7.8	511.0	8.5	558.8	29.6	<b>500.4</b>	7.8
1 2 8 8	52064	0.11	0.7343 5	3.8	0.08901	3.6	0.96	549 .7	19.1	559.1	16.1	597.7	21.7	<b>549.7</b>	19.1
1 3 1	14000	0.99	2.0213 7	1.8	0.18730	1.5	0.83	110 6.7	15.2	1122.7	12.3	1153.8	20.0	<b>1153. 8</b>	20.0
1 3 7	5171	0.56	0.8128 6	10.6	0.09152	5.4	0.51	564 .5	29.3	604.1	48.2	755.4	191. 8	<b>564.5</b>	29.3
5 5 1	51345	0.38	0.7524 9	1.4	0.09280	1.0	0.71	572 .1	5.5	569.7	6.2	560.1	21.8	<b>572.1</b>	5.5
3 8 6	23841	1.26	0.8380 0	2.0	0.09973	1.8	0.87	612 .8	10.4	618.0	9.5	637.2	21.6	<b>612.8</b>	10.4
5 9	6862	1.21	1.1238 2	2.8	0.12753	1.5	0.51	773 .8	10.6	764.8	15.2	738.7	51.3	<b>773.8</b>	10.6
2 2 3	31755	1.08	1.4707 2	1.4	0.15283	1.0	0.71	916 .8	8.5	918.4	8.6	922.3	20.6	<b>922.3</b>	20.6
2 4 7	33282	2.83	1.5041 4	1.4	0.15618	1.0	0.71	935 .5	8.7	932.1	8.6	923.8	20.6	<b>923.8</b>	20.6
1 2 5	16317	0.76	1.4196 8	1.7	0.14641	1.1	0.65	880 .8	9.2	897.2	10.3	937.9	26.8	<b>937.9</b>	26.8
1 3 8	14522	0.49	1.5483 6	2.0	0.15951	1.6	0.80	954 .1	14.0	949.8	12.1	940.1	24.0	<b>940.1</b>	24.0
7 4	10366	0.49	1.5283 2	2.6	0.15548	1.6	0.64	931 .6	14.3	941.8	15.8	965.8	40.3	<b>965.8</b>	40.3
1 3 4	19387	0.38	1.5520 8	1.6	0.15768	1.2	0.78	943 .9	10.8	951.3	9.8	968.6	20.5	<b>968.6</b>	20.5
1 3 8	17775	2.31	1.5497 6	1.7	0.15717	1.3	0.72	941 .0	11.0	950.4	10.8	972.1	24.7	<b>972.1</b>	24.7
6 7	10822	0.56	1.6697 8	1.8	0.16919	1.0	0.55	100 7.7	9.3	997.1	11.6	973.9	31.3	<b>973.9</b>	31.3
1 7 5	21024	0.47	1.5801 2	2.0	0.15993	1.8	0.87	956 .4	15.6	962.4	12.6	976.2	20.5	<b>976.2</b>	20.5

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U ( P P m )	$\frac{^{206}\text{Pb}}{^{204}\text{Pb}}$	U/Th	$\frac{^{207}\text{Pb}^*}{^{235}\text{U}}$	$\pm$ (%)	$\frac{^{206}\text{Pb}^*}{^{238}\text{U}}$	$\pm$ (%)	Error Corr.	$\frac{^{206}\text{Pb}^*}{^{238}\text{U}}$	$\pm$ (Ma)	$\frac{^{207}\text{Pb}^*}{^{235}\text{U}}$	$\pm$ (Ma)	$\frac{^{206}\text{Pb}^*}{^{207}\text{Pb}^*}$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
1 2 8	19354	1.05	1.6146 8	2.0	0.16224	1.7	0.87	969 .2	15.7	975.9	12.6	991.0	20.4	<b>991.0</b>	20.4
1 5 7	19400	0.61	1.6690 1	1.4	0.16736	1.0	0.71	997 .6	9.2	996.8	9.0	995.2	20.4	<b>995.2</b>	20.4
7 1	10734	0.52	1.6291 5	2.7	0.16287	1.5	0.55	972 .7	13.3	981.5	16.8	1001.4	45.2	<b>1001. 4</b>	45.2
3 3	3701	1.47	1.5257 6	4.1	0.15252	1.7	0.41	915 .1	14.2	940.8	24.9	1001.5	75.1	<b>1001. 5</b>	75.1
1 1 5	19448	0.75	1.6509 0	1.9	0.16470	1.0	0.53	982 .8	9.1	989.9	11.8	1005.5	32.1	<b>1005. 5</b>	32.1
