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SUPPLEMENTAL FILES

An Amazonian Mesoproterozoic basement in the core of the Ibero-Armorican Arc: $^{39}Ar/^{40}Ar$ detrital mica ages tell their tale.

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Sampling and procedures

Sample locations are shown in Figure 1A together with a synthetic stratigraphic column (Fig. 1B). Samples were collected in coarse grained sandstones, where the detrital micas are observable under a hand lens.

The <297 µm-size mineral fraction was selected and placed in a Holman-Wilfley Table. Different conditions were tried to obtain a fraction preferentially enriched in detrital mica. This step of separation was particularly useful to eliminate the fine fraction (< 2 µm), heavy minerals and a part of rounded grains. The fraction such enriched was used for magnetic separation at 0.9 amp. with 8º lateral tilt that allowed separation of micas from quartz and feldspar. Finally around 50 clean mica grains were hand picked from each sample avoiding those ones with any sign of intergrowth or stained aspect.

In order to obtain textural and chemical information, a Zeiss DSM 950 SEM equipped with an X-ray Link Analytical QX-20 energy-dispersive system (EDX) has been used at the Centro de Instrumentación Científica (C.I.C.) of the Universidad de Granada. Microprobe analyses of white K-micas were performed using wavelength-dispersive spectroscopy (WDX) on a Cameca SX50 electron microprobe (EMPA) at the C.I.C.. The instrument was set at an accelerating voltage of 20 kV, with a beam current of 30 nA and a beam diameter of <5 μm. Data were reduced using the procedure of Pouchou and Pichoir (1985) and the standards used were albite, orthoclase, periclase, wollastonite and synthetic oxides (Al_2O_3, Fe_2O_3 and $MnTiO_3$).

The study by back-scattered electron (BSE) imaging has allowed controlling the absence of signs of metamorphic alteration in white micas as for example the existence of mica/chlorite stacks.

The chemical composition of the detrital micas extends over a wide range (Table 1; Fig. 1 of this repository) suggesting a wide variety of possible rock types and geodynamic environments for their source including igneous or related to low-intermediate pressure metamorphism, as the Si content is always less than 3.25 a.p.f.u. (atoms per formula unit). In general, there are no compositional differences between the detrital micas of the Ediacaran and Cambrian sediments (Fig. 1a), with the only exception of some micas of Cambrian sediments, which present a slightly higher ferrimuscovite component (Fig.1b).

The wide range of chemical compositions of detrital micas (Fig. 1 of this repository) and the absence of stacks (SEM study) are significant arguments against any possible metamorphic resetting, that would produce homogeneous chemical compositions of muscovites in equilibrium with the new metamorphic conditions. Additionally, illitic (low K+Na content) instead of muscovitic compositions would be expectable in such low grade metamorphic conditions.

IR laser single grain total fusion

Twenty four single grain total fusion analysis (12 from Ediacaran (MD-1) and 12 from the Cambrian (MD-2) sediments) were performed in this study. After handpicking, the selected mineral grains were cleaned in methanol, followed by deionised water in an ultrasonic bath. Samples were then individually wrapped in aluminium foil, and all the samples were loaded into an aluminium package. Biotite age standard Tinto B (K-Ar age of 409.24 ± 0.71 Ma (Rex and Guise, 1995) was loaded at 5 mm intervals along the package to monitor the neutron flux gradient. The package was Cd-shielded and irradiated in the 5C position of the McMaster University Nuclear Reactor, Hamilton, Canada, for 90 hours. Upon return, the samples were loaded into an ultra-high vacuum laser chamber with a Kovar viewport and baked to 120°C overnight to remove adsorbed atmospheric argon from the samples and chamber walls.

A 110 W Spectron Laser Systems continuous-wave neodymium-yttrium-aluminium-garnet (CW-Nd-YAG) (λ = 1064 nm) laser, fitted with a TEM00 aperture, was used to totally fuse each single grain. The laser was fired through a Merchantek computer-controlled X-Y-Z sample chamber stage and microscope system, fitted with a high-resolution CCD camera, 6x computer controlled zoom, high magnification objective lens, and two light sources for sample illumination.

