

2 **BACKGROUND AND METHODS**

3 **Part I - Growth of orogenic wedges during continental subduction**

4 General setting : Orogenic wedges develop in subduction settings due to plate convergence
5 involving large shortening and deformation of the crust (Fig. A). This paper focus on orogens
6 caused by subduction of a continental margin lower-plate under an oceanic or continental
7 upper-plate following oceanic subduction. After closure of the oceanic domain, subduction of
8 the lithospheric mantle induces deformation of the continental crust and controls the
9 structural asymmetry of the mountain belt (Dewey and Bird, 1970; Mattauer, 1986 ;
10 Malavieille & Chemenda, 1997 ; Beaumont et al., 2000; Avouac, 2003). Since the fundating
11 works by Davis, Dahlen and Suppe in the Eighties (Davis et al., 1983; Dahlen et al., 1984),
12 mountain belts have been often considered by geologists as crustal scale accretionary wedges
13 (e.g., Malavieille, 1984; Platt, 1986) whose deformation mechanisms can be satisfactorily
14 described by a Coulomb behavior. The theory gives a simple mechanical setting allowing to
15 define different tectonic regimes depending on wedge stability : critical, undercritical,
16 overcritical (Dahlen, 1984). Then, it has been shown that orogens commonly adopt a distinct
17 geometry with a low-tapered pro-wedge facing the subducting plate, and a high-tapered
18 retro-wedge on the internal side. This concept of doubly vergent accretionary wedge is widely
19 explored since the nineties (Beaumont et al., 1992; Willett et al., 1993; Ellis and Beaumont,
20 1999; Pfiffner et al., 2000; Naylor et al., 2005; Selzer et al., 2008). Erosion has rapidly been
21 added as a significant parameter (Dahlen & Suppe, 1988; Dahlen, 1988; Dahlen & Barr, 1989)
22 because the impact of material transfer on the mechanics and structural evolution of sub-
23 aerial wedges relative to submarine ones is major (Simpson, 2006). The topography of
24 mountain belts depends of the behavior of continental rock units, itself depending on growth
25 and evolution of faults. Models involving plastic (Chapple, 1978; Willett et al., 1993) or
26 viscous behavior account well for displacements and produce velocity fields close to what is
27 observed in mountain belts, but they do not generate clear displacement discontinuities as
28 faults did. Thus, although the Coulomb wedge model gives a rigorous mechanical frame to
29 study the dynamics of orogenic wedges, it presents some limits as it does not account for
30 deformation processes at the scale of individual tectonic instabilities (Naylor et al., 2005).
31 Analysis is more complex when introducing surface processes whose interactions with
32 tectonics change the mechanical state of the wedge at different time and length scales. The
33 removal of material from the surface, involves a continuous deformation changing the way in
34 which the critical state is maintained. If the tectonic (shortening) and climatic conditions
35 (erosional potential) remain stable, the wedge reaches a dynamic steady state (Jamieson and
36 Beaumont, 1989; Willett, 1999; Willett and Brandon, 2002; Hilley and Strecker, 2004) in
37 which the incoming fluxes (accreted material) are compensated by the outgoing fluxes
38 (material removed by erosion). According to these models, the velocity field of the crust and,
39 hence, the exhumation paths of rock particles, depend on erosion at the surface (e.g., Horton,
40 1999; Persson & Sokoutis, 2002). Consequently, any changes in erosion rates potentially
41 result in a modification of the strain pattern and thus in the evolution of the wedge.

42 Décollements : Various processes of crustal decoupling exist during continental
43 subduction, at great depth, or in the orogenic wedge due either to fluid overpressure (Cobbold
44 et al., 2001) inducing weak crustal zones of strain concentration along brittle or plastic shear
45 zones or weak décollement layers in the sedimentary cover (Banks and Warburton, 1991).
46 During continental subduction, the whole or only part of the incoming rock sequences is
47 accreted to the wedge depending on the location of the décollements that allow material to be
48 detached from the subducting plate. The part which is not involved in wedge growth is