2 8 6	44477	0.56	1.6630 0	1.5	0.16582	1.0	0.72	989 .1	9.6	994.5	9.2	1006.6	20.3	<b>1006. 6</b>	20.3
4 1	6392	0.91	1.7147 0	3.0	0.17087	1.0	0.34	101 6.9	9.4	1014.0	19.1	1007.9	56.8	<b>1007. 9</b>	56.8
1 2 0	16698	0.44	1.6862 0	1.6	0.16777	1.0	0.64	999 .8	9.3	1003.3	9.9	1011.0	24.0	<b>1011. 0</b>	24.0
4 5	7506	0.64	1.6844 0	2.1	0.16758	1.0	0.50	998 .7	9.4	1002.6	13.1	1011.2	36.2	<b>1011. 2</b>	36.2
3 8 1	47326	1.23	1.7173 5	1.8	0.17064	1.4	0.82	101 5.6	13.5	1015.0	11.2	1013.7	20.3	<b>1013. 7</b>	20.3
9 7	14745	0.54	1.7437 2	2.1	0.17313	1.4	0.66	102 9.3	12.9	1024.8	13.3	1015.2	31.4	<b>1015. 2</b>	31.4
1 1 9	18502	0.32	1.6958 4	1.5	0.16833	1.0	0.67	100 2.9	9.3	1007.0	9.5	1015.8	22.4	<b>1015. 8</b>	22.4
1 9 7	23672	0.68	1.6335 1	2.2	0.16213	2.0	0.89	968 .6	18.0	983.2	14.1	1016.0	20.5	<b>1016. 0</b>	20.5
1 4 1	21795	0.59	1.7323 8	1.6	0.17193	1.0	0.61	102 2.7	9.5	1020.6	10.5	1016.2	26.2	<b>1016. 2</b>	26.2
1 0 3	17771	0.67	1.7913 4	1.4	0.17776	1.0	0.71	105 4.7	9.7	1042.3	9.2	1016.3	20.4	<b>1016. 3</b>	20.4
1 0 7	15200	0.64	1.7192 3	1.9	0.17053	1.7	0.85	101 5.0	15.6	1015.7	12.5	1017.3	20.5	<b>1017. 3</b>	20.5
8 4	14112	0.57	1.6934 9	1.7	0.16797	1.0	0.58	100 0.9	9.3	1006.1	10.9	1017.4	28.1	<b>1017. 4</b>	28.1
1 6 1	22261	0.44	1.7326 6	2.4	0.17183	2.1	0.90	102 2.2	20.2	1020.7	15.2	1017.6	20.3	<b>1017. 6</b>	20.3

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U ( P P m )	$^{206}\text{Pb}$ $\text{/}^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $\text{/}^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
2 1 3	28810	0.69	1.7713 8	1.9	0.17542	1.6	0.84	104 1.9	15.0	1035.0	12.1	1020.5	20.3	1020. 5	20.3
9 7	13340	0.52	1.7860 0	2.3	0.17678	1.0	0.44	104 9.4	9.7	1040.4	14.9	1021.5	41.8	1021. 5	41.8
1 5 0	21222	0.63	1.6829 8	1.4	0.16653	1.0	0.71	993 .0	9.2	1002.1	9.0	1022.1	20.3	1022. 1	20.3
1 4 9	20948	0.53	1.7243 2	1.4	0.16992	1.0	0.71	101 1.7	9.4	1017.6	9.1	1030.5	20.2	1030. 5	20.2
8 2	11894	0.56	1.6955 5	1.8	0.16708	1.0	0.55	996 .0	9.2	1006.9	11.7	1030.5	31.1	1030. 5	31.1
1 1 7	14508	0.62	1.7402 8	1.8	0.17146	1.1	0.60	102 0.2	10.5	1023.6	11.9	1030.8	29.9	1030. 8	29.9
1 7 2	17948	0.54	1.7954 3	1.4	0.17681	1.0	0.71	104 9.5	9.7	1043.8	9.2	1031.8	20.3	1031. 8	20.3
4 0	5361	0.56	1.7336 0	2.8	0.17071	1.3	0.45	101 6.0	12.0	1021.1	18.2	1032.0	51.0	1032. 0	51.0
4 8	6640	0.91	1.6804 6	3.6	0.16521	2.0	0.54	985 .7	17.9	1001.2	22.9	1035.2	61.1	1035. 2	61.1