The gases released by laser heating were 'gettered' using 3 SAES AP10 getter pumps to remove all active gases (CO_2, H_2O, H_2, N_2, O_2, CH_4, etc.). The remaining noble gases were equilibrated into a high sensitivity mass spectrometer (MAP 215-50), operated at a resolution of 600, and fitted with a Balzers SEV 217 multiplier. The automated extraction and data acquisition system was computer controlled, using a LabView program. The mean 5 minutes extraction system blank Ar isotope measurements obtained during the experiments were 1.43 x 10^{-12}, 1.08 x 10^{-14}, 2.71 x 10^{-15}, and 1.36 x 10^{-14}, cm^3 STP (standard temperature and pressure) for ^{40}Ar, ^{39}Ar, ^{38}Ar, ^{37}Ar, and ^{36}Ar respectively. Samples were corrected for mass spectrometer discrimination and nuclear interference reactions. Errors quoted on the ages are 1 sigma, and Ar-Ar ages were calculated using the decay constant quoted by Steiger and Jäger (1977). J values and errors are noted on the sample ^{40}Ar-^{39}Ar data table (Table 2).

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Steiger, R. J., Jäger, E., 1977. Subcommission on geochronology: Convention on the use of decay constants in geo- and cosmochronology. Earth and Planetary Science Letters, 36, 359-362

Figure Caption

Figure 1.- Diagrams of the chemical composition corresponding to the studied detrital micas (MD-1 and MD-2).