49 dragged deeper into the mantle. At lithospheric scale, oceanic and continental subduction
50 have been described by a simple setting (e.g., Malavieille, 1984) that is used as a first order
51 kinematic boundary condition for many modeling approaches (Fig. A). The location of
52 velocity discontinuities (the “S points” in numerical models, e.g., Beaumont et al., 1994)
53 determines the amount of accreted versus subducted material and controls which part of the
54 continental crust is subducted with the mantle (the whole crust or part of upper-crust). In
55 orogenic wedges, several kinematic singularities can exist mainly due to the mechanical
56 layering of the continental crust, they can be activated (simultaneously or not) during the
57 tectonic evolution. Such a crustal layering can be lithologic (e.g. basement cover interface, or
58 weak layers in a sedimentary sequence), rheologic (e.g., thermo-mechanical changes during
59 subduction or fluids pressure changes) or inherited from a former tectonic history (e.g., the
60 structural heritage of an extended margin prior to continental subduction). During mountain
61 building, these weak zones have a major impact on the mechanical behavior (Brun, 2002) as
62 they constitute potential décollement zones. How and where these décollements develop and
63 how they influence the mechanics and structural evolution of the orogenic wedge are major
64 questions (see Stockmal et al., 2007).

65 Exhumation : Exhumation of metamorphic rocks in mountain belts is a debated problem
66 and many papers have been published to date, some focusing on early exhumation of very
67 high-pressure rocks in subduction channel settings, others on exhumation processes in the
68 frame of the orogenic wedge itself. We focus here on exhumation in wedges submitted to
69 erosion-sedimentation. To analyze the kinematics of material transfer, particle paths have
70 been studied in numerical (e.g., Dahlen & Suppe, 1988) or experimental wedges (e.g.,
71 Konstantinovskaia & Malavieille, 2005). They define an accretionary flux directed from
72 bottom to top in the wedge body explaining the vertical advection of material at the origin of
73 thickening and relief development. Without erosion, these paths do not represent exhumation
74 paths, they only reflect uplift of material or uplift of topography (England & Molnar, 1990).
75 Because exhumation in orogenic wedges requires erosion (or at least normal faulting), the
76 way of exhumation depends on the internal dynamics and conversely, on how this dynamics is
77 modified by erosion (Horton, 1999 ; Burbank, 2002). Models show that local uplift induced by
78 basal accretion can generate localized high angle slopes. Applied to nature, such deformation
79 mechanisms occurring at depth in wedges would favor strong erosion and high denudation
80 rates above domains of underplating. Thus, due to internal strain partitioning, denudation
81 rates will vary along a mountain belt transect because erosion controlled exhumation is very
82 sensitive to the vertical component of displacement. In the same manner, the part of the
83 wedge located above the main décollement behave passively and is generally poorly
84 deformed during accretion. As the portion located between the underplating zone and the
85 domain of active frontal accretion does not undergo strong deformation, its angle of slope
86 remains low, suffering only minor erosion and consequently few exhumation. Due to uplift
87 and erosion, it is affected by wide amplitude folding of its basal contact, resulting in
88 characteristic large scale synformal structures (which remnants often outcrop as klippen of
89 exotic materials resting on top of the orogenic wedge), separated by antiformal culminations
90 of basement rocks (“metamorphic complexes”).

91 Décollement induced deformation partitioning largely controls particle trajectories and
92 strain patterns. One way to investigate orogen dynamics is to look at the ages recorded by
93 different thermochronometers across it (Kühni & Pfiffner, 2001; Willett & Brandon, 2002).
94 Exhumation of rocks means the approaching of a rock particle to the Earth’s surface, which is,
95 e.g. recorded by cooling rates calculated from thermochronologic data, whereas uplift of rocks
96 means the displacement of rocks with respect to the geoid England & Molnar (1990). The
97 study of material paths (trajectories) in mountain belts provides useful insights on their
98 kinematic evolution. Surface processes strongly influence the timing, localization and

amplitude of rock displacements in the varying members of an orogenic wedge. The comparison of their trajectories in experiments performed with and without erosion/sedimentation underscores this influence on material transfer (e.g., Cruz et al., 2008). The variations in rates of erosion and sedimentation modify the extent, the morphology, the structures, the timing of development and the material paths in the different models. Particles located in the converging lower-plate or in the upper-units above the main décollements show complex uplift paths related to deformation partitioning and various tectonic stages. At the scale of a mountain belt each tectonic unit records an individual specific exhumation path. Thus, exhumation rates calculated on the basis of simulated thermochronometry without knowledge of the particles trajectories and internal structure may result in erroneous estimations.