1 1 4	18279	0.46	1.7471 5	1.7	0.17078	1.2	0.71	101 6.4	11.2	1026.1	10.9	1046.9	24.2	1046. 9	24.2
9 7	9254	0.70	1.7048 6	2.7	0.16533	1.5	0.56	986 .3	13.8	1010.4	17.3	1062.8	45.2	1062. 8	45.2
2 9	5075	0.55	1.8391 3	2.4	0.17804	1.6	0.67	105 6.3	15.4	1059.5	15.6	1066.3	35.3	1066. 3	35.3
1 2 4	22367	0.39	1.8504 7	1.8	0.17897	1.5	0.83	106 1.3	14.8	1063.6	12.0	1068.2	20.2	1068. 2	20.2
7 8	9949	0.86	1.9932 7	2.8	0.19101	2.4	0.84	112 6.8	24.8	1113.2	19.2	1086.7	30.7	1086. 7	30.7
1 4 3	22541	0.58	1.9002 5	2.4	0.18046	2.1	0.91	106 9.5	21.2	1081.2	15.8	1104.8	20.1	1104. 8	20.1
1 1 1	7728	0.55	1.7195 3	3.2	0.16292	1.0	0.31	973 .0	9.0	1015.8	20.8	1109.5	61.7	1109. 5	61.7
3 9	2707	0.68	1.5867 0	4.4	0.14976	1.3	0.29	899 .6	10.9	965.0	27.7	1117.0	84.9	1117. 0	84.9
3 4 4	43610	0.26	1.9065 6	4.6	0.17962	4.5	0.98	106 4.9	44.5	1083.4	31.0	1120.7	20.0	1120. 7	20.0

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U ( P P m )	$^{206}\text{Pb}$ $\text{/}^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $\text{/}^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
2 8 3	39818	0.78	1.9758 7	1.9	0.18583	1.6	0.85	109 8.8	16.6	1107.3	13.0	1124.1	19.9	1124. 1	19.9
3 3	5649	2.42	2.1393 3	4.5	0.20064	1.9	0.41	117 8.8	20.2	1161.6	31.2	1129.8	81.8	1129. 8	81.8
4 7 3	75056	0.43	2.0155 3	1.4	0.18790	1.0	0.71	111 0.0	10.2	1120.8	9.6	1141.7	19.9	1141. 7	19.9
3 5 1	55514	0.56	2.0007 4	1.4	0.18652	1.0	0.71	110 2.5	10.1	1115.8	9.6	1141.7	19.9	1141. 7	19.9
7 2	10416	0.86	2.0124 4	4.0	0.18641	3.7	0.93	110 1.9	37.7	1119.7	27.0	1154.4	28.4	1154. 4	28.4
1 0 1	18146	0.54	2.2119 9	1.5	0.20395	1.0	0.69	119 6.5	10.9	1184.8	10.2	1163.6	20.9	1163. 6	20.9
5 1 0	63365	0.25	2.2014 5	1.4	0.20265	1.0	0.71	118 9.5	10.9	1181.5	9.9	1166.8	19.8	1166. 8	19.8
5 4	9368	0.81	2.1557 6	1.4	0.19737	1.0	0.70	116 1.2	10.6	1166.9	9.9	1177.5	20.3	1177. 5	20.3
2 1 2	25338	0.86	2.1637 9	6.1	0.19802	5.9	0.98	116 4.7	63.3	1169.5	42.3	1178.4	25.8	1178. 4	25.8
8 2	12200	0.59	2.2101 1	2.6	0.20128	2.4	0.91	118 2.2	25.6	1184.2	18.3	1188.0	22.0	1188. 0	22.0
9 2	15858	0.60	2.2221 4	1.7	0.20236	1.0	0.61	118 8.0	11.3	1188.0	12.0	1188.1	26.9	1188. 1	26.9
2 8 2	45866	0.81	2.2479 4	1.4	0.20471	1.0	0.71	120 0.5	11.0	1196.1	9.9	1188.2	19.8	1188. 2	19.8
3 7 9	56661	0.18	2.3437 8	2.5	0.21314	2.3	0.91	124 5.5	25.5	1225.7	17.6	1190.9	19.7	1190. 9	19.7
1 5 0	27127	0.75	2.2557 3	1.7	0.20433	1.3	0.79	119 8.5	14.3	1198.6	11.6	1198.6	19.8	1198. 6	19.8
1 7 4	24551	0.69	2.2610 0	3.1	0.20386	3.0	0.95	119 6.0	32.3	1200.2	22.0	1207.8	19.7	1207. 8	19.7