TABLE 1 –WHITE MICA GEOCHEMICAL DATA

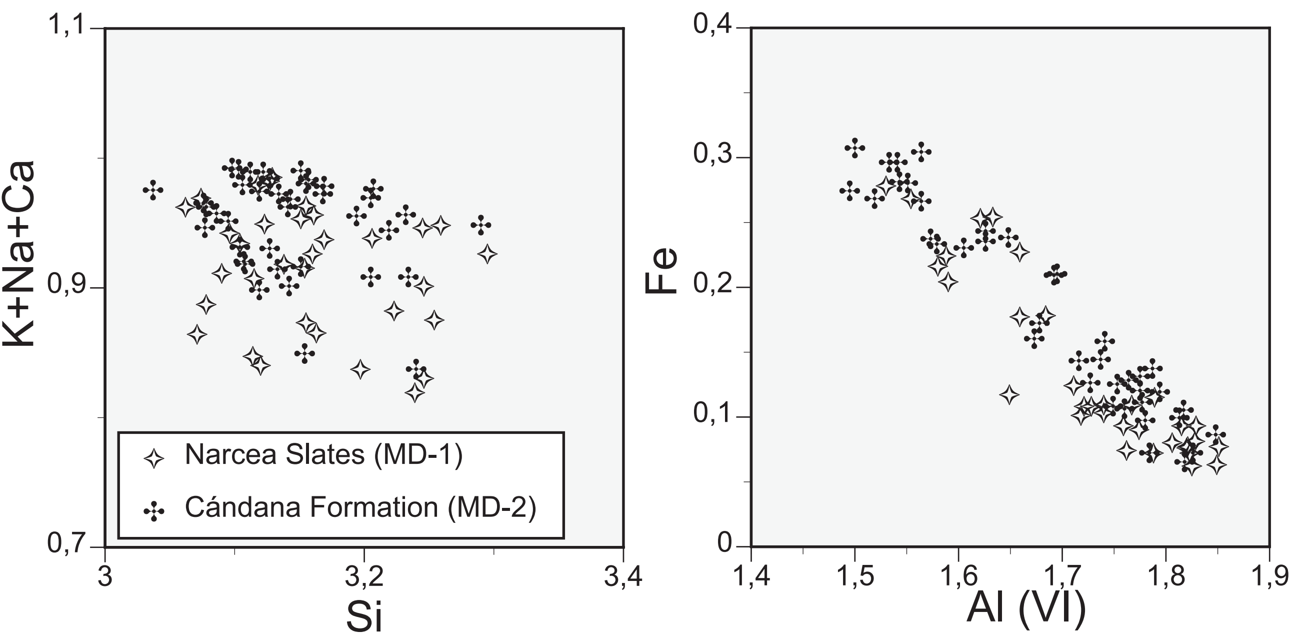
Samples	Si	AlIV	AlVI	Fe	Mg	Mn	Ti	Cr	Ni	oct.	K	Na	Ca	inter.	Al tot	Fe+Mg	O	OH	F	Cl
										(Atoms per formula unit)										
SAMPLE MD-2. 1. 1	3.119	0.881	1.787	0.137	0.072	0.003	0.005	0.000	0.000	2.005	0.943	0.030	0.002	0.974	2.668	0.209	10	1.999	0.000	0.000
SAMPLE MD-2. 1. 2	3.076	0.924	1.741	0.158	0.099	0.001	0.025	0.001	0.001	2.027	0.855	0.109	0.001	0.965	2.665	0.258	10	1.990	0.009	0.000
SAMPLE MD-2. 2 .1	3.078	0.922	1.794	0.119	0.077	0.000	0.024	0.000	0.000	2.015	0.826	0.136	0.000	0.962	2.716	0.197	10	1.975	0.025	0.000
SAMPLE MD-2 2. 4. 1	3.207	0.793	1.500	0.307	0.192	0.001	0.022	0.000	0.001	2.023	0.949	0.025	0.001	0.976	2.293	0.499	10	1.980	0.019	0.001
SAMPLE MD-2 2. 4. 2	3.168	0.832	1.533	0.296	0.186	0.003	0.017	0.000	0.001	2.036	0.939	0.032	0.001	0.972	2.365	0.482	10	1.965	0.035	0.000
SAMPLE MD-2 to 3. 2	3.037	0.963	1.817	0.105	0.041	0.001	0.041	0.003	0.000	2.008	0.885	0.089	0.001	0.975	2.780	0.146	10	1.988	0.012	0.000
SAMPLE MD-2 to 3. 3	3.234	0.766	1.673	0.160	0.136	0.001	0.031	0.000	0.000	2.002	0.881	0.026	0.001	0.908	2.439	0.297	10	1.976	0.015	0.009
SAMPLE MD-2 to 3. 4	3.240	0.760	1.678	0.172	0.143	0.001	0.032	0.001	0.000	2.027	0.815	0.020	0.001	0.837	2.437	0.315	10	1.973	0.017	0.010
SAMPLE MD-2 3. 1	3.290	0.710	1.495	0.274	0.231	0.001	0.015	0.001	0.000	2.018	0.934	0.014	0.001	0.948	2.204	0.506	10	1.970	0.030	0.000
SAMPLE MD-2 3. 2. 1	3.108	0.892	1.818	0.065	0.092	0.000	0.039	0.004	0.000	2.019	0.835	0.083	0.000	0.918	2.710	0.157	10	1.998	0.002	0.000
SAMPLE MD-2 3. 2. 2	3.095	0.905	1.784	0.072	0.106	0.001	0.047	0.004	0.000	2.015	0.869	0.081	0.000	0.951	2.689	0.178	10	2.000	0.000	0.000
SAMPLE MD-2 5. 1. 1	3.143	0.857	1.626	0.235	0.108	0.016	0.029	0.000	0.000	2.014	0.936	0.032	0.000	0.968	2.483	0.343	10	1.999	0.000	0.001
SAMPLE MD-2 5. 2. 1	3.142	0.858	1.648	0.238	0.105	0.018	0.028	0.001	0.001	2.040	0.875	0.026	0.000	0.901	2.506	0.344	10	1.983	0.017	0.000
SAMPLE MD-2 5. 2. 2	3.086	0.914	1.826	0.072	0.079	0.000	0.031	0.001	0.000	2.009	0.869	0.088	0.000	0.957	2.739	0.151	10	2.000	0.000	0.000
SAMPLE MD-2 5. 3	3.169	0.831	1.551	0.280	0.167	0.001	0.024	0.000	0.000	2.022	0.949	0.029	0.000	0.978	2.382	0.447	10	1.989	0.009	0.001