Normal faults : Coulomb wedge theory supports the idea that when the mechanical state changes from critical to overcritical, gravitational forces may cause local extension and subsequent normal faulting (Dahlen et al., 1984). Indeed, if there is no (or only minor) erosion (for example in submarine prisms), normal faults are required in the wedge body for exhumation to occur. Such models have been applied to mountain belts (e.g., Platt, 1986). If we check the effect of erosion and piedmont sedimentation on wedge dynamics in a stability field diagram (Dahlen, 1984), it decreases the slope angle and as a consequence displaces the stability field, favoring an evolution from overcritical to stable or from stable to undercritical state (Leturmy et al., 2000). This trend does not favor extension. Thus, although extension is commonly invoked to explain exhumation of metamorphic rocks and synchronous enigmatic zones of normal shearing observed in most mountain belts, in many cases, this cannot be the dominant mechanism. Since many years, uplift induced normal sense shear zones and concomitant brittle normal faults (developed at lower depth) are described in both ancient (e.g. the Variscan belt, Pérez-Estaún et al., 1991) or active mountain belts (e.g. the Taiwan belt, Crespi et al., 1996). Interpretation of such deformation features in the frame of mountain building is still controversial today and proposed models range between end-members involving compressional (convergent) or extensional (divergent) settings. Experiments with décollements and erosion suggest an alternative way to develop crustal scale normal sense shear zones during continental subduction. Such structures can be the result of the vertical shear induced by strain partitioning within the orogenic wedge (Fig. B). Continuous uplift of underplated crustal units relative to comparatively stable surrounding rocks favors vertical shear and as a consequence a strong stretching and thinning of the formerly stacked tectonic units. At depth these domains are characterized by the development of foliation zones of combined pure and simple shear deformation with a normal sense shearing component. They evolve to brittle normal faults superimposed on former ductile foliation when reaching upper-crustal domains during synconvergence erosion assisted uplift.

Backthrusting : Depending on the behavior of the backstop upper-plate, specific models suggest that underplating induced deformation at the back part of the wedge evolves through continuous shortening. When the upper-plate becomes thinner due to combined effect of uplift and surface erosion, large scale backthrusting may develop in the hinterland, changing material transfer paths in the orogen (Fig. C).

Part II - Modeling principles, techniques and limits

The sandbox devices (Fig. A) are generally composed of a basal plate bounded by two lateral glass walls. A motor pulls a plastic sheet with a surface on which basal friction can be specified. The analogue granular materials deposited on the plastic sheet have frictional properties satisfying the Coulomb theory and they correctly mimic a non-linear deformation

behavior of upper-crustal rocks (Lohrman et al., 2003). They are generally accreted against a backstop (that simulates the undeformed part of the upper-plate lithosphere) developing a thrust wedge during convergence. Upper-plate backstop can be rigid or deformable depending on the material used. In some experiments, we have used materials with a cohesion higher than pure sand. A synthesis on scaling of models, and characterization of analogue materials is given in Graveleau (2008). A maximum convergence of 2.5 m allows large shortening deformation of the models. Influence of erosion, sedimentation and structural heritage on model wedges is studied using an empiric approach (see for example in; Bonnet et al., 2007; 2008). Generally, after the development of a proto thrust wedge (equivalent to the early accretionary wedge developed in submarine conditions), erosion of the model is performed by hand with a thin metal plate (the sand in excess being removed using a vacuum cleaner) to keep the slope at a constant angle. In some cases, a proto sand-wedge is built to allow rapidly a self location of the velocity discontinuity in the model. Erosion of the units is applied independently of their compositional nature, as a function of surface deformation. To obtain a condition of flux and topographic steady-state (e.g., Willett and Brandon, 2002), the domains of high surface slope which develops locally due to internal deformation of the wedge were first eroded each 2cm of model shortening. Then all the material in excess relative to the mean steady state profile is removed. This simple approach could be compared to an erosion affecting more the domains of high surface deformation and subsequent uplift than the areas where surface is less deformed. Such conditions are close to what is expected in wedges submitted to high erosion rates such as Taiwan or New Zealand.

When sedimentation is integrated, it is performed by sprinkling sand. Different situations have been tested with variable amounts of the material eroded from the growing wedge deposited in front of the wedge at the place where the slope breaks and thrusts propagate (this was the case for the experiments devoted to the Alps, where past deformation and erosion rates have been lower than in Taiwan).

Introduction of weak layers of glass beads in the incoming sequence of material allows to simulate décollements and also to take into account the structural heritage of a subducting margin (former normal faults in basement). The internal glass bead layer serves only as a décollement if its internal strength is lower than the strength along the basal detachment interface (Kukovski et al., 2002).