7 5	12962	1.26	2.2869 3	1.9	0.20611	1.0	0.51	120 8.0	11.0	1208.3	13.8	1208.6	33.0	1208. 6	33.0
9 3	17233	0.53	2.2231 2	1.6	0.20013	1.0	0.64	117 6.0	10.7	1188.4	11.0	1210.9	23.9	1210. 9	23.9
1 0 7	21196	0.63	2.2589 3	1.4	0.20330	1.0	0.71	119 3.0	10.9	1199.6	10.0	1211.4	19.7	1211. 4	19.7

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U ( P P m )	$^{206}\text{Pb}$ $/^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}$ $/^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $/^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
7 4	11474	1.19	2.1942 7	2.3	0.19711	1.8	0.79	115 9.8	19.3	1179.2	16.0	1215.1	27.6	1215. 1	27.6
3 1 6	46773	0.61	2.2418 0	1.4	0.20073	1.0	0.72	117 9.2	11.1	1194.2	10.1	1221.4	19.7	1221. 4	19.7
1 0 6	21558	0.59	2.3532 7	1.5	0.21034	1.1	0.75	123 0.6	12.8	1228.5	10.8	1224.9	19.7	1224. 9	19.7
1 0 2	16985	0.72	2.2935 5	1.4	0.20481	1.0	0.72	120 1.1	11.3	1210.3	10.2	1226.7	19.7	1226. 7	19.7
1 8 5	16318	4.01	2.3067 0	1.8	0.20580	1.5	0.83	120 6.4	16.3	1214.3	12.7	1228.5	19.8	1228. 5	19.8
1 2 4	26619	0.46	2.4382 4	1.5	0.21728	1.0	0.68	126 7.5	11.5	1254.0	10.6	1230.8	21.1	1230. 8	21.1
6 4 8	107071	0.39	2.3951 7	1.4	0.21281	1.0	0.71	124 3.8	11.3	1241.2	10.1	1236.6	19.6	1236. 6	19.6
1 2 2	19515	1.19	2.4028 2	1.4	0.21263	1.0	0.71	124 2.8	11.3	1243.4	10.2	1244.5	19.6	1244. 5	19.6
4 7	9366	0.78	2.3398 9	2.4	0.20599	1.0	0.42	120 7.4	11.0	1224.5	17.1	1254.6	42.6	1254. 6	42.6
5 6	11218	0.93	2.5630 0	1.6	0.22173	1.3	0.79	129 1.0	15.0	1290.1	11.9	1288.7	19.7	1288. 7	19.7
2 6 2	36048	0.84	2.5854 5	1.4	0.22149	1.0	0.72	128 9.7	12.1	1296.5	10.6	1307.8	19.5	1307. 8	19.5
2 3 2	36087	1.35	2.6393 5	1.6	0.22424	1.2	0.77	130 4.2	14.1	1311.7	11.5	1323.8	19.4	1323. 8	19.4
1 3 7	33160	1.04	2.9509 4	1.4	0.23896	1.0	0.72	138 1.3	13.0	1395.1	11.0	1416.3	19.1	1416. 3	19.1
8 0	15222	1.27	3.2571 2	2.3	0.25643	2.0	0.86	147 1.5	26.6	1470.9	18.2	1469.9	22.6	1469. 9	22.6
1 1 2	20230	0.97	3.3017 0	1.7	0.25419	1.4	0.81	146 0.1	18.2	1481.5	13.4	1512.2	18.9	1512. 2	18.9
3 0 4	57973	0.46	3.4667 7	1.6	0.26517	1.2	0.77	151 6.2	16.4	1519.7	12.4	1524.5	18.9	1524. 5	18.9
2 6 2	49636	0.52	3.5119 8	1.4	0.26824	1.0	0.71	153 1.9	13.6	1529.9	11.2	1527.2	18.8	1527. 2	18.8
4	80926	0.72	3.4551	1.7	0.26378	1.4	0.82	150	19.0	1517.0	13.6	1528.1	18.8	1528. 1	18.8