SAMPLE MD-2 5. 4	3.157	0.843	1.543	0.281	0.163	0.002	0.032	0.000	0.000	2.021	0.936	0.047	0.000	0.983	2.386	0.444	10	1.983	0.017	0.000
SAMPLE MD-2 5. 5 green edge	3.141	0.859	1.775	0.120	0.091	0.001	0.015	0.000	0.000	2.002	0.908	0.054	0.000	0.962	2.635	0.211	10	1.957	0.042	0.001
SAMPLE MD-2 5. 5. 1	3.151	0.849	1.775	0.131	0.093	0.001	0.015	0.000	0.000	2.016	0.879	0.037	0.000	0.916	2.624	0.224	10	1.956	0.043	0.001
SAMPLE MD-2 5. 6	3.103	0.897	1.764	0.128	0.102	0.001	0.014	0.000	0.000	2.010	0.936	0.054	0.001	0.991	2.661	0.230	10	1.979	0.020	0.001
SAMPLE MD-2 5 to 4. 1. 1	3.077	0.923	1.813	0.099	0.069	0.001	0.032	0.000	0.000	2.014	0.907	0.038	0.001	0.946	2.736	0.169	10	1.991	0.009	0.001
SAMPLE MD-2 5 to 4. 1. 2	3.106	0.894	1.753	0.125	0.095	0.001	0.030	0.000	0.000	2.004	0.947	0.031	0.001	0.979	2.647	0.220	10	1.993	0.007	0.000
SAMPLE MD-2 5 to 4. 1. 3	3.112	0.888	1.716	0.143	0.124	0.001	0.028	0.000	0.000	2.011	0.962	0.027	0.000	0.989	2.604	0.266	10	1.987	0.013	0.000
SAMPLE MD-2 4. 1	3.133	0.867	1.737	0.144	0.122	0.000	0.026	0.000	0.000	2.029	0.890	0.023	0.001	0.914	2.604	0.266	10	1.989	0.010	0.001
SAMPLE MD-2 4. 2. 1	3.205	0.795	1.579	0.233	0.169	0.001	0.027	0.001	0.001	2.011	0.925	0.044	0.001	0.969	2.374	0.401	10	1.946	0.054	0.000
SAMPLE MD-2 4. 2. 2	3.205	0.795	1.605	0.230	0.163	0.001	0.028	0.000	0.000	2.027	0.870	0.038	0.001	0.908	2.400	0.393	10	1.945	0.055	0.000
SAMPLE MD-2 6. 1. 1	3.104	0.896	1.692	0.209	0.097	0.007	0.027	0.000	0.001	2.033	0.868	0.063	0.000	0.931	2.588	0.306	10	1.897	0.103	0.000
SAMPLE MD-2 6. 1. 2	3.107	0.893	1.695	0.210	0.097	0.006	0.026	0.000	0.000	2.034	0.864	0.056	0.000	0.920	2.588	0.307	10	1.891	0.108	0.001
SAMPLE MD-2 7. 1	3.134	0.866	1.749	0.108	0.164	0.001	0.005	0.000	0.001	2.028	0.913	0.059	0.000	0.972	2.616	0.272	10	1.987	0.012	0.000
SAMPLE MD-2 8. 1. 1	3.098	0.902	1.760	0.106	0.112	0.000	0.029	0.000	0.000	2.007	0.948	0.044	0.000	0.992	2.662	0.218	10	1.999	0.001	0.000
SAMPLE MD-2 8. 1. 2	3.119	0.881	1.777	0.111	0.112	0.000	0.030	0.000	0.001	2.031	0.869	0.028	0.000	0.898	2.658	0.222	10	1.985	0.015	0.000
SAMPLE MD-2 8. 2	3.122	0.878	1.727	0.126	0.124	0.000	0.029	0.000	0.000	2.005	0.954	0.034	0.000	0.989	2.604	0.249	10	1.986	0.014	0.000