Obviously, our simple 2D approach presents several approximations due to the limits imposed by the experimental procedure. It does not take into account the isostatic response of the lower plate, but as we study the growth of wedges close to a steady state, we assume that these effects do not affect drastically our first order results. The chosen way to perform erosion and sedimentation is also very important in the experiments as it will influence the location and evolution of deformation in the wedge. At the moment, there is no experimental work which perfectly accounts for the complex natural erosion processes. Some 2D numerical modeling better approach what is suspected to be natural erosion laws, but they also fail somewhere as erosion in mountain belts remains a 3D problem. Thus, although today, analogue models are not properly scaled to analyze quantitatively the interactions between tectonics and surface processes, this approach allows to outline several first order behavior of thrust wedges suffering erosion and foreland sedimentation. Plastic deformation at depth plays a major role in the geometry and kinematic evolution of orogenic wedges. Thus, another experimental limit concerns the progressive transition from brittle to plastic behavior that is not properly described by sand. Nevertheless, as the size of our model sand wedges is big, the important diffuse deformation suffered by the granular materials at depth tends to mimic macroscopically a plastic behavior, developing structures which geometry and evolution are close to what is observed in mountain belts. Thus, although the mechanics of our materials is

196 far from well understood, our empirical approach may be able to give significant insights on
197 the growth of accretionary belts.

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199 REFERENCES CITED

200 Avouac J.-P., 2003. Mountain building, erosion, and the seismic cycle in the Nepal Himalaya.
201 *Advances in Geophysics*, 46, 1-80.

202 Banks, C.J., & Warburton, J., 1991. Mid-crustal detachment in the Betic system of southeast
203 Spain, *Tectonophysics*, 191, 275-289.

204 Beaumont, C., Fullsack, P. and Hamilton, J., 1992. Erosional contr l of active compressional
205 orogens. In: *Thrust tectonics*, K.R.McClay, ed., Chapman & Hall, London, 1-18.

206 Beaumont, C., Fullsack, P., Hamilton, J., 1994. Styles of crustal deformation in compressional
207 orogens caused by subduction of the underlying lithosphere, *Tectonophysics* 232, 119–132.

208 Beaumont, C., Munoz, J.A., Hamilton, J., and Fullsack, P., 2000. Factors controlling the Alpine
209 evolution of the central Pyrenees inferred from a comparison of observations and
210 geodynamical models, *J. Geophys. Res.*, 105, 8 121-8 145.

211 Bonnet, C., Malavieille, J. and Mosar, J., 2007. Interactions between tectonics, erosion, and
212 sedimentation during the recent evolution of the Alpine orogen: Analogue modeling insights.
213 *Tectonics*, 26, TC6016, doi:10.1029/2006TC002048.

214 Bonnet, C., Malavieille, J. and Mosar, J., 2008. Surface processes versus kinematics of thrust
215 belts: impact on rates of erosion, sedimentation, and exhumation – Insights from analogue
216 models. *Bulletin de la Soci t  G ologique de France*, 2008, 179(3) : 179-192.

217 Brun, J.P., 2002. Deformation of the continental lithosphere: Insights from brittle-ductile
218 models. In : De Meer S., Drury M., De Bresser J.H.P., Pennock G.M., *Deformation mechanisms,*
219 *rheology and tectonics : Current status and future perspectives.* Geological Society of
220 London, Special Publication, vol. 200. 355-370.

221 Burbank, D.W., 2002. Rates of erosion and their implications for exhumation. *Mineral. Mag.*,
222 66, 25–52.

223 Chapple, W.M., 1978. Mechanics of thin-skinned fold-and-thrust belts. *Geological Society of*
224 *America Bulletin*, 89 : 1189-1198.

225 Cobbold, P.R., Durand, S. and Mourgues, R., 2001. Sandbox modelling of thrust wedges with
226 fluid-assisted detachments, *Tectonophysics*, 334, 245 – 258.

227 Crespi, J. M., Chan, Y. -C., and Swaim, M. S., 1996, Synorogenic extension and exhumation of the
228 Taiwan hinterland : *Geology*, v. 24, p. 247-250.

229 Cruz, L ., Teyssier, C., Perg, L., Take, A., Fayon, A., 2008. Deformation, exhumation, and
230 topography of experimental doubly-vergent orogenic wedges subjected to asymmetric
231 erosion, *Journal of Structural Geology*, 30 (2008), 98-115.

232 Dahlen, F.A., 1984. Non Cohesive Critical Coulomb Wedges : An Exact Solution. *Journal of*
233 *Geophysical Research*, 89 (B12), 10 125-10 133.

234 Dahlen, F.A., Suppe, J. & Davis, D., 1984. Mechanics of fold-and-thrust belts and accretionary
235 wedges : cohesive coulomb theory. *Journal of Geophysical Research*, 89 (B12), 10 087-10
236 101.