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U ( p p m )	$^{206}\text{Pb}$ / $^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ / $^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ / $^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*$ / $^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ / $^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ / $^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)	
0 2			6					9.1							1	
3 8 1	77865	0.64	3.5880 0	1.8	0.27319	1.4	0.82	155 6.9	20.0	1546.9	14.0	1533.1	18.8	1533. 1	18.8	
3 3 0	61494	0.69	3.3928 7	1.7	0.25759	1.4	0.81	147 7.5	18.1	1502.8	13.3	1538.5	18.8	1538. 5	18.8	
3 1 0	68822	0.56	3.5126 6	1.5	0.26589	1.1	0.75	151 9.9	15.2	1530.1	11.9	1544.1	18.8	1544. 1	18.8	
2 5 7	52542	0.72	3.6992 9	1.9	0.27962	1.7	0.86	158 9.4	23.3	1571.2	15.5	1546.8	18.8	1546. 8	18.8	
7 0	14475	1.06	3.6059 6	1.5	0.26914	1.1	0.72	153 6.4	14.5	1550.8	11.7	1570.5	19.3	1570. 5	19.3	
2 9 8	40313	0.87	3.5308 9	3.5	0.26335	1.4	0.40	150 7.0	18.7	1534.2	27.3	1571.9	59.2	1571. 9	59.2	
9 0	20815	1.16	3.7488 8	1.4	0.27865	1.0	0.71	158 4.6	14.0	1581.9	11.4	1578.2	18.8	1578. 2	18.8	
7 7	15933	1.53	3.7278 9	1.9	0.27403	1.6	0.82	156 1.2	21.5	1577.4	15.2	1599.0	20.4	1599. 0	20.4	
2 7 5	62102	0.58	4.3349 0	1.4	0.29880	1.0	0.71	168 5.3	14.8	1700.0	11.7	1718.2	18.4	1718. 2	18.4	
6 4	20710	0.69	4.5480 5	1.4	0.30777	1.0	0.71	172 9.7	15.2	1739.8	11.8	1751.9	18.4	1751. 9	18.4	
1 8 3	16118	1.33	4.9132 4	2.6	0.31523	2.4	0.92	176 6.4	37.5	1804.5	22.2	1848.8	18.1	1848. 8	18.1	
5 5	17924	1.23	5.6056 1	1.4	0.35176	1.0	0.71	194 3.0	16.8	1917.0	12.2	1888.9	18.0	1888. 9	18.0	
1 0 0	30657	1.49	5.1953 5	1.9	0.32506	1.6	0.84	181 4.4	24.9	1851.9	15.9	1894.2	18.0	1894. 2	18.0	
1 1 3	5948	0.61	1.2215 6	3.8	0.12071	3.2	0.85	734 -6	22.4	810.5	21.3	1024.9	41.3	734.6	22.4	
8 0	3746	0.85	1.2385 6	5.0	0.12299	4.3	0.87	747 -7	30.3	818.2	27.9	1015.0	50.4	747.7	30.3	
2 6 6	30374	0.65	1.4938 6	1.5	0.15505	1.0	0.68	929 -2	8.7	927.9	9.0	924.8	22.2	924.8	22.2	
2 3	24182	0.60	1.4295 6	3.2	0.14628	3.0	0.93	880 -1	24.6	901.4	19.1	953.9	23.6	953.9	23.6	

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U ( P P m )	$^{206}\text{Pb}$ $\text{/}^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $\text{/}^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}$ $\text{/}^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $\text{/}^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $\text{/}^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
3															
127	12600	0.79	1.50277	2.1	0.15294	1.4	0.67	917.4	12.0	931.5	12.7	965.0	31.3	<b>965.0</b>	31.3