SAMPLE MD-2 8. 3	3.194	0.806	1.564	0.304	0.139	0.004	0.010	0.000	0.000	2.020	0.937	0.018	0.000	0.955	2.370	0.442	10	1.960	0.040	0.000
SAMPLE MD-2 8. 4	3.232	0.768	1.573	0.237	0.194	0.001	0.013	0.000	0.000	2.018	0.924	0.032	0.000	0.956	2.341	0.431	10	1.984	0.016	0.000
SAMPLE MD-2 8. 5. 1	3.151	0.849	1.564	0.266	0.132	0.001	0.042	0.000	0.000	2.006	0.962	0.027	0.001	0.990	2.413	0.398	10	1.981	0.019	0.000
SAMPLE MD-2 8. 5. 2	3.127	0.873	1.626	0.243	0.124	0.001	0.023	0.000	0.000	2.017	0.957	0.028	0.000	0.984	2.499	0.367	10	1.977	0.022	0.000
SAMPLE MD-2 8. 6	3.155	0.845	1.541	0.296	0.147	0.000	0.034	0.000	0.000	2.018	0.960	0.020	0.000	0.980	2.386	0.444	10	1.980	0.020	0.000
SAMPLE MD-2 9. 1	3.219	0.781	1.519	0.268	0.195	0.005	0.036	0.001	0.000	2.023	0.905	0.039	0.000	0.944	2.299	0.463	10	1.961	0.036	0.002
SAMPLE MD-2 9. 2	3.127	0.873	1.780	0.097	0.158	0.000	0.005	0.000	0.001	2.041	0.878	0.051	0.001	0.930	2.653	0.255	10	1.992	0.007	0.001
SAMPLE MD-2 9. 3	3.154	0.846	1.848	0.086	0.071	0.000	0.019	0.000	0.000	2.024	0.750	0.097	0.002	0.849	2.694	0.157	10	1.986	0.013	0.001
SAMPLE MD-1. 1. 1	3.129	0.871	1.530	0.275	0.174	0.001	0.048	0.000	0.001	2.029	0.971	0.011	0.000	0.982	2.401	0.449	10	1.974	0.026	0.000
SAMPLE MD-1. 2. 1	3.138	0.862	1.554	0.265	0.177	0.002	0.050	0.000	0.000	2.047	0.909	0.006	0.000	0.915	2.415	0.442	10	1.981	0.018	0.000
SAMPLE MD-1. 4 to 5. 1	3.295	0.705	1.580	0.213	0.209	0.000	0.010	0.001	0.001	2.013	0.879	0.043	0.001	0.923	2.285	0.422	10	1.970	0.029	0.000
SAMPLE MD-1. 6. 3. 1	3.074	0.926	1.806	0.077	0.078	0.000	0.044	0.001	0.001	2.006	0.917	0.049	0.000	0.966	2.732	0.155	10	1.996	0.004	0.001
SAMPLE MD-1. 6. 3. 2	3.078	0.922	1.828	0.078	0.082	0.000	0.045	0.002	0.001	2.034	0.846	0.038	0.001	0.884	2.750	0.160	10	1.983	0.016	0.001
SAMPLE MD-1. 6. 4	3.123	0.877	1.740	0.106	0.130	0.001	0.040	0.001	0.000	2.018	0.906	0.038	0.002	0.946	2.617	0.236	10	1.978	0.022	0.000
SAMPLE MD-1. 6. 5	3.254	0.746	1.728	0.105	0.192	0.000	0.005	0.000	0.001	2.032	0.819	0.048	0.005	0.872	2.474	0.298	10	1.976	0.023	0.000
SAMPLE MD-1. 6 to 7. 1	3.223	0.777	1.759	0.090	0.148	0.001	0.020	0.002	0.000	2.019	0.790	0.087	0.003	0.879	2.536	0.238	10	1.965	0.018	0.017
SAMPLE MD-1. 7. 1. 1	3.239	0.761	1.774	0.087	0.151	0.000	0.021	0.002	0.000	2.035	0.750	0.065	0.002	0.816	2.535	0.238	10	1.976	0.008	0.016
SAMPLE MD-1. 7. 1. 2	3.104	0.896	1.825	0.059	0.092	0.000	0.036	0.001	0.001	2.015	0.813	0.117	0.001	0.931	2.721	0.151	10	1.994	0.006	0.000