237 Dahlen, F.A., 1988. Mechanical energy budget of a fold-and-thrust belt. *Nature*, 331 : 335-337.

238 Dahlen, F.A. & Suppe, J., 1988. Mechanics, growth, and erosion of mountain belts. *Geological*
239 *Society of America, Special Paper*, 218 : 161-178.

240 Dahlen, F.A. & Barr, T.D., 1989. Brittle Frictional Mountain Building, 1. Deformation and
241 mechanical energy budget. *Journal of Geophysical Research*, 94 : 3906-3922.

242 Davis, D., Suppe, J. & Dahlen, F.A., 1983. Mechanics of fold-and-thrust belts and accretionary
243 wedges. *Journal of Geophysical Research*, 88 (B12), 1153-1172.

244 Dewey, J., & Bird, J., 1970. Mountain belts and the new Global Tectonics, *J. Geophys. Res.*, 75,
245 2625-2647.

246 Ellis, S., & Beaumont, C., 1999. Models of convergent boundary tectonics : implications for the
247 interpretation of Lithoprobe data, *Can. J. Earth Sci.*, 36, 1 711-1 745.

248 England, P.C., & Molnar, P., 1990. Surface uplift, uplift of rocks and exhumation of rock.
249 *Geology*, 18(12), 1173-1177.

250 Graveleau, F., 2008. Interactions Tectonique, Erosion, Sédimentation dans les avant-pays de
251 chaînes : Modélisation analogique et étude des piémonts de l'est du Tian Shan (Asie
252 centrale), Thesis, Université Montpellier II - Sciences et Techniques du Languedoc,
253 (17/10/2008), 487pp.

254 Hilley, G.E. & Strecker, M.R., 2004. Steady state erosion of critical Coulomb wedges with
255 applications to Taiwan and the Himalaya. *Journal of Geophysical Research*, 109, B01411,
256 doi:10.1029/2002JB002284.

257 Horton, B.K., 1999. Erosional control on the geometry and kinematics of thrust belt
258 development in the central Andes. *Tectonics*, 18 : 1292-1304.

259 Jamieson, R.A. & Beaumont, C., 1989. Deformation and metamorphism in convergent orogens:
260 a model for uplift and exhumation of metamorphic terranes. In: Daly, J.S., Cliff R.A. et Yardley
261 B.W. (eds.), *Evolution of Metamorphic Belts*, *Geol. Soc. Lond. Spec. Publ.*, 43, 17-129.

262 Konstantinovskaia, E., & Malavieille, J., 2005. Erosion and exhumation in accretionary
263 orogens: Experimental and geological approaches, *Geochemistry, Geophysics and*
264 *Geosystems*, 6, Q02006, doi:10.1029/2004GC000794.

265 Kühni, A., and Pfiffner, O. A., 2001. Drainage patterns and tectonic forcing: A model study for
266 the Swiss Alps, *Basin Res.*, 13, 169 – 197.

267 Kukowski, N., Lallemand, S., Malavieille, J., Gutscher, M.-A. and Reston, T.J., 2002. Mechanical
268 decoupling and basal duplex formation observed in sandbox experiments with application to
269 the Mediterranean Ridge accretionary complex. *Marine Geology*, 186: 29-42.

270 Leturmy, P., Mugnier, J.L., Vinour, P., Baby, P., Colletta, B. and Chabron E., 2000. Piggyback
271 basin development above a thin-skinned thrust belt with two detachment levels as a
272 function of interactions between tectonic and superficial mass transfer : the case of the
273 Subandean Zone (Bolivia). *Tectonophysics*, 320 : 45-67.