157	23389	0.24	1.58011	2.0	0.16036	1.6	0.77	958.8	14.1	962.4	12.7	970.8	26.6	<b>970.8</b>	26.6
77	7617	1.40	1.45521	2.6	0.14761	1.5	0.58	887.6	12.4	912.0	15.4	971.7	42.4	<b>971.7</b>	42.4
131	13169	0.31	1.41316	1.7	0.14307	1.2	0.74	862.0	10.0	894.5	9.9	975.6	22.6	<b>975.6</b>	22.6
60	6603	0.48	1.44515	5.8	0.14591	5.4	0.93	878.0	44.2	907.9	34.7	981.2	42.7	<b>981.2</b>	42.7
470	37979	0.80	1.52572	1.6	0.15382	1.3	0.79	922.4	11.1	940.8	10.0	984.1	20.4	<b>984.1</b>	20.4
152	24150	0.36	1.65534	1.8	0.16665	1.3	0.76	993.6	12.4	991.6	11.2	987.1	23.3	<b>987.1</b>	23.3
297	20092	0.83	1.42253	1.8	0.14294	1.5	0.83	861.3	12.2	898.4	10.8	991.0	20.4	<b>991.0</b>	20.4
351	46780	0.40	1.67446	1.4	0.16802	1.0	0.71	100.1.2	9.3	998.9	9.0	993.7	20.3	<b>993.7</b>	20.3
55	7136	0.61	1.59196	2.7	0.15961	1.4	0.53	954.6	12.5	967.1	16.7	995.5	46.4	<b>995.5</b>	46.4
224	25482	0.34	1.51574	2.6	0.15184	2.3	0.89	911.3	19.6	936.8	15.7	997.2	23.4	<b>997.2</b>	23.4
219	47649	0.53	1.64132	1.4	0.16435	1.0	0.71	980.9	9.1	986.2	8.9	998.0	20.3	<b>998.0</b>	20.3
59	9084	0.99	1.65327	3.0	0.16517	1.0	0.33	985.4	9.1	990.8	19.1	1002.7	57.9	<b>1002.7</b>	57.9
241	23136	0.49	1.56609	1.5	0.15627	1.1	0.72	936.0	9.2	956.9	9.0	1005.1	20.4	<b>1005.1</b>	20.4
197	34221	0.44	1.70005	1.9	0.16957	1.6	0.84	100.9.7	14.6	1008.5	11.9	1006.0	20.3	<b>1006.0</b>	20.3
355	36670	0.96	1.65396	1.4	0.16476	1.0	0.71	983.2	9.3	991.1	9.0	1008.6	20.3	<b>1008.6</b>	20.3
355	35468	0.52	1.60630	2.3	0.16000	2.0	0.90	956.8	18.0	972.7	14.1	1008.7	20.3	<b>1008.7</b>	20.3

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U ( P P m )	$^{206}\text{Pb}$ $/^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $/^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)
6 8 6	55454	0.51	1.6619 7	1.7	0.16547	1.3	0.79	987 .1	12.0	994.1	10.5	1009.7	20.3	1009. 7	20.3
1 7 0	20053	0.54	1.5566 6	1.7	0.15477	1.3	0.72	927 .6	10.9	953.1	10.7	1012.5	24.2	1012. 5	24.2
2 1 9	30381	0.85	1.6345 3	1.4	0.16240	1.0	0.71	970 .1	9.0	983.6	8.9	1013.8	20.3	1013. 8	20.3
1 5 7	22045	0.46	1.6832 2	1.8	0.16711	1.5	0.83	996 .2	14.1	1002.2	11.6	1015.4	20.3	1015. 4	20.3
1 2 0	17965	0.43	1.7297 9	1.4	0.17168	1.0	0.71	102 1.4	9.4	1019.7	9.1	1016.0	20.4	1016. 0	20.4
8 3	11224	0.81	1.7056 9	2.1	0.16927	1.3	0.62	100 8.1	11.9	1010.7	13.3	1016.2	33.2	1016. 2	33.2
1 2 5	20037	0.65	1.6664 2	1.5	0.16523	1.1	0.74	985 .8	10.1	995.8	9.5	1018.0	20.4	1018. 0	20.4