SAMPLE MD-1. 7. 2	3.120	0.880	1.849	0.060	0.092	0.000	0.037	0.002	0.001	2.041	0.758	0.077	0.002	0.837	2.730	0.152	10	1.988	0.011	0.000
SAMPLE MD-1. 8. 1	3.161	0.839	1.767	0.106	0.123	0.001	0.012	0.000	0.001	2.009	0.908	0.044	0.001	0.953	2.606	0.229	10	1.981	0.018	0.001
SAMPLE MD-1. 8. 2	3.163	0.837	1.789	0.112	0.124	0.000	0.013	0.001	0.001	2.040	0.831	0.031	0.000	0.862	2.626	0.236	10	1.982	0.017	0.001
SAMPLE MD-1. 8. 3	3.245	0.755	1.649	0.114	0.271	0.001	0.002	0.000	0.001	2.037	0.919	0.024	0.000	0.943	2.403	0.385	10	1.995	0.005	0.000
SAMPLE MD-1. 8 to 9. 1	3.062	0.938	1.821	0.074	0.047	0.000	0.055	0.002	0.001	1.999	0.866	0.092	0.001	0.959	2.760	0.120	10	1.990	0.010	0.001
SAMPLE MD-1. 9. 1	3.071	0.929	1.851	0.074	0.047	0.000	0.055	0.002	0.000	2.029	0.800	0.060	0.001	0.861	2.780	0.121	10	1.990	0.009	0.001
SAMPLE MD-1. 9. 2. 1	3.206	0.794	1.684	0.175	0.134	0.000	0.015	0.000	0.000	2.008	0.908	0.024	0.002	0.935	2.479	0.309	10	1.981	0.019	0.000
SAMPLE MD-1. 9. 2. 2	3.127	0.873	1.659	0.224	0.097	0.002	0.025	0.000	0.000	2.008	0.947	0.033	0.000	0.979	2.533	0.321	10	1.985	0.015	0.000
SAMPLE MD-1. 9. 3	3.155	0.845	1.621	0.250	0.114	0.001	0.026	0.000	0.000	2.012	0.925	0.034	0.001	0.960	2.466	0.364	10	1.989	0.011	0.000
SAMPLE MD-1. 9. 4	3.154	0.846	1.633	0.251	0.118	0.003	0.026	0.000	0.000	2.031	0.880	0.031	0.001	0.912	2.479	0.369	10	1.981	0.019	0.000
SAMPLE MD-1. 10. 1	3.246	0.754	1.718	0.098	0.144	0.001	0.036	0.005	0.000	2.003	0.853	0.042	0.003	0.898	2.471	0.242	10	1.944	0.054	0.001
SAMPLE MD-1. 11. 1	3.246	0.754	1.740	0.100	0.145	0.001	0.036	0.005	0.000	2.027	0.796	0.028	0.003	0.827	2.494	0.245	10	1.931	0.067	0.002
SAMPLE MD-1. 11. 2	3.155	0.845	1.829	0.090	0.095	0.001	0.013	0.000	0.001	2.029	0.807	0.060	0.004	0.870	2.673	0.186	10	1.985	0.013	0.002
SAMPLE MD-1. 11. 3	3.197	0.803	1.815	0.090	0.118	0.000	0.011	0.000	0.000	2.034	0.788	0.042	0.004	0.834	2.617	0.208	10	1.987	0.012	0.001
SAMPLE MD-1. 11 to 12. 1	3.096	0.904	1.762	0.071	0.109	0.001	0.066	0.002	0.000	2.012	0.876	0.061	0.001	0.939	2.666	0.180	10	1.986	0.013	0.001
SAMPLE MD-1. 11 to 12. 2	3.114	0.886	1.788	0.069	0.112	0.002	0.066	0.003	0.001	2.040	0.804	0.039	0.002	0.844	2.673	0.181	10	2.000	0.000	0.000
SAMPLE MD-1. 11 to 12. 3	3.160	0.840	1.711	0.121	0.127	0.000	0.050	0.001	0.001	2.011	0.879	0.043	0.001	0.923	2.551	0.248	10	1.983	0.015	0.001