- 274 Lohrmann, J., Kukowski, N., Adam, J. and Oncken, O., 2003. The impact of analogue material
275 properties on the geometry, kinematics, and dynamics of convergent sand wedges. *Journal of*
276 *Structural Geology*, 25(10) : 1691-1711.
- 277 Malavieille, J., 1984. Modélisation expérimentale des chevauchements imbriqués: application
278 aux chaînes de montagnes. *Bulletin de la Société Géologique de France*, 26 : 129-138.
- 279 Malavieille, J. & Chemenda, A., 1997. Impact of initial geodynamic settings on the structure,
280 ophiolite emplacement and tectonic evolution of collisional belts. *Ofioliti*, 22 (1), 3-13.
- 281 Mattauer, M., 1986, Intracrustal subduction, crust–mantle decollement and crustal-stacking
282 wedge in the Himalayas and other collision belts, *Geol. Soc. London Collision Tectonics*. Vol
283 *Spec 19* (1986), pp. 37–50.
- 284 Naylor, M., Sinclair, H. D., Willett, S., and Cowie, P. A., 2005, A discrete element model for
285 orogenesis and accretionary wedge growth, *J. Geophys. Res.*, 110, B12403,
286 doi:10.1029/2003JB002940.
- 287 Pérez-Estaún, A., Martínez-Catalan, J.R., and Bastida, F., 1991. Crustal thickening and
288 deformation sequence in the footwall to the suture of the Variscan belt of northwest Spain.
289 In A. Pérez-Estaún and M.P. Coward (Editors), *Deformation and Plate Tectonics*.
290 *Tectonophysics*, 191 : 243-253.
- 291 Persson, K.S. & Sokoutis, D., 2002. Analogue models of orogenic wedges controlled by erosion.
292 *Tectonophysics*, 356 : 323-336
- 293 Pfiffner, O.A., Ellis, S., & Beaumont, C., 2000. Collision tectonics in the Swiss Alps: Insight from
294 geodynamic modeling. *Tectonics*, 19, 6, 1065-1094.
- 295 Platt, J.P., 1986. Dynamics of orogenic wedges and the uplift of high-pressure metamorphic
296 rocks. *Geological Society of America Bulletin*, 97: 1037-1053.
- 297 Selzer, C., S. J. H. Buiter, and O. A. Pfiffner, 2008. Numerical modeling of frontal and basal
298 accretion at collisional margins, *Tectonics*, 27, TC3001, doi:10.1029/ 2007TC002169.
- 299 Simpson, G.D.H., 2006. How and to what extent does the emergence of orogens above sea level
300 influence their tectonic development? *Terra Nova*, 18, 447–451, 2006, doi: 10.1111/j.1365-
301 3121.2006.00711.
- 302 Stockmal, G.S., Beaumont, C., Nguyen, M. and Lee, B., 2007. Mechanics of thin-skinned fold-
303 and-thrust belts: Insights from numerical models, *The Geological Society of America*, Special
304 *Paper 433*, p. 63-98.
- 305 Willett, S.D., Beaumont, C. and Fullsack, P., 1993. Mechanical model for the tectonics of doubly
306 vergent compressional orogens. *Geology*, 21(4) : 371-374.
- 307 Willett, S.D., 1999. Orogeny and orography : The effects of erosion on the structure of
308 mountain belts, *Journal of Geophysical Research*, 104(B12) : 28 957–28 982.
- 309 Willett, S.D. & Brandon, M.T., 2002. On steady states in mountain belts. *Geology*, 30 : 175-178.

310 **Figure captions**

311 Figure A : a) Kinematic setting of continental subduction. b) Schematic setting used for
312 analogue modeling of thrust wedges. Backstop geometries and rheologies can be modified.
313 Dotted line represents the chosen erosion surface.

314 Figure B : Cartoon showing deformation partitioning and kinematics of thrust units in a
315 décollement type wedge. Notice the deformation of upper plate (orogenic lid) resting on top
316 of the former refolded décollement. Early folds are suggested to show evolution of U-P
317 geometry. A possible deformation mechanism responsible for vertical shear inducing
318 stretching and thinning of the underplated units is schematized. Red ellipsoids show resulting
319 strain. U-P = pre-structured upper-plate, L-P = basement lower-plate.

320 Figure C : Conceptual model of orogenic wedge growth showing the impact of surface
321 processes; a) end of oceanic subduction stage (early exhumation of high pressure rocks in the
322 subduction channel), b) subduction of the continental margin, stacking of underplated crust
323 units and uplift favored erosion of the upper plate, c) a new stage of basal accretion develops
324 in the foreland inverting inherited features of the margin, d) during the late stages, major
325 backthrusting develops at the back of the wedge due to strong thinning of the upper plate lid
326 by erosion. Synformal U.P. klippen are preserved between domains of underplating.