1 3 0 7	42453	0.31	1.5860 1	5.1	0.15714	4.6	0.91	940 .9	40.6	964.7	31.9	1019.5	43.7	1019. 5	43.7
2 5 8	34528	0.31	1.7357 7	3.8	0.17187	3.7	0.96	102 2.4	34.8	1021.9	24.6	1020.8	20.3	1020. 8	20.3
2 0 8	13825	0.40	1.5367 8	1.9	0.15192	1.6	0.85	911 .7	13.9	945.2	11.8	1024.1	20.3	1024. 1	20.3
2 1 2	29164	1.32	1.7184 1	1.6	0.16957	1.2	0.74	100 9.7	10.9	1015.4	10.1	1027.7	21.5	1027. 7	21.5
9 5	16133	0.57	1.7324 2	1.9	0.17090	1.2	0.62	101 7.1	10.9	1020.7	12.0	1028.3	29.5	1028. 3	29.5
3 9	3285	0.71	1.2944 6	6.9	0.12719	2.4	0.35	771 .8	17.7	843.3	39.4	1036.3	130. 0	1036. 3	130.0
1 0 1	14391	0.77	1.8037 0	1.6	0.17696	1.0	0.63	105 0.3	9.7	1046.8	10.4	1039.4	25.0	1039. 4	25.0
5 3	7748	0.44	1.7079 0	2.7	0.16750	1.3	0.46	998 .3	11.6	1011.5	17.3	1040.1	48.2	1040. 1	48.2
8 0	9459	0.36	1.5521 8	5.8	0.15191	5.4	0.93	911 .7	46.2	951.4	35.9	1044.3	41.8	1044. 3	41.8
1 1 5	13118	0.40	1.5016 6	2.7	0.14692	2.2	0.82	883 .7	17.9	931.1	16.2	1045.0	31.0	1045. 0	31.0
1	9472	0.46	1.5631	2.2	0.15289	1.4	0.65	917	12.2	955.7	13.7	1045.6	34.2	1045. 5	34.2

U ( P P m )	$^{206}\text{Pb}$ $/^{204}\text{Pb}$	U/Th	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (%)	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (%)	Error Corr.	$^{206}\text{Pb}^*$ $/^{238}\text{U}$	$\pm$ (Ma)	$^{207}\text{Pb}^*$ $/^{235}\text{U}$	$\pm$ (Ma)	$^{206}\text{Pb}^*$ $/^{207}\text{Pb}^*$	$\pm$ (Ma)	Best Age (Ma)	$\pm$ (Ma)	
4 0			7					.1							6	
9 0	12481	0.55	1.6512 0	2.1	0.16131	1.0	0.48	964 .1	9.0	990.0	13.2	1047.9	37.0	1047. 9	37.0	
6 2	6766	0.56	1.6487 7	1.7	0.16103	1.0	0.58	962 .5	8.9	989.1	11.0	1048.5	28.7	1048. 5	28.7	
2 1 8	15931	0.32	1.6447 4	1.8	0.16055	1.3	0.72	959 .8	11.6	987.5	11.4	1049.6	25.1	1049. 6	25.1	
2 1 2	9860	0.90	1.6937 3	3.5	0.16447	2.5	0.71	981 .6	22.3	1006.2	22.2	1060.1	49.6	1060. 1	49.6	
1 2 5	9619	0.53	1.6823 9	3.5	0.16305	2.2	0.64	973 .7	20.0	1001.9	22.1	1064.0	53.7	1064. 0	53.7	
9 9	8105	0.40	1.6890 1	4.2	0.16260	3.9	0.94	971 .2	35.5	1004.4	26.7	1077.5	28.4	1077. 5	28.4	
8 7	4023	0.61	1.5180 4	2.4	0.14565	1.0	0.41	876 .6	8.2	937.7	14.9	1084.2	44.4	1084. 2	44.4	
4 4	5588	0.73	1.7360 9	2.7	0.16462	1.1	0.41	982 .4	10.0	1022.0	17.3	1107.8	49.0	1107. 8	49.0	
1 8 9	20200	0.44	2.0436 1	1.7	0.18774	1.4	0.80	110 9.1	13.8	1130.2	11.5	1170.8	19.8	1170. 8	19.8	
2 1 3	18206	0.51	2.0599 5	3.8	0.18883	3.7	0.96	111 5.1	37.8	1135.6	26.1	1175.1	19.8	1175. 1	19.8	

## SUPPLEMENTARY REFERENCES

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