SAMPLE MD-1. 12. 1. 1	3.118	0.882	1.721	0.105	0.121	0.003	0.052	0.001	0.000	2.003	0.933	0.041	0.002	0.976	2.603	0.226	10	1.976	0.024	0.000
SAMPLE MD-1. 12. 1. 2	3.115	0.885	1.820	0.073	0.098	0.000	0.031	0.001	0.002	2.025	0.735	0.168	0.002	0.904	2.705	0.171	10	2.000	0.000	0.000
SAMPLE MD-1. 12. 2. 1	3.090	0.910	1.823	0.069	0.090	0.001	0.040	0.001	0.000	2.025	0.720	0.187	0.001	0.908	2.733	0.159	10	1.997	0.003	0.000
SAMPLE MD-1. 12. 3	3.151	0.849	1.659	0.174	0.120	0.003	0.049	0.000	0.001	2.006	0.901	0.048	0.001	0.950	2.508	0.294	10	1.927	0.073	0.000
SAMPLE MD-1. 12. 4	3.259	0.741	1.590	0.201	0.156	0.003	0.039	0.000	0.000	1.989	0.892	0.053	0.001	0.945	2.331	0.357	10	1.943	0.056	0.000
SAMPLE MD-1.out	3.169	0.831	1.588	0.221	0.176	0.002	0.043	0.004	0.000	2.034	0.900	0.032	0.002	0.934	2.419	0.397	10	1.972	0.027	0.001