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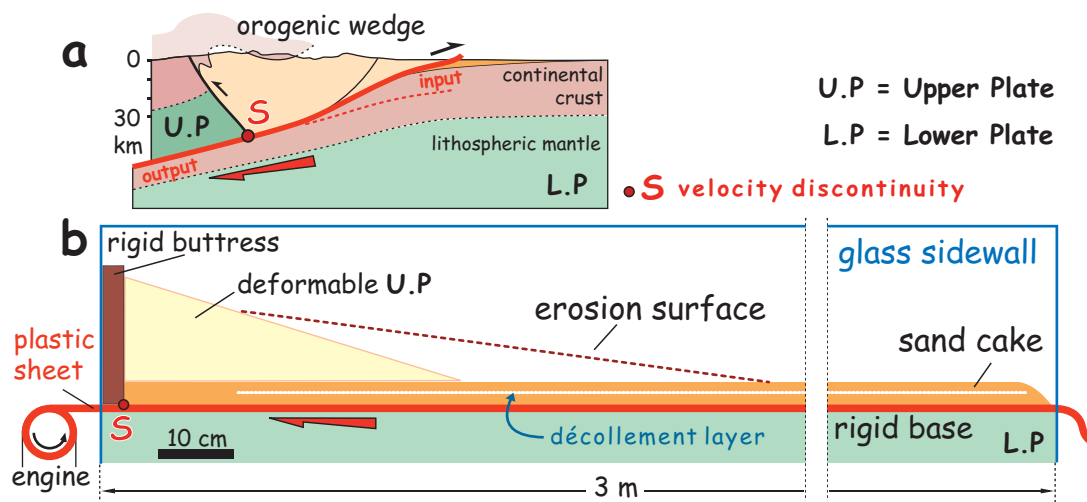