TABLE 2. 40Ar/39Ar ANALYTICAL RESULTS

Grain	Age (Ma)	+- (Ma)	40Ar*/39Ar	+- (σ1)	40Ar/39Ar	+- (σ1)	38Ar/39Ar	+- (σ1)	37Ar/39Ar	+- (σ1)	36Ar/39Ar	+- (σ1)	39Ar (cm3)	+- (σ1)
SAMPLE MD-1														
Grain 1	**628,08**	**4,67**	19,32	0,14	19,99	0,04	0,01348	0,00101	0,04167	0,04114	0,00225	0,00045	2,99E-12	5,59E-15
2	**662,88**	**3,04**	20,60	0,05	20,64	0,02	0,01305	0,00014	0,01286	0,02840	0,00014	0,00014	9,69E-12	8,24E-15
3	**719,27**	**3,24**	22,73	0,05	22,93	0,03	0,01320	0,00028	0,06440	0,01272	0,00068	0,00014	9,69E-12	1,12E-14
4	**714,29**	**9,03**	22,54	0,33	23,46	0,11	0,01283	0,00006	0,09596	0,09474	0,00310	0,00104	1,30E-12	6,06E-15
5	**634,06**	**2,80**	19,54	0,03	19,83	0,03	0,01273	0,00012	0,01110	0,03288	0,00096	0,00000	1,12E-11	1,68E-14
6	**648,26**	**2,87**	20,06	0,03	20,24	0,03	0,01249	0,00031	0,08637	0,08527	0,00060	0,00000	4,34E-12	6,78E-15
7	**590,23**	**3,01**	17,96	0,06	18,01	0,02	0,01160	0,00001	0,00000	0,00000	0,00019	0,00019	7,19E-12	5,42E-15
8	**598,03**	**2,97**	18,24	0,05	18,45	0,05	0,01197	0,00003	0,00000	0,00000	0,00072	0,00010	1,32E-11	3,25E-14
9	**631,31**	**3,04**	19,44	0,05	19,44	0,02	0,01204	0,00001	0,00000	0,00000	0,00000	0,00000	1,64E-11	1,63E-14
10	**634,58**	**3,14**	19,56	0,06	19,73	0,02	0,01264	0,00001	0,00000	0,00000	0,00059	0,00020	1,39E-11	1,09E-14
11	**783,48**	**3,21**	25,24	0,02	25,23	0,02	0,01185	0,00013	0,01187	0,01172	0,00000	0,00000	2,11E-11	1,36E-14
12	**632,08**	**2,71**	19,47	0,02	19,47	0,02	0,01274	0,00001	0,00000	0,00000	0,00000	0,00000	1,00E-11	8,13E-15
SAMPLE MD-2														
Grain 1	**44,77**	**2,02**	1,17	0,05	1,22	0,00	0,01307	0,00013	0,01078	0,01065	0,00018	0,00018	2,27E-11	2,21E-14
2	**918,38**	**4,41**	30,80	0,11	30,97	0,03	0,01209	0,00012	0,00000	0,00000	0,00058	0,00035	1,16E-11	9,09E-15
3	**1590,20**	**5,62**	65,63	0,12	65,63	0,12	0,01410	0,00044	0,00000	0,00000	0,00000	0,00000	3,06E-12	5,42E-15
4	**1784,60**	**5,87**	78,37	0,10	78,36	0,10	0,01306	0,00035	0,08515	0,00011	0,00000	0,00000	8,62E-12	1,08E-14
5	**46,70**	**0,26**	1,22	0,00	1,22	0,00	0,01083	0,00001	0,00000	0,00000	0,00000	0,00000	8,73E-12	8,24E-15
6	**644,91**	**3,00**	19,94	0,05	19,94	0,05	0,01331	0,00003	0,00000	0,00000	0,00000	0,00000	1,46E-12	3,03E-15
7	**1584,62**	**5,36**	65,28	0,05	65,30	0,05	0,01271	0,00008	0,01484	0,01466	0,00008	0,00008	1,65E-11	1,08E-14
8	**1673,62**	**9,33**	70,93	0,49	70,93	0,34	0,01843	0,00120	0,00000	0,00000	0,00000	0,00000	1,13E-12	5,42E-15
9	**1726,79**	**6,41**	74,44	0,21	74,44	0,21	0,01312	0,00048	0,00000	0,00000	0,00000	0,00000	2,86E-12	8,13E-15
10	**1050,86**	**4,82**	36,68	0,12	36,68	0,12	0,01649	0,00085	0,00000	0,00000	0,00000	0,00000	1,60E-12	5,42E-15
11	**550,99**	**3,39**	16,57	0,08	16,57	0,04	0,01291	0,00025	0,02237	0,06626	0,00000	0,00000	5,49E-12	1,36E-14
12	**1067,15**	**4,49**	37,43	0,09	37,43	0,07	0,01257	0,00022	0,01949	0,05773	0,00000	0,00000	6,30E-12	1,08E-14



1,1
0,9
0,7
K+Na+Ca
3
3,2
3,4
Si
Narcea Slates (MD-1)
Cándana Formation (MD-2)
0,4
0,3
0,2
0,1
0
Fe
1,4
1,5
1,6
1,7
1,8
1,9
Al (VI)