Figure A

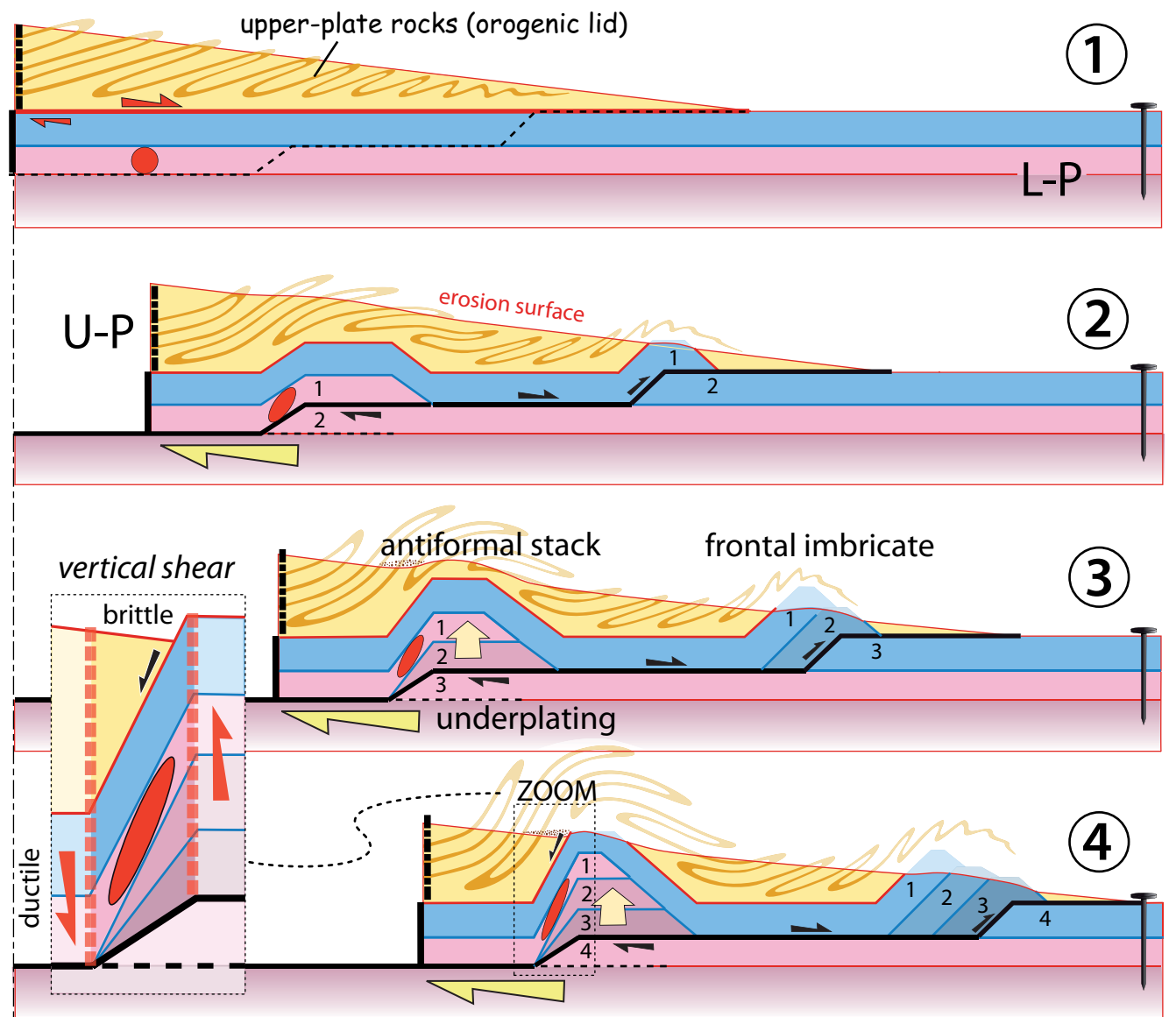


Figure B

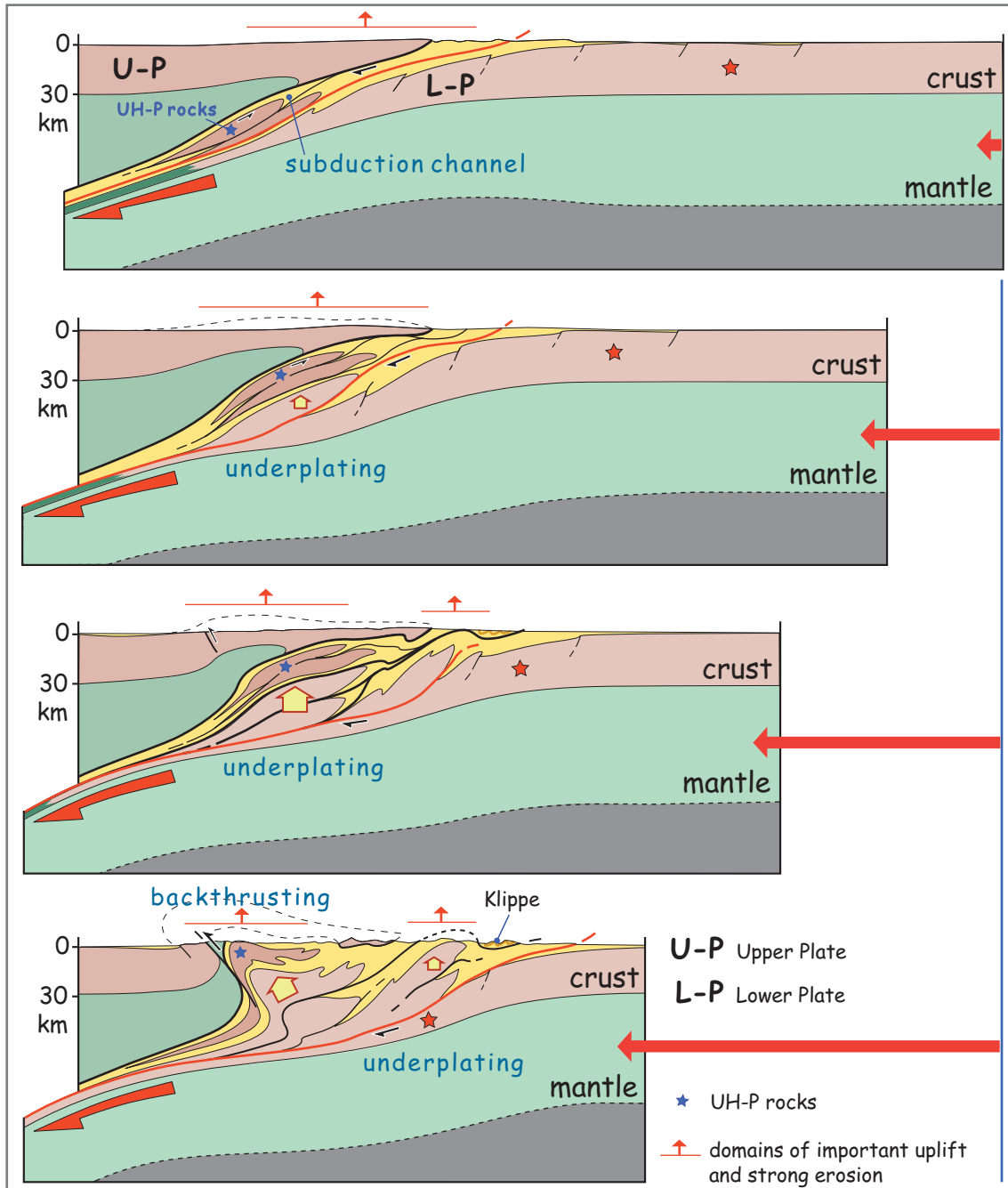


Figure C